

**THE  
MANITOBA  
BRIDGE & IRON WORKS  
LIMITED  
WINNIPEG - CANADA**



**CATALOGUE  
1927**





ALBERTA AND BRITISH COLUMBIA  
518 Lancaster Building  
CALGARY

SASKATCHEWAN  
510 Westman Chambers  
REGINA

Catalogue "F"

• 1927 •

Structural and Fabricated  
**STEEL *and* IRON**  
FOR  
*Architects - Contractors - Manufacturers*

STEEL STRUCTURES

BUILDINGS—*Offices - Warehouses - Industrial Plants*  
BRIDGES—*Railway - Highway - Pontoon - Foot*  
TRANSMISSION TOWERS - WATER TANKS

PLATE AND TANK CONSTRUCTION

TANKS for Gas - Oil - Water - Air  
SPECIAL CATALOGUE FURNISHED ON REQUEST  
PLATE WORK—*Bins - Hoppers - Chutes - Slacks*

CASTINGS

GREY IRON - STEEL - SEMI STEEL

FORGINGS

UPSET RODS - CONTRACTORS' REQUIREMENTS  
COMPLETE CONSTRUCTION LINE

COAL MINING EQUIPMENT

TIPPLES - CAR HAULS - SCREENS  
AIR CLEANING EQUIPMENT - PORTABLE CONVEYORS

CONTRACTORS' SUPPLIES

DERRICKS - BUCKETS - DUMP CARS  
PILE SHOES AND CAPS - SCRAPERS

TRANSMISSION AND CONVEYING MACHINERY

SPECIAL CATALOGUE FURNISHED ON REQUEST

STOCKS

LARGE STOCKS OF STRUCTURALS, PLATES AND BARS

*The*  
**MANITOBA BRIDGE & IRON WORKS**  
*Limited*

Calgary

WINNIPEG

Regina



# *The Leading Steel and Iron Industries*



THE MANITOBA BRIDGE AND IRON WORKS PLANT AT WINNIPEG

Structural Steel and Iron for Bridges and Buildings  
 Steel Tanks and Manufactures of Plate  
 Mining Equipment Grain Elevator and Transmission Machinery  
 Grey Iron Castings Forgings and Pressed Work  
 Railway Frogs, Switches and Crossings



THE MANITOBA STEEL AND IRON CO. WAREHOUSE AT WINNIPEG

Large Stocks of Steel and Iron Bars, Angles, Beams, Channels, Sheets, Plates,  
 Shafting, Boiler Tubes, Bolts, Nuts, Rivets, Reinforcing Steel, Etc.

A Quality  
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Capacity: 25,000  
 Products in  
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Plant:  
 WINNIPEG  
 and  
 SELKIRK



# Industry of Western Canada

A Quarter of a Century of Service and Growth is the record of the Manitoba Bridge and Iron Works, Limited. Development from a small beginning twenty-five years ago is shown better by these views of its plants and warehouses than by words.



THE MANITOBA ROLLING MILLS PLANT AT SELKIRK

Capacity: 25,000 Tons per annum of New Billet Basic Open Hearth Steel  
Products include Merchant Bars, Forging Bars, Concrete Reinforcing—  
Plain and Deformed, Manufacturers' Special Sections.

IN THIS BRIEF SPACE it is impossible to give in detail a picture of our many activities, but the following pages, if carefully studied, will afford the reader many surprises concerning the quality, volume and variety of our products, and the many lines of building and manufacturing in which we are engaged.

## The MANITOBA BRIDGE AND IRON WORKS LIMITED

Plants:  
WINNIPEG  
AND  
SELKIRK

Head Office:  
WINNIPEG

Branches:  
CALGARY  
AND  
REGINA



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## *Announcement*

**T**HIS COMPANY, owned and controlled by Western Canadian capital, has been serving its patrons of the West for a quarter of a century. Commencing twenty-five years ago with a foundry, forge, machine and boiler shop, its progress throughout the years has been practically uninterrupted and at this time additional buildings and departments, comprising bridge and structural, frog and switch, galvanizing, tank, bolt and rivet manufacturing all combine to make it the most comprehensive industry of its kind west of Toronto.

Such growth in a few years, despite the post war depression, was only made possible by the production of first-class goods and the rendering of such service to our new patrons as has made them permanent customers.

Our interests are so interwoven with the welfare of the whole West that we must be able to advise the trade with respect to the best engineering practice in all lines, and to this end maintain a corps of engineering specialists well versed in the different branches.

Branch offices are maintained at Regina and Calgary for the convenience of our many friends.

As large stocks of various grades of steel are stored at our Winnipeg yards, immediate needs can be satisfied at once.

With such a range of manufacturing coupled with capable engineering direction we feel that we are well justified in seeking your business, and invite your inquiries and problems, all of which will be promptly and carefully treated.

THE MANITOBA BRIDGE & IRON WORKS, LIMITED  
WINNIPEG





No. 1—Interior of the Structural Shop of the Manitoba Bridge and Iron Works, Limited

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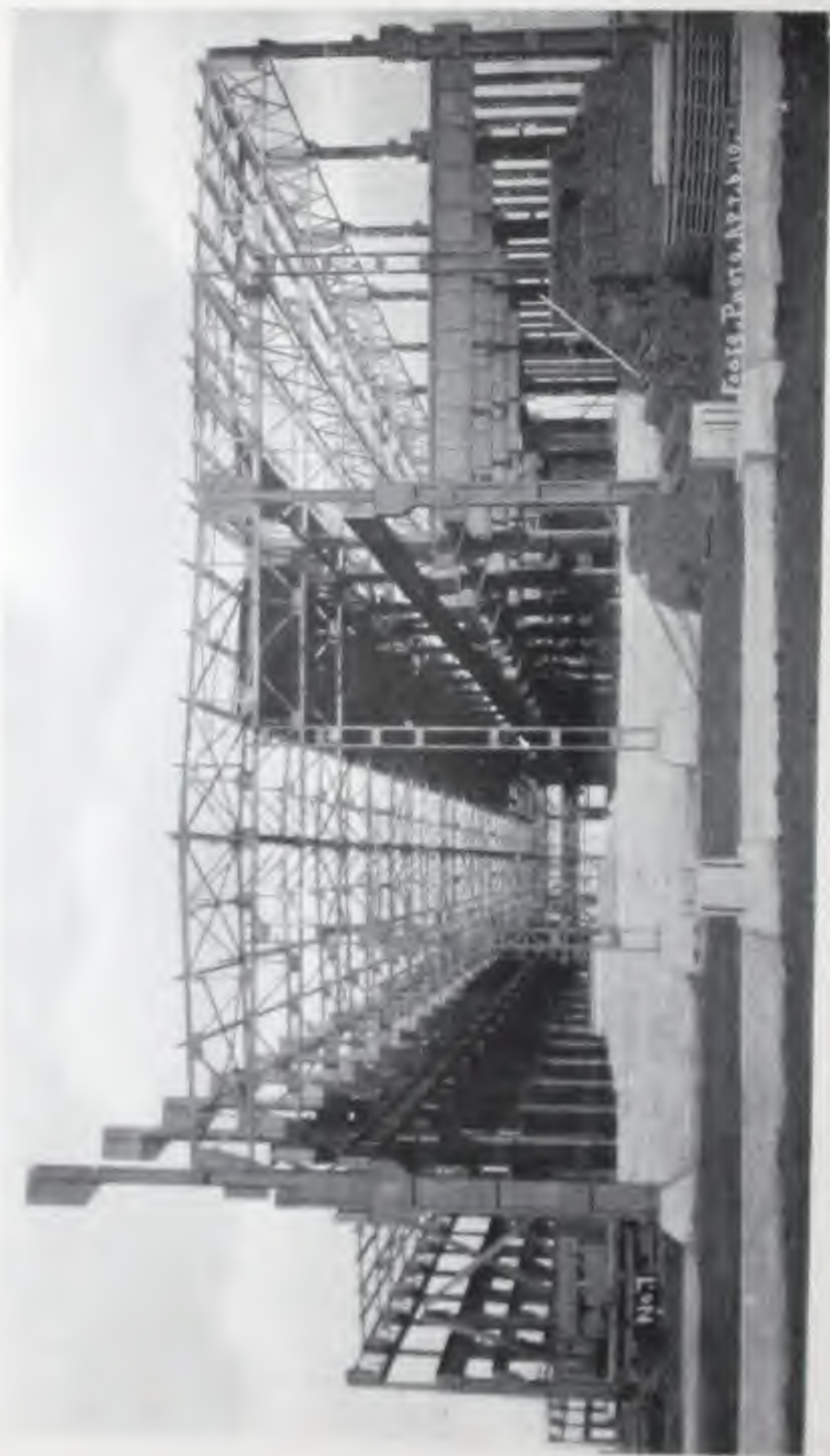
## STRUCTURAL STEEL WORK



FIG. 2—Left Building, in Winnipeg's Business Section, Fabricated and Erected by the Manitoba Bridge and Iron Works, Limited.

The satisfactory service accorded to our customers in contracts which involve the use of structural steel is the result of almost twenty years of specialization in this line, aided by complete equipment to fill the most complicated order.





No. 3—Railway Locomotive Shop, Fabricated and Erected by the Manitoba Bridge and Iron Works, Limited

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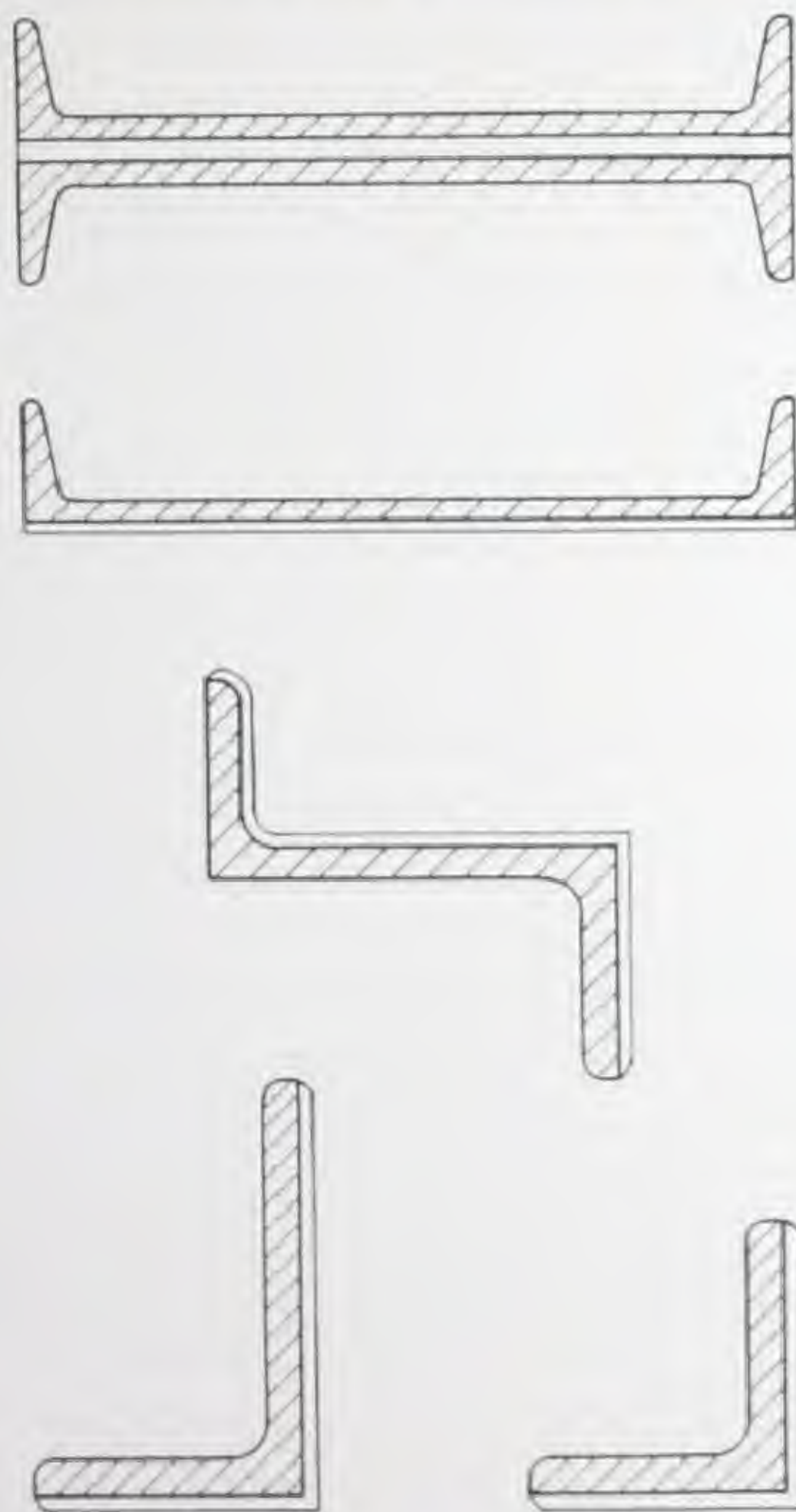
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## STRUCTURAL STEEL

The steel used in structures is in the form of single sections or in combination of two or more sections.

These sections may be in any of the following shapes: square and round bars, flat bars, plates, channels, angles, I-beams, H-sections, zees and tees. Flat bars more than six or seven inches wide are termed plates.



No. 4—Method of Increasing Sectional Areas and Weights of Structural Shapes.

Structural shapes are rolled to a minimum sectional area and the method of increasing the area and weights is shown in the cuts. The hatched portion represents the minimum section, the blank portion the added areas. In case of channels and beams, the enlargement of the section adds an equal amount to the thickness of the web and width of flanges. In the case of angles and zees the effect is to increase slightly the length of the legs.



# THE MANITOBA BRIDGE AND IRON WORKS, LIMITED

**Beams and Channels**—The properties of standard sections are the same, irrespective of the source of manufacture, but different manufacturers have special sections which they roll for particular purposes. Standard I-beams are rolled in depths of from 3-inch to 24-inch, and channels from 3-inch to 15-inch. Depths of beams are from 3-inch to 10-inch consecutively, then 12-inch, 15-inch, 18-inch, 20-inch and 24-inch. For channels, 3-inch to 10-inch consecutively, then 12-inch and 15-inch. For each depth of beam or channel there are several standard weights.

The sizes usually carried in stock are the minimum weights shown in the tables but in the larger sizes two weights are usually carried.

STANDARD CHANNELS IN STOCK

BEAMS			CHANNELS		
Size, In.	Weight per Foot, Lbs.		Size, In.	Weight per Foot, Lbs.	
3	5.7	7.5	3	4.1	
4	7.7	10.0	4	5.4	
5	10.0	13.75	5	6.7	
6	12.3	17.25	6	8.2	13.0
7	15.3	20.0	7	9.8	17.25
8	18.4	23.5	8	11.3	19.25
9	21.8	27.0	9	13.4	
10	25.4	31.0	10	15.2	25.0
12	31.5	36.0	12	20.7	30.0
15	42.0	46.0	15	31.9	36.0
18	54.7	70.0			
20	65.4	81.0			
24	79.0	101.0			

In addition to the above all the sections shown in the tables can be supplied but a reasonable allowance of time must be given to prepare sections from the mill.

**H-Sections**—H-sections as shown in the tables from 3-inch up to 8-inch are all carried in stock and are rolled by the Carnegie Steel Company.

The larger sizes from 8-inch up to 14-inch are usually carried in stock in their minimum weights and other weights to give a gradual increase in size up to the larger sizes. All sizes over 8-inch are rolled by the Bethlehem Steel Company, although the Carnegie Steel Company are now preparing to roll larger sections.

H-SECTIONS (MINIMUM WEIGHTS) IN STOCK

Size, In.	Weight per Foot, Lbs.					
4	12.0					
6	18.0					
8	24.0					
10	32.0	34.0	36.0*	38.0	40.0*	42.0
12	40.0	42.0	44.0*	46.0	48.0*	50.0
14	50.0	52.0	54.0*	56.0	58.0*	60.0

The large range in weights of the 8-inch section is due to the fact that this size is rolled by both Carnegie Steel Company and Bethlehem, the former marked with an asterisk (\*) being Carnegie products, the others Bethlehem.



The Bethlehem Steel Company also roll H-beams in larger weights than shown in all sizes up to 14-inch x 287.5 lbs. per foot but these are only for special conditions. It is usual however, where an extra heavy column is required, to use one of the standard weights and bring it up to the required area by using rivetted cover plates.

**Bethlehem Beams and Girders**—These differ from manufacturers' standard sections rolled by other manufacturers. The beams have heavier flanges and lighter webs. The girders are the strongest sections rolled, for their depth, but are uneconomical where there is room for a deeper section. Tables showing properties and loading are given in the Bethlehem Handbook.

**Angles, Tees and Zees**—Angles are carried in stock in all sizes from  $\frac{1}{2}$ -inch square up to 8-inch square and in all thicknesses from  $\frac{1}{8}$ -inch up to 1-inch both in equal and unequal legs.

Up to 3-inch angles, the thickness varies by  $\frac{1}{16}$ -inches, and weights are carried up to  $\frac{3}{8}$ -inch thick. Over 3-inch to 5-inch, thicknesses are from  $\frac{1}{4}$ -inch, to  $\frac{1}{2}$ -inch, varying by  $\frac{1}{16}$ -inches.

From 6-inch to 8-inch, the thickness starts at  $\frac{3}{8}$ -inch and varies by  $\frac{1}{8}$ -inches up to  $\frac{3}{4}$ -inch. The above variations are those usually carried in stock.

Tees and zees are used only to a limited extent for special purposes and a few of the commoner sizes only are carried in stock.

#### Notes about Structural Sections—

Flanges of both standard I-beams and channels have a uniform slope of  $16\frac{2}{3}\%$  equivalent to 2 inches per foot.

For I-beams and channels, the enlargement of the section adds a proportional amount to the thickness of the web and the width of the flanges. All other dimensions remain unchanged.

For angles, the enlargement of the section (by separating the rolls) slightly increases the length of the legs.

I-beams and channels should be ordered to weights given in the tables. Any weights ordered other than those shown will be furnished and charged for at the next higher weight.

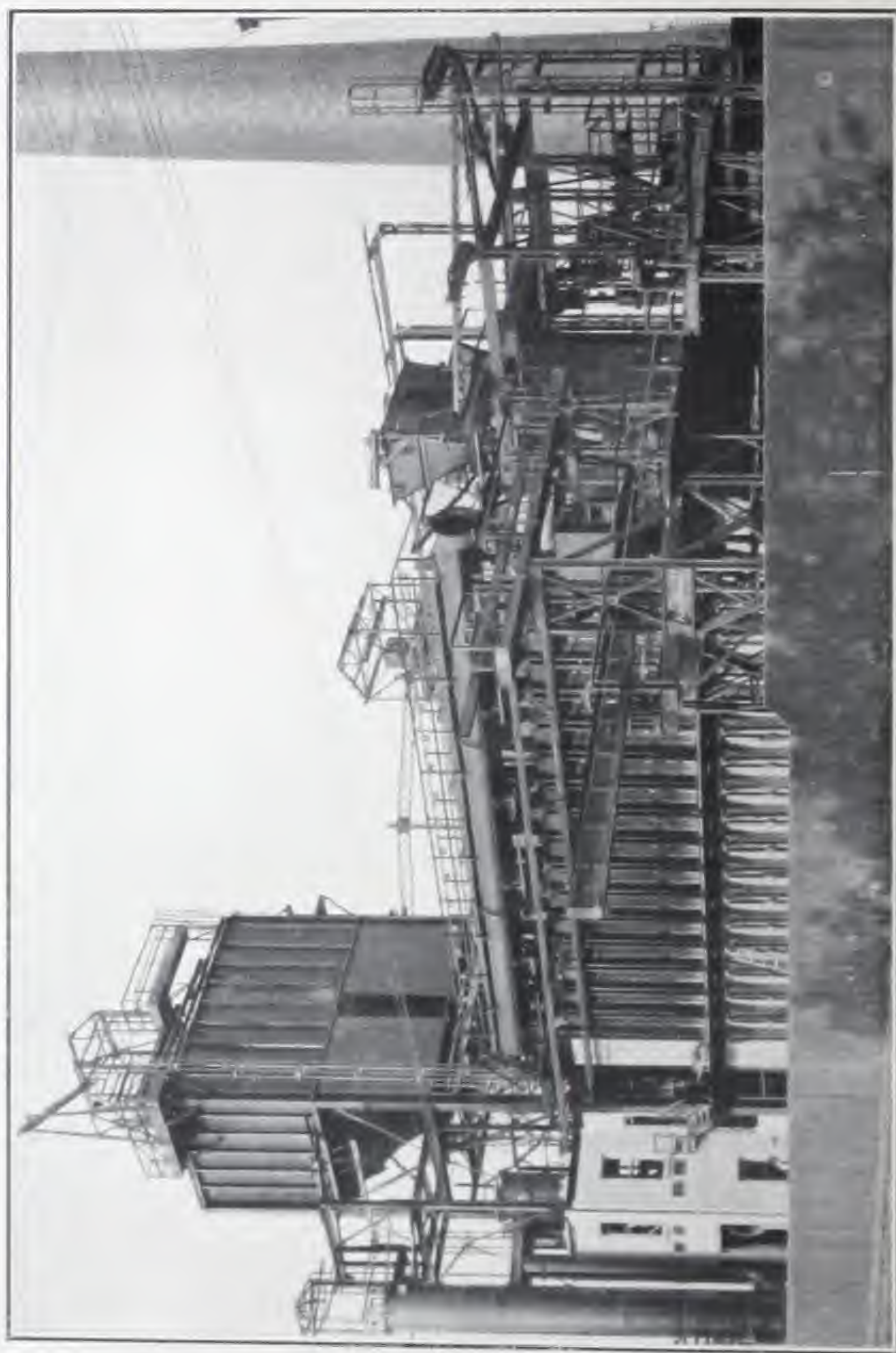
Angles are rolled only to the variation in thickness and weight given in the table.

In ordering, designate either the weight or thickness wanted, but not both.

All structural sections have an allowable variation of  $2\frac{1}{2}\%$  either way from the nominal weight of the section.

All structural sections will be cut to lengths, the extreme variation not exceeding  $\frac{3}{4}$ -inch, unless otherwise arranged.





**No. 5.** — Koppers Coke Plant at the Winnipeg Electric Company's Gas Works, Winnipeg.

The steel and miscellaneous iron work in this building was fabricated by the Manitoba Bridge and Iron Works, Limited, for the Koppers Company of Pittsburgh, Pa.

This is an ideal illustration of the industrial steel and iron fabrication in which we specialize.



# DIMENSIONS, WEIGHTS AND ELEMENTS OF STRUCTURAL BEAMS



Depth of Beam In.	Weight per Foot Lbs.	Area of Section In. <sup>2</sup>	Width of Flange In.	Thick- ness of Web In.	Axis 1-1			Axis 2-2		
					I In. <sup>4</sup>	r In.	S In. <sup>3</sup>	I In. <sup>4</sup>	r In.	S In. <sup>3</sup>
27	90.0	26.34	9.000	0.524	2538.3	10.60	210.1	73.3	1.69	16.7
24	120.0	33.13	8.048	0.708	3010.8	9.26	250.9	84.9	1.56	21.1
	115.0	33.67	7.987	0.737	2940.5	9.35	245.0	82.8	1.57	20.7
	110.0	32.18	7.925	0.675	2869.1	9.44	239.1	80.6	1.58	20.3
	105.0	30.98	7.875	0.625	2811.5	9.53	234.3	78.9	1.60	20.0
	100.0	29.55	7.847	0.747	2371.8	9.65	197.6	48.4	1.29	15.4
	95.0	27.79	7.189	0.689	2301.5	9.68	191.8	47.0	1.30	15.0
	90.0	26.30	7.124	0.624	2250.1	9.71	185.8	45.5	1.32	14.8
	85.0	24.84	7.053	0.563	2150.8	9.53	180.0	44.2	1.33	14.5
	79.9	23.53	7.000	0.500	2087.2	9.46	173.0	42.9	1.36	14.2
	74.2	21.70	6.000	0.470	1950.1	9.48	162.5	61.2	1.68	12.6
21	60.1	17.68	8.250	0.828	1233.5	8.36	117.7	41.5	1.57	10.6
20	100.0	29.20	7.273	0.873	1648.3	7.51	164.8	52.4	1.34	14.4
	95.0	27.74	7.200	0.800	1599.7	7.59	160.0	50.5	1.35	14.0
	90.0	26.26	7.126	0.726	1550.3	7.68	155.0	48.7	1.36	13.7
	85.0	24.80	7.053	0.653	1501.7	7.78	150.2	47.0	1.38	13.3
	81.4	23.74	7.000	0.600	1466.3	7.86	146.0	45.8	1.39	13.1
	75.0	21.96	6.391	0.641	1263.5	7.63	126.3	39.1	1.17	9.4
	70.0	20.42	6.317	0.567	1214.2	7.71	121.4	28.9	1.10	8.2
	65.4	19.08	6.250	0.500	1169.6	7.83	116.9	27.9	1.21	8.9
	60.0	17.68	6.250	0.500	1169.6	7.83	116.9	27.9	1.21	8.9
18	90.0	26.29	7.236	0.796	1256.5	6.91	139.0	51.9	1.40	14.3
	85.0	24.81	7.154	0.714	1216.6	7.00	133.2	49.8	1.42	14.0
	80.0	23.34	7.072	0.632	1176.8	7.10	130.8	47.9	1.43	13.6
	75.0	22.04	7.000	0.560	1141.8	7.20	126.9	46.1	1.45	13.2
	70.0	20.46	6.251	0.711	917.5	6.70	101.9	24.4	1.09	7.8
	65.0	18.98	6.166	0.626	877.7	6.80	97.5	23.4	1.11	7.6
	60.0	17.50	6.087	0.547	837.8	6.92	93.1	22.3	1.13	7.3
	54.7	15.93	6.000	0.460	795.5	7.07	88.4	21.2	1.15	7.1
	48.5	14.66	7.500	0.380	737.1	7.23	81.9	30.0	1.36	8.0
	45.0	13.85	6.278	0.868	687.2	7.61	61.6	30.6	1.14	9.8
15	70.0	20.38	6.180	0.770	659.6	5.69	67.9	28.8	1.16	9.0
	65.0	18.91	6.082	0.672	632.1	5.78	64.3	27.2	1.20	8.6
	60.8	17.68	6.000	0.590	609.0	5.87	61.2	26.0	1.21	8.5
	55.0	16.06	5.738	0.648	568.7	5.63	67.8	27.0	1.63	5.9
	50.0	14.59	5.646	0.550	481.1	5.74	64.2	26.0	1.65	5.7
	45.0	13.12	5.542	0.452	453.6	5.88	60.5	15.0	1.67	5.4
	42.8	12.45	5.500	0.410	441.8	5.95	58.8	14.0	1.68	5.5
	37.8	10.91	5.295	0.362	405.6	6.10	54.1	10.9	1.25	4.9



# DIMENSIONS, WEIGHTS AND ELEMENTS OF STRUCTURAL BEAMS



Depth of Beam In.	Weight per Foot Lbs.	Area of Section In. <sup>2</sup>	Width of Flange In.	Thickness of Web In.	Axis 1-1			Axis 2-2		
					I In. <sup>4</sup>	r In.	S In. <sup>3</sup>	I In. <sup>4</sup>	r In.	S In. <sup>3</sup>
12	55.0	16.04	5.600	0.810	319.3	4.46	53.2	17.3	1.04	6.2
	50.0	14.57	5.477	0.687	301.6	4.55	50.3	16.0	1.05	5.8
	45.0	13.10	5.255	0.565	284.1	4.66	47.3	14.8	1.06	5.5
	40.8	11.84	5.250	0.460	268.9	4.77	44.8	13.8	1.08	5.3
	35.0	10.20	5.078	0.428	227.0	4.72	37.8	10.0	0.99	3.9
	31.8	9.26	5.000	0.350	215.8	4.83	36.0	9.5	1.01	3.8
	27.9	8.15	6.000	0.284	199.4	4.95	33.2	12.6	1.24	4.2
10	40.0	11.69	5.091	0.741	158.0	3.68	31.6	9.4	0.90	3.7
	35.0	10.22	4.944	0.594	145.8	3.78	29.2	8.5	0.91	3.4
	30.0	8.75	4.797	0.447	133.5	3.91	26.7	7.6	0.93	3.2
	25.4	7.38	4.660	0.310	122.1	4.07	24.4	6.9	0.97	3.0
	22.4	6.54	5.500	0.252	113.6	4.17	22.7	9.0	1.17	3.3
9	35.0	10.22	4.764	0.724	111.3	3.30	24.7	7.3	0.84	3.0
	30.0	8.76	4.601	0.561	101.4	3.40	22.5	6.4	0.85	2.8
	25.0	7.28	4.437	0.397	91.4	3.54	20.3	5.6	0.88	2.5
	21.8	6.32	4.330	0.290	84.9	3.67	18.9	5.2	0.90	2.4
8	25.5	7.43	4.262	0.522	68.1	3.03	17.0	4.7	0.80	2.2
	23.0	6.71	4.171	0.441	64.2	3.09	16.0	4.4	0.81	2.1
	20.5	5.97	4.079	0.349	60.2	3.18	15.1	4.0	0.82	2.0
	18.4	5.34	4.000	0.270	56.9	3.26	14.2	3.8	0.84	1.9
	17.5	5.13	5.000	0.220	58.4	3.38	14.6	6.2	1.10	2.5
7	20.0	5.83	3.860	0.450	41.9	2.68	12.0	3.1	0.74	1.6
	17.5	5.09	3.755	0.345	38.9	2.77	11.1	2.9	0.76	1.6
	15.3	4.43	3.660	0.250	36.2	2.86	10.4	2.7	0.78	1.5
6	17.25	5.02	3.565	0.405	26.0	2.28	8.7	2.3	0.68	1.3
	14.75	4.20	3.443	0.343	23.8	2.36	7.9	2.1	0.69	1.2
	12.5	3.61	3.330	0.230	21.8	2.46	7.3	1.8	0.72	1.1
5	14.75	4.29	3.284	0.494	15.0	1.87	6.0	1.7	0.63	1.0
	12.25	3.56	3.137	0.347	13.5	1.95	5.4	1.4	0.63	0.91
	10.0	2.87	3.000	0.210	12.1	2.05	4.8	1.2	0.65	0.82
4	10.5	3.05	2.870	0.400	7.1	1.52	3.5	1.0	0.57	0.70
	9.5	2.76	2.790	0.326	6.7	1.56	3.3	0.91	0.58	0.65
	8.5	2.46	2.723	0.253	6.3	1.60	3.2	0.83	0.58	0.61
	7.7	2.21	2.660	0.190	6.0	1.64	3.0	0.77	0.59	0.58
3	7.5	2.17	2.509	0.349	2.9	1.15	1.9	0.59	0.52	0.47
	6.5	1.88	2.411	0.251	2.7	1.19	1.8	0.51	0.52	0.43
	5.7	1.64	2.330	0.170	2.5	1.23	1.7	0.46	0.53	0.40

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Area, in.<sup>2</sup>

I<sub>1-1</sub>, in.<sup>4</sup>

r<sub>1-1</sub>, in.

I<sub>2-2</sub>, in.<sup>4</sup>

r<sub>2-2</sub>, in.

Weight, Lbs. per Foot

Safe load

type are (





# DIMENSIONS, WEIGHTS, ELEMENTS AND SAFE LOADS OF

## H- AND I-BEAM COLUMNS

Safe Loads in Thousands of Pounds

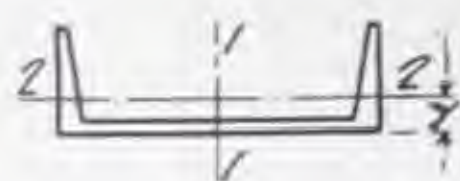
Allowable fiber stress per square inch

13,000 pounds for lengths of 60 feet or under, reduced for lengths over 60 feet. Weights do not include details.

Effective Length in Feet	I-Beams					H-Beams									
	8 in.	10 in.	12 in.	14 in.	16 in.	8 in.		10 in.		12 in.		14 in.		16 in.	
	15.4 lb.	15.4 lb.	15.4 lb.	15.4 lb.	15.4 lb.	37.7 lb.	34.3 lb.	37.7 lb.	34.3 lb.	37.7 lb.	34.3 lb.	37.7 lb.	34.3 lb.	37.7 lb.	34.3 lb.
3	69.3	57.5	46.0	37.3	28.5	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
4	69.3	56.7	44.4	33.5	24.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
5	63.3	49.9	38.8	32.8	21.9	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
6	55.7	43.1	32.2	22.9	16.5	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
7	48.1	36.2	26.2	18.0	12.5	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
8	40.5	30.2	22.2	15.0	10.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
9	32.9	24.6	17.9	12.0	8.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0	143.0	130.0
10	25.3	19.5	14.0	9.0	6.0	136.9	126.0	136.9	126.0	136.9	126.0	136.9	126.0	136.9	126.0
11	22.5	17.0	12.5	8.0	5.0	129.7	119.6	129.7	119.6	129.7	119.6	129.7	119.6	129.7	119.6
12	19.7	14.5	10.5	7.0	4.0	122.5	113.2	122.5	113.2	122.5	113.2	122.5	113.2	122.5	113.2
13	16.9	12.5	9.0	6.0	3.0	115.3	106.8	115.3	106.8	115.3	106.8	115.3	106.8	115.3	106.8
14	14.1	10.5	7.5	5.0	2.0	108.1	100.4	108.1	100.4	108.1	100.4	108.1	100.4	108.1	100.4
15	11.3	8.5	6.0	4.0	1.5	100.9	93.9	100.9	93.9	100.9	93.9	100.9	93.9	100.9	93.9
16						93.7	87.5	93.7	87.5	93.7	87.5	93.7	87.5	93.7	87.5
17						86.4	81.1	86.4	81.1	86.4	81.1	86.4	81.1	86.4	81.1
18						79.2	74.7	79.2	74.7	79.2	74.7	79.2	74.7	79.2	74.7
19						71.9	68.0	71.9	68.0	71.9	68.0	71.9	68.0	71.9	68.0
20						64.6	61.0	64.6	61.0	64.6	61.0	64.6	61.0	64.6	61.0
21						57.3	54.0	57.3	54.0	57.3	54.0	57.3	54.0	57.3	54.0
22						50.0	47.0	50.0	47.0	50.0	47.0	50.0	47.0	50.0	47.0
23						42.7	40.0	42.7	40.0	42.7	40.0	42.7	40.0	42.7	40.0
24						35.4	33.0	35.4	33.0	35.4	33.0	35.4	33.0	35.4	33.0
25						28.1	26.0	28.1	26.0	28.1	26.0	28.1	26.0	28.1	26.0
26						20.8	19.0	20.8	19.0	20.8	19.0	20.8	19.0	20.8	19.0
27						13.5	12.0	13.5	12.0	13.5	12.0	13.5	12.0	13.5	12.0
28						6.2	5.5	6.2	5.5	6.2	5.5	6.2	5.5	6.2	5.5
29															
30															
Area, in. <sup>2</sup>	34.4	45.3	61.2	81.2	110.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
I <sub>x</sub> , in. <sup>4</sup>	569.0	2,221.8	8,121.1	16,010.0	27,112.8	47,443.1	144,052.8	10,710.7							
I <sub>y</sub> , in. <sup>4</sup>	3,262.8	8,622.4	16,010.0	27,112.8	47,443.1	10,710.7	3,472.5	5,622.0	8,622.4	16,010.0	27,112.8	47,443.1	10,710.7	3,472.5	5,622.0
I <sub>x</sub> , in. <sup>3</sup>	3,861.2	11,811.7	27,112.8	47,443.1	10,710.7	15,714.7	14,714.7	13,714.7	12,714.7	11,714.7	10,714.7	9,714.7	8,714.7	7,714.7	6,714.7
I <sub>y</sub> , in. <sup>3</sup>	11,811.7	27,112.8	47,443.1	10,710.7	15,714.7	14,714.7	13,714.7	12,714.7	11,714.7	10,714.7	9,714.7	8,714.7	7,714.7	6,714.7	5,714.7
Weight, lbs. per foot	18.4	24.6	33.0	44.0	58.0	37.7	34.3	37.7	34.3	37.7	34.3	37.7	34.3	37.7	34.3

Safe load values in "light" type are for ratios of L/r not over 80; in "heavy" type are for ratios up to 120 (L/r); in "medium" type are for ratios not over 200 (L/r).



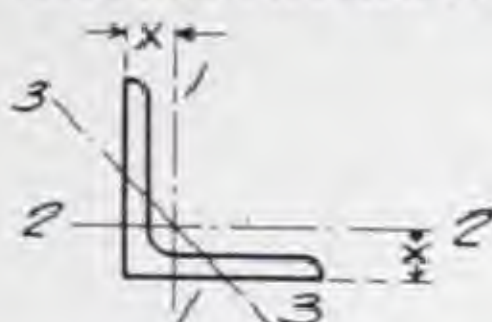


# DIMENSIONS, WEIGHTS AND ELEMENTS OF STRUCTURAL CHANNELS American Standard Sections

Depth of Channel	Weight per Foot	Area of Section	Width of Flange	Thick- ness of Web	Axis 1-1			Axis 2-2			
					I	r	S	I	r	S	Y
In.	Lbs.	In. <sup>2</sup>	In.	In.	In. <sup>4</sup>	In.	In. <sup>3</sup>	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.
15	55.0	16.11	3.814	0.814	429.0	5.16	57.2	12.1	0.87	4.1	0.82
	50.0	14.64	3.716	0.716	401.4	5.24	53.6	11.2	0.87	3.8	0.80
	45.0	13.17	3.618	0.618	373.9	5.33	49.8	10.3	0.88	3.6	0.79
	40.0	11.70	3.520	0.520	346.3	5.44	46.2	9.3	0.89	3.4	0.78
	35.0	10.23	3.422	0.422	318.7	5.58	42.5	8.4	0.91	3.2	0.79
	33.9	9.90	3.400	0.400	312.6	5.62	41.7	8.2	0.91	3.2	0.79
12	40.0	11.73	3.415	0.755	196.5	4.09	32.8	6.6	0.75	2.5	0.72
	35.0	10.26	3.292	0.632	178.8	4.18	29.8	5.9	0.76	2.3	0.69
	30.0	8.79	3.170	0.510	161.2	4.28	26.9	5.2	0.77	2.1	0.68
	25.0	7.32	3.047	0.387	143.5	4.43	23.9	4.5	0.79	1.9	0.68
	20.7	6.03	2.940	0.280	128.1	4.61	21.4	3.9	0.81	1.7	0.70
10	35.0	10.27	3.180	0.820	115.2	3.34	23.0	4.6	0.67	1.9	0.69
	30.0	8.80	3.033	0.673	103.0	3.42	20.6	4.0	0.67	1.7	0.65
	25.0	7.33	2.886	0.526	90.7	3.52	18.1	3.4	0.68	1.5	0.62
	20.0	5.86	2.739	0.379	78.5	3.66	15.7	2.8	0.70	1.3	0.61
	15.3	4.47	2.600	0.240	66.9	3.87	13.4	2.3	0.72	1.2	0.64
9	25.0	7.33	2.812	0.612	70.5	3.10	15.7	3.0	0.64	1.4	0.61
	20.0	5.86	2.648	0.448	60.6	3.22	13.5	2.4	0.65	1.2	0.59
	15.0	4.39	2.485	0.285	50.7	3.40	11.3	1.9	0.67	1.0	0.59
	13.4	3.89	2.430	0.230	47.3	3.49	10.5	1.8	0.67	0.97	0.61
8	21.25	6.23	2.619	0.579	47.6	2.77	11.9	2.2	0.60	1.1	0.59
	18.75	5.49	2.527	0.487	43.7	2.82	10.9	2.0	0.60	1.0	0.57
	16.25	4.76	2.435	0.395	39.8	2.89	9.9	1.8	0.61	0.94	0.56
	13.75	4.02	2.343	0.303	35.8	2.99	9.0	1.5	0.62	0.86	0.56
	11.5	3.36	2.260	0.220	32.3	3.10	8.1	1.3	0.63	0.79	0.58
7	19.75	5.79	2.509	0.629	33.1	2.39	9.4	1.8	0.56	0.96	0.58
	17.25	5.05	2.404	0.524	30.1	2.44	8.6	1.6	0.56	0.86	0.55
	14.75	4.32	2.299	0.419	27.1	2.51	7.7	1.4	0.57	0.79	0.53
	12.25	3.58	2.194	0.314	24.1	2.59	6.9	1.2	0.58	0.71	0.53
	9.8	2.85	2.090	0.210	21.1	2.72	6.0	0.98	0.59	0.63	0.55
6	15.5	4.54	2.279	0.559	19.5	2.07	6.5	1.3	0.53	0.73	0.55
	13.0	3.81	2.157	0.437	17.3	2.13	5.8	1.1	0.53	0.65	0.52
	10.5	3.07	2.034	0.314	15.1	2.22	5.0	0.87	0.53	0.57	0.50
	8.2	2.39	1.920	0.200	13.0	2.34	4.3	0.70	0.54	0.50	0.52
5	11.5	3.36	2.032	0.472	10.4	1.76	4.1	0.82	0.49	0.54	0.51
	9.0	2.63	1.885	0.325	8.8	1.83	3.5	0.64	0.49	0.45	0.48
	6.7	1.95	1.750	0.190	7.4	1.95	3.0	0.48	0.50	0.38	0.49
4	7.25	2.12	1.720	0.320	4.5	1.47	2.3	0.44	0.46	0.35	0.46
	6.25	1.82	1.647	0.247	4.1	1.50	2.1	0.38	0.45	0.32	0.46
	5.4	1.56	1.580	0.180	3.8	1.56	1.9	0.32	0.45	0.29	0.46
3	6.0	1.75	1.596	0.356	2.1	1.08	1.4	0.31	0.42	0.27	0.46
	5.0	1.46	1.498	0.258	1.8	1.12	1.2	0.25	0.41	0.24	0.44
	4.1	1.19	1.410	0.170	1.6	1.17	1.1	0.20	0.41	0.21	0.44



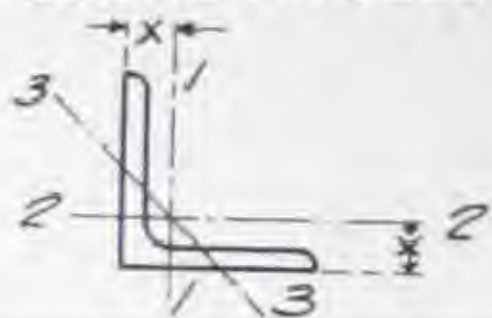
### DIMENSIONS, WEIGHTS AND ELEMENTS OF EQUAL ANGLES



Size In.	Thickness In.	Weight per Foot Lbs.	Area of Section In. <sup>2</sup>	Axis 1-1 and Axis 2-2				Axis 3-3
				I In. <sup>4</sup>	r In.	S In. <sup>3</sup>	x In.	r <sub>min.</sub> In.
8 x 8	1 1/8	56.9	16.73	98.0	2.42	17.5	2.41	1.55
	1 1/16	54.0	15.87	93.5	2.43	16.7	2.39	1.56
	1	51.0	15.00	89.0	2.44	15.8	2.37	1.56
	15/16	48.1	14.12	84.3	2.44	14.9	2.34	1.56
	7/8	45.0	13.23	79.6	2.45	14.0	2.32	1.56
	13/16	42.0	12.34	74.7	2.46	13.1	2.30	1.57
	3/4	38.9	11.44	69.7	2.47	12.2	2.28	1.57
	11/16	35.8	10.53	64.6	2.48	11.2	2.25	1.58
	5/8	32.7	9.61	59.4	2.49	10.3	2.23	1.58
	9/16	29.6	8.68	54.1	2.50	9.3	2.21	1.58
	1/2	26.4	7.75	48.6	2.51	8.4	2.19	1.58
6 x 6	1	37.4	11.00	35.5	1.80	8.6	1.86	1.16
	15/16	35.3	10.37	33.7	1.80	8.1	1.84	1.16
	7/8	33.1	9.73	31.9	1.81	7.6	1.82	1.17
	13/16	31.0	9.09	30.1	1.82	7.2	1.80	1.17
	3/4	28.7	8.44	28.2	1.83	6.7	1.78	1.17
	11/16	26.5	7.78	26.2	1.83	6.2	1.75	1.17
	5/8	24.2	7.11	24.2	1.84	5.7	1.73	1.17
	9/16	21.9	6.43	22.1	1.85	5.1	1.71	1.18
	1/2	19.6	5.75	19.9	1.86	4.6	1.68	1.18
	7/16	17.2	5.06	17.7	1.87	4.1	1.66	1.19
	3/8	14.9	4.36	15.4	1.88	3.5	1.64	1.19
5 x 5	1	30.6	9.00	19.6	1.48	5.8	1.61	0.96
	15/16	28.9	8.50	18.7	1.48	5.5	1.59	0.96
	7/8	27.2	7.98	17.8	1.49	5.2	1.57	0.96
	13/16	25.4	7.47	16.8	1.50	4.9	1.55	0.97
	3/4	23.6	6.94	15.7	1.50	4.5	1.52	0.97
	11/16	21.8	6.40	14.7	1.51	4.2	1.50	0.97
	5/8	20.0	5.86	13.6	1.52	3.9	1.48	0.97
	9/16	18.1	5.31	12.4	1.53	3.5	1.46	0.98
	1/2	16.2	4.75	11.3	1.54	3.2	1.43	0.98
	7/16	14.3	4.18	10.0	1.55	2.8	1.41	0.98
	3/8	12.3	3.61	8.7	1.56	2.4	1.39	0.99
4 x 4	15/16	19.9	5.84	8.1	1.18	3.0	1.29	0.77
	3/4	18.5	5.44	7.7	1.19	2.8	1.27	0.77
	11/16	17.1	5.03	7.2	1.19	2.6	1.25	0.77
	5/8	15.7	4.61	6.7	1.20	2.4	1.23	0.77
	9/16	14.3	4.18	6.1	1.21	2.2	1.21	0.78
	1/2	12.8	3.75	5.6	1.22	2.0	1.18	0.78
	7/16	11.3	3.31	5.0	1.23	1.8	1.16	0.78
	3/8	9.8	2.86	4.4	1.23	1.5	1.14	0.79
	5/16	8.2	2.40	3.7	1.24	1.3	1.12	0.79
	1/4	6.6	1.94	3.0	1.25	1.0	1.09	0.79



# DIMENSIONS, WEIGHTS AND ELEMENTS OF EQUAL ANGLES



Size In.	Thickness In.	Weight per Foot Lbs.	Area of Section In. <sup>2</sup>	Axis 1-1 and Axis 2-2				Axis 3-3
				I In. <sup>4</sup>	r In.	S In. <sup>3</sup>	x In.	r <sub>min.</sub> In.
3½ x 3½	¾	16.0	4.69	5.0	1.03	2.1	1.15	0.67
	⅝	13.6	3.98	4.3	1.04	1.8	1.10	0.68
	½	11.1	3.25	3.6	1.06	1.5	1.06	0.68
	⅜	9.8	2.87	3.3	1.07	1.3	1.04	0.68
	⅜	8.5	2.48	2.9	1.07	1.2	1.01	0.69
	⅜	7.2	2.09	2.5	1.08	0.98	0.99	0.69
	¼	5.8	1.69	2.0	1.09	0.79	0.97	0.69
3 x 3	⅝	11.5	3.36	2.6	0.88	1.3	0.98	0.57
	½	9.4	2.75	2.2	0.90	1.1	0.93	0.58
	⅜	8.3	2.43	2.0	0.91	0.95	0.91	0.58
	⅜	7.2	2.11	1.8	0.91	0.83	0.89	0.58
	⅜	6.1	1.78	1.5	0.92	0.71	0.87	0.59
	¼	4.9	1.44	1.2	0.93	0.58	0.84	0.59
2½ x 2½	½	7.7	2.25	1.2	0.74	0.73	0.81	0.47
	⅜	5.9	1.73	0.98	0.75	0.57	0.76	0.48
	⅜	5.0	1.47	0.85	0.76	0.48	0.74	0.49
	¼	4.1	1.19	0.70	0.77	0.39	0.72	0.49
	⅜	3.07	0.90	0.55	0.78	0.30	0.69	0.49
	⅜	2.08	0.61	0.38	0.79	0.20	0.67	0.50
2 x 2	⅝	4.7	1.36	0.48	0.59	0.35	0.64	0.39
	⅜	3.92	1.15	0.42	0.60	0.30	0.61	0.39
	¼	3.19	0.94	0.35	0.61	0.25	0.59	0.39
	⅜	2.44	0.71	0.28	0.62	0.19	0.57	0.40
	⅜	1.65	0.48	0.19	0.63	0.13	0.55	0.40
1¾ x 1¾	⅝	3.99	1.17	0.31	0.51	0.26	0.57	0.34
	⅜	3.39	1.00	0.27	0.52	0.23	0.55	0.34
	¼	2.77	0.81	0.23	0.53	0.19	0.53	0.34
	⅜	2.12	0.62	0.18	0.54	0.14	0.51	0.35
	⅜	1.44	0.42	0.13	0.55	0.10	0.48	0.35
1½ x 1½	⅝	3.35	0.98	0.19	0.44	0.19	0.51	0.29
	⅜	2.86	0.84	0.16	0.44	0.16	0.49	0.29
	¼	2.34	0.69	0.14	0.45	0.13	0.47	0.29
	⅜	1.80	0.53	0.11	0.46	0.10	0.44	0.29
	⅜	1.23	0.36	0.08	0.46	0.07	0.42	0.30
1¼ x 1¼	¼	1.92	0.56	0.08	0.37	0.09	0.40	0.24
	⅜	1.48	0.43	0.06	0.38	0.07	0.38	0.24
	⅜	1.01	0.30	0.04	0.38	0.05	0.35	0.25
1 x 1	¼	1.49	0.44	0.04	0.29	0.06	0.34	0.19
	⅜	1.16	0.34	0.03	0.30	0.04	0.32	0.19
	⅜	0.80	0.23	0.02	0.31	0.03	0.30	0.19



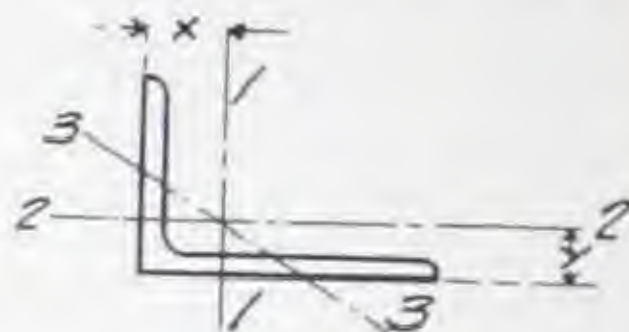
# DIMENSIONS, WEIGHTS AND ELEMENTS OF UNEQUAL ANGLES



Size	Thick- ness	Wt. per Foot	Area of Sec- tion	Axis 1-1				Axis 2-2				Axis 3-3	
				I	r	S	x	I	r	S	y	r <sub>min</sub>	
In.	In.	Lbs.	In. <sup>2</sup>	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In.	
8 x 6	1	44.2	13.00	80.8	2.49	15.1	2.65	38.8	1.73	8.9	1.65	1.28	
	$\frac{13}{16}$	41.7	12.25	76.6	2.50	14.3	2.63	36.8	1.73	8.4	1.63	1.28	
	$\frac{7}{8}$	39.1	11.48	72.3	2.51	13.4	2.61	34.9	1.74	7.9	1.61	1.28	
	$\frac{15}{16}$	36.5	10.72	67.9	2.52	12.5	2.59	32.8	1.75	7.4	1.59	1.29	
	$\frac{3}{4}$	33.8	9.94	63.4	2.53	11.7	2.56	30.7	1.76	6.9	1.56	1.29	
	$\frac{11}{16}$	31.2	9.15	58.8	2.54	10.8	2.54	28.6	1.77	6.4	1.54	1.29	
	$\frac{5}{8}$	28.5	8.36	54.1	2.54	9.9	2.52	26.3	1.77	5.9	1.52	1.30	
	$\frac{9}{16}$	25.7	7.56	49.3	2.55	8.9	2.50	24.0	1.78	5.3	1.50	1.30	
	$\frac{1}{2}$	23.0	6.75	44.3	2.56	8.0	2.47	21.7	1.79	4.8	1.47	1.30	
	$\frac{7}{16}$	20.2	5.93	39.2	2.57	7.1	2.45	19.3	1.80	4.2	1.45	1.30	
8 x 3 $\frac{1}{2}$	1	35.7	10.50	66.2	2.51	13.7	3.17	7.8	0.86	3.0	0.92	0.73	
	$\frac{15}{16}$	33.7	9.90	62.9	2.52	12.9	3.14	7.4	0.87	2.9	0.89	0.73	
	$\frac{7}{8}$	31.7	9.30	59.4	2.53	12.2	3.12	7.1	0.87	2.7	0.87	0.73	
	$\frac{13}{16}$	29.6	8.68	55.9	2.54	11.4	3.10	6.7	0.88	2.5	0.85	0.73	
	$\frac{3}{4}$	27.5	8.06	52.3	2.55	10.6	3.07	6.3	0.88	2.3	0.82	0.73	
	$\frac{11}{16}$	25.3	7.43	48.5	2.56	9.8	3.05	5.9	0.89	2.2	0.80	0.73	
	$\frac{5}{8}$	23.2	6.80	44.7	2.57	9.0	3.03	5.4	0.90	2.0	0.78	0.74	
	$\frac{9}{16}$	21.0	6.15	40.8	2.57	8.2	3.00	5.0	0.90	1.8	0.75	0.74	
	$\frac{1}{2}$	18.7	5.50	36.7	2.58	7.3	2.98	4.5	0.91	1.6	0.73	0.74	
	$\frac{7}{16}$	16.5	4.84	32.5	2.59	6.4	2.95	4.1	0.92	1.5	0.70	0.74	
7 x 3 $\frac{1}{2}$	1	32.3	9.50	45.4	2.19	10.6	2.71	7.5	0.89	3.0	0.96	0.74	
	$\frac{15}{16}$	30.5	8.97	43.1	2.19	10.0	2.69	7.2	0.89	2.8	0.94	0.74	
	$\frac{7}{8}$	28.7	8.42	40.8	2.20	9.4	2.66	6.8	0.90	2.6	0.91	0.74	
	$\frac{13}{16}$	26.8	7.87	38.4	2.21	8.8	2.64	6.5	0.91	2.5	0.89	0.74	
	$\frac{3}{4}$	24.9	7.31	36.0	2.22	8.2	2.62	6.1	0.91	2.3	0.87	0.74	
	$\frac{11}{16}$	23.0	6.75	33.5	2.23	7.6	2.60	5.7	0.92	2.1	0.85	0.74	
	$\frac{5}{8}$	21.0	6.17	30.9	2.24	7.0	2.57	5.3	0.93	2.0	0.82	0.75	
	$\frac{9}{16}$	19.1	5.59	28.2	2.25	6.3	2.55	4.9	0.93	1.8	0.80	0.75	
	$\frac{1}{2}$	17.0	5.00	25.4	2.25	5.7	2.53	4.4	0.94	1.6	0.78	0.75	
	$\frac{7}{16}$	15.0	4.40	22.6	2.26	5.0	2.50	4.0	0.95	1.4	0.75	0.76	
6 x 4	1	30.6	9.00	30.8	1.85	8.0	2.17	10.8	1.09	3.8	1.17	0.85	
	$\frac{15}{16}$	28.9	8.50	29.3	1.86	7.6	2.14	10.3	1.10	3.6	1.14	0.85	
	$\frac{7}{8}$	27.2	7.98	27.7	1.86	7.2	2.12	9.8	1.11	3.4	1.12	0.86	
	$\frac{13}{16}$	25.4	7.47	26.1	1.87	6.7	2.10	9.2	1.11	3.2	1.10	0.86	
	$\frac{3}{4}$	23.6	6.94	24.5	1.88	6.2	2.08	8.7	1.12	3.0	1.08	0.86	
	$\frac{11}{16}$	21.8	6.40	22.8	1.89	5.8	2.06	8.1	1.13	2.8	1.06	0.86	
	$\frac{5}{8}$	20.0	5.86	21.1	1.90	5.3	2.03	7.5	1.13	2.5	1.03	0.86	
	$\frac{9}{16}$	18.1	5.31	19.3	1.90	4.8	2.01	6.9	1.14	2.3	1.01	0.87	
	$\frac{1}{2}$	16.2	4.75	17.4	1.91	4.3	1.99	6.3	1.15	2.1	0.99	0.87	
	$\frac{7}{16}$	14.3	4.18	15.5	1.92	3.8	1.96	5.6	1.16	1.8	0.96	0.87	
	$\frac{3}{8}$	12.3	3.61	13.5	1.93	3.3	1.94	4.9	1.17	1.6	0.94	0.88	



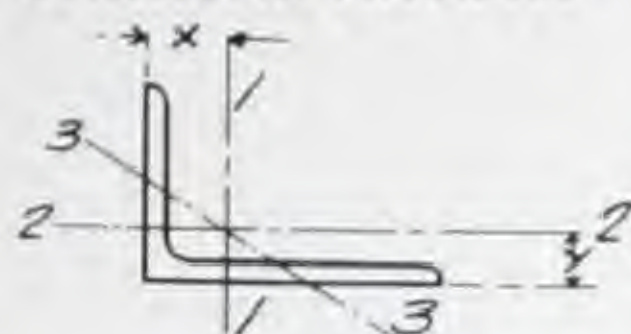
# DIMENSIONS, WEIGHTS AND ELEMENTS OF UNEQUAL ANGLES



Size	Thick- ness	Wt. per Foot	Area of Sec- tion	Axis 1-1				Axis 2-2				Axis 3-3
				I	r	S	x	I	r	S	y	r <sub>min.</sub>
In.	In.	Lbs.	In. <sup>2</sup>	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In.
6 x 3½	1	28.9	8.50	29.2	1.85	7.8	2.26	7.2	0.92	2.9	1.01	0.74
	¾	27.3	8.03	27.8	1.86	7.4	2.24	6.9	0.93	2.7	0.99	0.74
	⅝	25.7	7.55	26.4	1.87	7.0	2.22	6.6	0.93	2.6	0.97	0.75
	½	24.0	7.06	24.9	1.88	6.6	2.20	6.2	0.94	2.4	0.95	0.75
	⅜	22.4	6.56	23.3	1.89	6.1	2.18	5.8	0.94	2.3	0.93	0.75
	⅓	20.6	6.06	21.7	1.89	5.6	2.15	5.5	0.95	2.1	0.90	0.75
	¼	18.9	5.55	20.1	1.90	5.2	2.13	5.1	0.96	1.9	0.88	0.75
	⅓	17.1	5.03	18.4	1.91	4.7	2.11	4.7	0.96	1.8	0.86	0.75
	½	15.3	4.50	16.6	1.92	4.2	2.08	4.3	0.97	1.6	0.83	0.76
	⅝	13.5	3.97	14.8	1.93	3.7	2.06	3.8	0.98	1.4	0.81	0.76
	¾	11.7	3.42	12.9	1.94	3.3	2.04	3.3	0.99	1.2	0.79	0.77
	⅞	9.8	2.87	10.9	1.95	2.7	2.01	2.9	1.00	1.0	0.76	0.77
5 x 4	¾	24.2	7.11	16.4	1.52	5.0	1.71	9.2	1.14	3.3	1.21	0.84
	⅝	22.7	6.65	15.5	1.53	4.7	1.68	8.7	1.15	3.1	1.18	0.84
	½	21.1	6.19	14.6	1.54	4.4	1.66	8.2	1.15	2.9	1.16	0.84
	⅜	19.5	5.72	13.6	1.54	4.1	1.64	7.7	1.16	2.7	1.14	0.84
	⅓	17.8	5.23	12.6	1.55	3.7	1.62	7.1	1.17	2.5	1.12	0.84
	¼	16.2	4.75	11.6	1.56	3.4	1.60	6.6	1.18	2.3	1.10	0.85
	⅓	14.5	4.25	10.5	1.57	3.1	1.57	6.0	1.18	2.0	1.07	0.85
	½	12.8	3.75	9.3	1.58	2.7	1.55	5.3	1.19	1.8	1.05	0.85
5 x 3½	¾	22.7	6.67	15.7	1.53	4.9	1.79	6.2	0.96	2.5	1.04	0.75
	⅝	21.3	6.25	14.8	1.54	4.6	1.77	5.9	0.97	2.4	1.02	0.75
	½	19.8	5.81	13.9	1.55	4.3	1.75	5.6	0.98	2.2	1.00	0.75
	⅜	18.3	5.37	13.0	1.56	4.0	1.72	5.2	0.98	2.1	0.97	0.75
	⅓	16.8	4.92	12.0	1.56	3.7	1.70	4.8	0.99	1.9	0.95	0.75
	¼	15.2	4.47	11.0	1.57	3.3	1.68	4.4	1.00	1.7	0.93	0.75
	⅓	13.6	4.00	10.0	1.58	3.0	1.66	4.0	1.01	1.6	0.91	0.75
	½	12.0	3.53	8.9	1.59	2.6	1.63	3.6	1.01	1.4	0.88	0.76
5 x 3	¾	10.4	3.05	7.8	1.60	2.3	1.61	3.2	1.02	1.2	0.86	0.76
	⅝	8.7	2.56	6.6	1.61	1.9	1.59	2.7	1.03	1.0	0.84	0.76
	½	19.9	5.84	14.0	1.55	4.5	1.86	3.7	0.80	1.7	0.86	0.64
	⅜	18.5	5.44	13.2	1.55	4.2	1.84	3.5	0.80	1.6	0.84	0.64
	⅓	17.1	5.03	12.3	1.56	3.9	1.82	3.3	0.81	1.5	0.82	0.64
	¼	15.7	4.61	11.4	1.57	3.5	1.80	3.1	0.81	1.4	0.80	0.64
	⅓	14.3	4.18	10.4	1.58	3.2	1.77	2.8	0.82	1.3	0.77	0.65
	½	12.8	3.75	9.5	1.59	2.9	1.75	2.6	0.83	1.1	0.75	0.65
3½ x 2½	¾	11.3	3.31	8.4	1.60	2.6	1.73	2.3	0.84	1.0	0.73	0.65
	⅝	9.8	2.86	7.4	1.61	2.2	1.70	2.0	0.84	0.89	0.70	0.65
	½	8.2	2.40	6.3	1.61	1.9	1.68	1.8	0.85	0.75	0.68	0.66



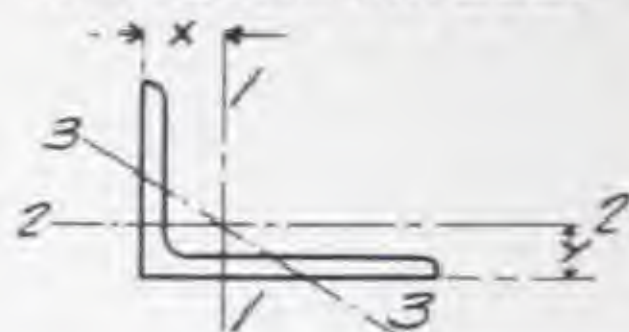
### DIMENSIONS, WEIGHTS AND ELEMENTS OF UNEQUAL ANGLES



Size	Thick- ness	Wt. per Foot	Area of Sec- tion	Axis 1-1				Axis 2-2				Axis 3-3	
				I	r	S	x	I	r	S	y	r <sub>min.</sub>	
In.	In.	Lbs.	In. <sup>2</sup>	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In.	In.
4½ x 3	¾	17.3	5.06	9.7	1.39	3.4	1.63	3.4	0.82	1.6	0.88	0.64	
	11/16	16.0	4.68	9.1	1.39	3.1	1.60	3.2	0.83	1.5	0.85	0.64	
	5/8	14.7	4.30	8.4	1.40	2.9	1.58	3.0	0.83	1.4	0.83	0.64	
	9/16	13.3	3.90	7.8	1.41	2.6	1.56	2.8	0.85	1.3	0.81	0.64	
	1/2	11.9	3.50	7.0	1.42	2.4	1.54	2.5	0.95	1.1	0.79	0.65	
	7/16	10.6	3.09	6.3	1.43	2.1	1.51	2.3	0.85	1.0	0.76	0.65	
	3/8	9.1	2.67	5.5	1.44	1.8	1.49	2.0	0.86	0.88	0.74	0.66	
	5/16	7.7	2.25	4.7	1.44	1.5	1.47	1.7	0.87	0.75	0.72	0.66	
4 x 3½	¾	17.3	5.06	7.3	1.20	2.8	1.34	5.2	1.01	2.1	1.09	0.72	
	11/16	16.0	4.68	6.9	1.21	2.6	1.32	4.9	1.02	2.0	1.07	0.72	
	5/8	14.7	4.30	6.4	1.22	2.4	1.29	4.5	1.03	1.8	1.04	0.72	
	9/16	13.3	3.90	5.9	1.23	2.1	1.27	4.2	1.03	1.7	1.02	0.72	
	1/2	11.9	3.50	5.3	1.23	1.9	1.25	3.8	1.04	1.5	1.00	0.72	
	7/16	10.6	3.09	4.8	1.24	1.7	1.23	3.4	1.05	1.3	0.98	0.72	
	3/8	9.1	2.67	4.2	1.25	1.5	1.21	3.0	1.06	1.2	0.96	0.73	
	5/16	7.7	2.25	3.6	1.26	1.3	1.18	2.6	1.07	1.0	0.93	0.73	
4 x 3	¾	16.0	4.69	6.9	1.22	2.7	1.42	3.3	0.84	1.6	0.92	0.64	
	11/16	14.8	4.34	6.5	1.22	2.5	1.39	3.1	0.84	1.5	0.89	0.64	
	5/8	13.6	3.98	6.0	1.23	2.3	1.37	2.9	0.85	1.4	0.87	0.64	
	9/16	12.4	3.62	5.6	1.24	2.1	1.35	2.7	0.86	1.2	0.85	0.64	
	1/2	11.1	3.25	5.0	1.25	1.9	1.33	2.4	0.86	1.1	0.83	0.64	
	7/16	9.8	2.87	4.5	1.25	1.7	1.30	2.2	0.87	1.0	0.80	0.64	
	3/8	8.5	2.48	4.0	1.26	1.5	1.28	1.9	0.88	0.87	0.78	0.64	
	5/16	7.2	2.09	3.4	1.27	1.2	1.26	1.7	0.89	0.74	0.76	0.65	
3½ x 3	¾	14.7	4.31	4.7	1.04	2.1	1.21	3.1	0.85	1.5	0.96	0.62	
	11/16	13.6	4.00	4.4	1.05	1.9	1.19	3.0	0.86	1.4	0.94	0.62	
	5/8	12.5	3.67	4.1	1.06	1.8	1.17	2.8	0.87	1.3	0.92	0.62	
	9/16	11.4	3.34	3.8	1.07	1.6	1.15	2.5	0.87	1.2	0.90	0.62	
	1/2	10.2	3.00	3.5	1.07	1.5	1.13	2.3	0.88	1.1	0.88	0.62	
	7/16	9.1	2.65	3.1	1.08	1.3	1.10	2.1	0.89	0.98	0.85	0.62	
	3/8	7.9	2.30	2.7	1.09	1.1	1.08	1.8	0.90	0.85	0.83	0.62	
	5/16	6.6	1.93	2.3	1.10	0.96	1.06	1.6	0.90	0.72	0.81	0.63	
3½ x 2½	¾	11.5	3.36	3.8	1.07	1.7	1.25	1.6	0.69	0.92	0.75	0.53	
	11/16	10.4	3.06	3.6	1.08	1.6	1.23	1.5	0.70	0.84	0.73	0.53	
	1/2	9.4	2.75	3.2	1.09	1.4	1.20	1.4	0.70	0.76	0.70	0.53	
	7/16	8.3	2.43	2.9	1.09	1.3	1.18	1.2	0.71	0.68	0.68	0.54	
	3/8	7.2	2.11	2.6	1.10	1.1	1.16	1.1	0.72	0.59	0.66	0.54	
	5/16	6.1	1.78	2.2	1.11	0.93	1.14	0.94	0.73	0.50	0.64	0.54	
	1/4	4.9	1.44	1.8	1.12	0.75	1.11	0.78	0.74	0.41	0.61	0.54	



# DIMENSIONS, WEIGHTS AND ELEMENTS OF UNEQUAL ANGLES

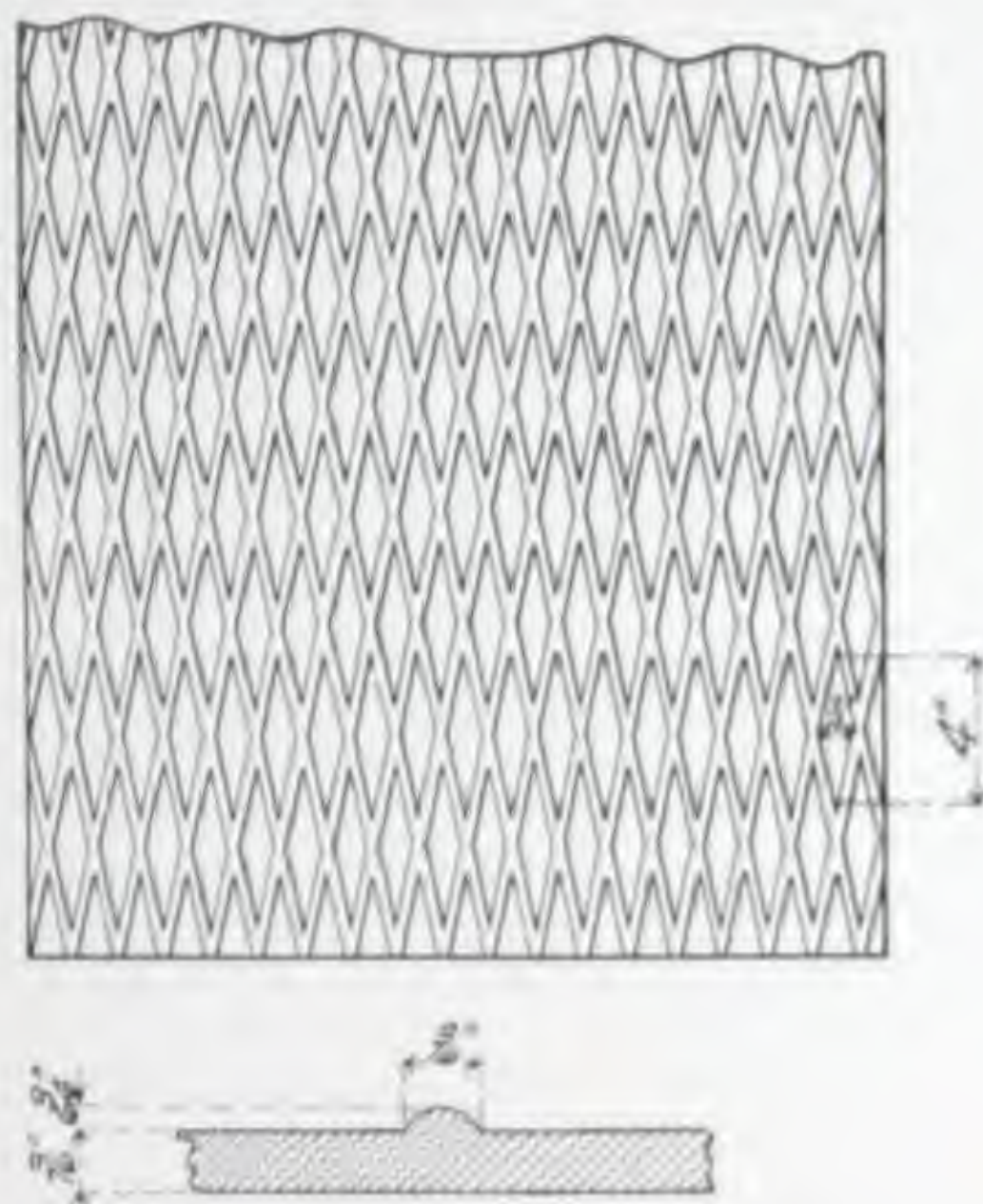


Size	Thick- ness	Wt. per foot	Area of Sec- tion	Axis 1-1				Axis 2-2				Axis 3-3
				I	r	S	x	I	r	S	y	r <sub>min.</sub>
In.	In.	Lbs.	In.	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In. <sup>4</sup>	In.	In. <sup>3</sup>	In.	In.
3 x 2½	½	8.5	2.50	2.1	0.91	1.0	1.00	1.3	0.72	0.74	0.75	0.52
	⅞	7.6	2.21	1.9	0.92	0.93	0.98	1.2	0.73	0.66	0.73	0.52
	⅝	6.6	1.92	1.7	0.93	0.81	0.96	1.0	0.74	0.58	0.71	0.52
	⅜	5.6	1.62	1.4	0.94	0.69	0.93	0.90	0.74	0.49	0.68	0.53
	¼	4.5	1.31	1.2	0.95	0.56	0.91	0.74	0.75	0.40	0.66	0.53
3 x 2	½	7.7	2.25	1.9	0.92	1.0	1.08	0.67	0.55	0.47	0.58	0.43
	⅞	6.8	2.00	1.7	0.93	0.89	1.06	0.61	0.55	0.42	0.56	0.43
	⅝	5.9	1.73	1.5	0.94	0.78	1.04	0.54	0.56	0.37	0.54	0.43
	⅜	5.0	1.47	1.3	0.95	0.66	1.02	0.47	0.57	0.32	0.52	0.43
	¼	4.1	1.19	1.1	0.95	0.54	0.99	0.39	0.57	0.25	0.49	0.43
2½ x 2	½	6.8	2.00	1.1	0.75	0.70	0.88	0.64	0.56	0.46	0.63	0.42
	⅞	6.1	1.78	1.0	0.76	0.62	0.85	0.58	0.57	0.41	0.60	0.42
	⅝	5.3	1.55	0.91	0.77	0.55	0.83	0.51	0.58	0.36	0.58	0.42
	⅜	4.5	1.31	0.79	0.78	0.47	0.81	0.45	0.58	0.31	0.56	0.42
	¼	3.62	1.06	0.65	0.78	0.38	0.79	0.37	0.59	0.25	0.54	0.42
	⅜	2.75	0.81	0.51	0.79	0.29	0.76	0.29	0.60	0.20	0.51	0.43
	⅝	1.86	0.55	0.35	0.80	0.20	0.74	0.20	0.61	0.13	0.49	0.43
2½ x 1½	⅝	3.92	1.15	0.71	0.79	0.44	0.90	0.19	0.41	0.17	0.40	0.32
	⅜	3.19	0.94	0.59	0.79	0.36	0.88	0.16	0.41	0.14	0.38	0.32
	¼	2.44	0.72	0.46	0.80	0.28	0.85	0.13	0.42	0.11	0.35	0.33
2¼ x 1½	⅞	5.0	1.45	0.68	0.69	0.48	0.83	0.24	0.41	0.23	0.46	0.32
	⅝	4.4	1.27	0.61	0.69	0.42	0.81	0.21	0.41	0.20	0.44	0.32
	⅜	3.66	1.07	0.53	0.70	0.36	0.79	0.19	0.42	0.17	0.42	0.32
	¼	2.98	0.88	0.44	0.71	0.30	0.77	0.16	0.42	0.14	0.39	0.32
	⅝	2.28	0.67	0.34	0.72	0.23	0.75	0.12	0.43	0.11	0.37	0.33
2 x 1½	⅝	3.99	1.17	0.43	0.61	0.34	0.71	0.21	0.42	0.20	0.46	0.32
	⅜	3.39	1.00	0.38	0.62	0.29	0.69	0.18	0.42	0.17	0.44	0.32
	¼	2.77	0.81	0.32	0.62	0.24	0.66	0.15	0.43	0.14	0.41	0.32
	⅝	2.12	0.62	0.25	0.63	0.18	0.64	0.12	0.44	0.11	0.39	0.32
	⅜	1.44	0.42	0.17	0.64	0.13	0.62	0.09	0.45	0.08	0.37	0.33
2 x 1¼	¼	2.55	0.75	0.30	0.63	0.23	0.71	0.09	0.34	0.10	0.33	0.27
	⅝	1.96	0.57	0.23	0.64	0.18	0.69	0.07	0.35	0.08	0.31	0.27
1½ x 1¼	¼	2.34	0.69	0.20	0.54	0.18	0.60	0.09	0.35	0.10	0.35	0.27
	⅝	1.80	0.53	0.16	0.55	0.14	0.58	0.07	0.36	0.08	0.33	0.27
	⅜	1.23	0.36	0.11	0.56	0.09	0.56	0.05	0.37	0.05	0.31	0.27
1½ x 1¼	⅝	2.59	0.76	0.16	0.45	0.16	0.52	0.10	0.35	0.11	0.40	0.26
	⅜	2.13	0.63	0.13	0.46	0.13	0.50	0.08	0.36	0.09	0.38	0.26
	¼	1.64	0.48	0.10	0.46	0.10	0.48	0.07	0.37	0.07	0.35	0.26



## CHECKERED PLATES

These plates are for use in boiler and engine rooms, breweries, for stairways, fire escapes, gutter plates, car platforms, sidewalks, deck plates on ships and every place where a cast iron plate is now used. They are made of the best open hearth steel, and are much stronger than cast iron floor plates, cheaper, and fifty per cent lighter.



No. 6.—Checkered Plate, showing Section at Rib

## WIDTHS AND MAXIMUM LENGTHS ROLLED

Thickness, Inches.	Width and Length, Inches			Weight per Square Foot, Pounds
	6 to 31 1/2	12 to 48	48 1/2 to 60	
1/2	120	240	240	21.4
5/8	120	240	240	18.9
3/4	120	240	240	16.3
7/8	120	240	240	13.8
1	120	240	240	11.2
1 1/8	120	180		8.7

The sizes carried in stock are 3/8-inch, 1/2-inch and 3/4-inch. Others are special.



**RECTANGULAR UNIVERSAL PLATES—Carbon Steel**  
**UNIVERSAL MILL PLATES, ONE-FOURTH INCH AND OVER,**  
**EXTREME SIZES**

Thick- ness, Inches	Weight, Lbs. per Sq. Ft.	Widths and Lengths in Inches										
		48-46	45-41	40-36	35-31	30-26	25-20	19-17	16-15	14-12	11	10-6 1/8
1/4	10.20						1020	1020	1020	1020	540	540
3/16	12.75	1020	1020	1140	1260	1320	1320	1080	1080	1080	600	600
1/8	15.30	1200	1200	1320	1380	1380	1380	1080	1080	1080	900	840
7/16	17.85	1320	1320	1380	1380	1380	1380	1080	1080	1080	900	840
1/2	20.40	1380	1380	1380	1380	1380	1380	1080	1080	1080	1020	840
5/8	22.95	1380	1380	1380	1380	1380	1380	1080	1080	1080	1020	840
3/4	25.50	1380	1380	1380	1380	1380	1380	1080	1080	1080	1020	840
7/8	30.60	1353	1357	1363	1372	1380	1380	1080	1080	1080	900	840
1	35.70	1160	1163	1169	1177	1188	1203	1080	1080	1080	900	840
	40.80	1015	1018	1023	1030	1039	1052	1080	1080	1080	900	840
1 1/8	45.90	903	905	910	916	924	936	1080	1080	1080	840	840
1 1/4	51.00	812	814	818	824	832	842	1071	1080	1080	840	840
1 3/8	56.10	738	740	744	749	756	766	973	1080	1080	840	840
1 1/2	61.20	677	679	682	687	693	702	892	1059	1080	840	840
1 5/8	66.30	625	626	629	634	640	648	823	978	1080	840	840
1 3/4	71.40	580	581	584	588	594	601	765	908	1038	720	720
1 7/8	76.50	541	543	545	549	554	561	714	847	968	660	720
2	81.60	507	509	511	515	519	526	669	794	907	600	720

**RECTANGULAR AND CIRCULAR PLATES—Carbon Steel**  
**SHEARED PLATES, THREE-SIXTEENTH INCH, EXTREME SIZES**

Thick- ness, Inches	Weight, Lbs. per Sq. Ft.	Widths and Lengths in Inches										Diam., In.
		90	84	78	72	70	68	66	64	60	54-24	
3/16	7.65	270	320	345	375	390	400	420	450	470	480	90



**RECTANGULAR AND CIRCULAR PLATES—Carbon Steel**  
**SHEARED PLATES, ONE-FOURTH INCH AND OVER,**  
**EXTREME SIZES**

Thick- ness, Inches	Weight Lbs. per Sq. Ft.	Widths and Lengths in Inches										Diag. In.
		128	120	120	114	108	102	96	90	84	78	
$\frac{1}{4}$	10.20				175	230	280	300	330	375	400	115
$\frac{3}{8}$	12.75			240	270	320	360	380	420	440	460	120
$\frac{1}{2}$	15.30	220	240	270	320	365	380	410	450	500	520	130
$\frac{3}{4}$	17.85	240	270	300	360	370	410	430	460	510	520	130
$\frac{7}{8}$	20.40	260	270	320	365	400	450	480	510	520	580	130
$1\frac{1}{8}$	22.95	260	270	320	375	420	470	500	530	570	600	130
$1\frac{1}{4}$	25.50	260	300	350	390	450	500	520	540	600	620	130
$1\frac{1}{2}$	28.05	260	300	360	420	450	500	520	540	600	620	130
$1\frac{3}{4}$	30.60	260	300	360	400	450	480	520	540	600	620	130
$1\frac{7}{8}$	33.15	260	300	340	385	440	480	510	530	600	620	130
$2\frac{1}{8}$	35.70	260	300	330	375	440	480	510	530	600	620	130
1	40.80	250	300	300	340	440	480	500	520	580	600	130
$1\frac{1}{8}$	45.90	250	300	300	330	410	440	450	500	520	580	130
$1\frac{1}{4}$	51.00	240	270	300	310	380	400	420	480	500	520	130
$1\frac{1}{2}$	56.10	230	230	260	280	330	320	340	420	440	480	130
$1\frac{3}{4}$	61.20	200	200	220	240	280	270	300	380	380	410	130
2	66.30	180	180	190	210	240	240	260	320	320	360	130
$2\frac{1}{4}$	71.40	150	160	170	190	210	210	230	280	280	320	130

Thick- ness, Inches	Weight Lbs. per Sq. Ft.	Widths and Lengths in Inches										Diag. In.
		72	66	60	54	50	48	42	36	30	24	
$\frac{1}{4}$	10.20	430	475	525	530	580	520	520	520	520	520	115
$\frac{3}{8}$	12.75	480	500	560	530	575	575	520	520	520	520	120
$\frac{1}{2}$	15.30	600	600	620	620	620	620	600	580	600	600	130
$\frac{3}{4}$	17.85	600	620	620	640	640	640	600	580	600	600	130
$\frac{7}{8}$	20.40	610	620	620	640	640	640	600	580	620	600	130
$1\frac{1}{8}$	22.95	620	640	640	640	640	640	600	580	620	600	130
$1\frac{1}{4}$	25.50	620	640	640	640	640	640	600	580	600	600	130
$1\frac{1}{2}$	28.05	620	640	640	640	640	640	600	580	600	580	130
$1\frac{3}{4}$	30.60	620	640	640	640	640	640	600	580	600	580	130
$1\frac{7}{8}$	33.15	620	640	640	640	640	640	600	580	570	550	130
$2\frac{1}{8}$	35.70	620	640	640	640	640	640	600	580	550	520	130
1	40.80	600	630	630	640	640	640	580	580	520	520	130
$1\frac{1}{8}$	45.90	580	620	620	640	640	640	580	580	520	500	130
$1\frac{1}{4}$	51.00	550	600	600	600	600	600	580	580	520	450	130
$1\frac{1}{2}$	56.10	520	600	600	600	600	600	540	540	475	420	130
$1\frac{3}{4}$	61.20	450	490	520	530	550	550	540	540	420	380	130
2	66.30	400	440	480	500	500	500	500	500	400	350	130
$2\frac{1}{4}$	71.40	350	380	420	450	450	450	430	430	305	280	130



# WEIGHTS OF FLAT ROLLED STEEL

## POUNDS PER LINEAL FOOT

Width, Inches	Thickness, Inches															
	1/8	3/16	1/4	5/16	3/8	7/16	1/2	5/8	3/4	7/8	1	1 1/8	1 1/4	1 1/2	1 3/4	2
1/8	0.53	1.06	1.59	2.13	2.67	3.20	3.74	4.28	4.81	5.35	5.88	6.42	6.95	7.49	8.02	8.56
1/4	1.06	2.13	3.19	4.25	5.31	6.38	7.44	8.50	9.56	10.62	11.68	12.74	13.80	14.86	15.92	16.98
3/8	1.59	3.19	4.78	6.38	7.97	9.56	11.15	12.74	14.33	15.92	17.51	19.10	20.69	22.28	23.87	25.46
1/2	2.13	4.25	6.38	8.50	10.62	12.74	14.86	16.98	19.10	21.22	23.34	25.46	27.58	29.69	31.81	33.93
5/8	2.67	5.31	7.97	10.62	13.27	15.92	18.57	21.22	23.87	26.52	29.17	31.81	34.46	37.11	39.76	42.41
3/4	3.20	6.38	9.56	12.74	15.92	19.10	22.28	25.46	28.64	31.81	34.99	38.17	41.35	44.53	47.71	50.89
7/8	3.74	7.44	11.15	14.86	18.57	22.28	25.99	29.70	33.41	37.11	40.82	44.53	48.24	51.95	55.66	59.37
1	4.28	8.50	12.74	16.98	21.22	25.46	29.69	33.93	38.17	42.41	46.65	50.89	55.13	59.37	63.61	67.85
1 1/8	4.81	9.56	14.33	19.10	23.34	27.58	31.81	36.05	40.28	44.53	48.77	52.99	57.23	61.47	65.71	69.95
1 1/4	5.35	10.62	15.92	21.22	26.52	31.81	36.05	40.28	44.53	48.77	52.99	57.23	61.47	65.71	69.95	74.19
1 1/2	5.88	11.68	17.51	23.34	29.17	34.46	39.76	44.53	49.30	54.07	58.84	63.61	68.38	73.15	77.92	82.69
1 3/4	6.42	12.74	19.10	25.46	31.81	37.11	42.41	47.71	52.99	58.28	63.57	68.86	74.15	79.44	84.73	89.92
2	6.95	13.80	20.69	27.58	33.93	39.76	45.59	51.42	57.25	63.08	68.91	74.74	80.57	86.40	92.23	98.06
2 1/4	7.49	14.86	22.28	29.69	36.05	41.95	47.78	53.61	59.44	65.27	71.10	76.93	82.76	88.59	94.42	100.25
2 1/2	8.02	15.92	23.87	31.81	38.17	44.07	49.90	55.73	61.56	67.39	73.22	79.05	84.88	90.71	96.54	102.37
2 3/4	8.56	16.98	25.46	33.93	40.28	46.17	52.00	57.83	63.66	69.49	75.32	81.15	86.98	92.81	98.64	104.47
3	9.09	18.04	27.05	36.05	42.41	48.24	54.07	59.90	65.73	71.56	77.39	83.22	89.05	94.88	100.71	106.54
3 1/4	9.63	19.10	28.64	38.17	44.53	50.36	56.19	62.02	67.85	73.68	79.51	85.34	91.17	96.99	102.82	108.65
3 1/2	10.17	20.16	30.23	40.28	46.65	52.48	58.31	64.14	69.97	75.80	81.63	87.46	93.29	99.12	104.95	110.78
3 3/4	10.71	21.22	31.81	42.41	48.77	54.60	60.43	66.26	72.09	77.92	83.75	89.58	95.41	101.24	107.07	112.90
4	11.25	22.28	33.41	44.53	50.89	56.72	62.55	68.38	74.21	80.04	85.87	91.70	97.53	103.36	109.19	115.02
4 1/4	11.79	23.34	34.99	46.65	52.99	58.82	64.65	70.48	76.31	82.14	87.97	93.80	99.63	105.46	111.29	117.12
4 1/2	12.33	24.40	36.57	48.77	55.13	60.96	66.79	72.62	78.45	84.28	90.11	95.94	101.77	107.60	113.43	119.26
4 3/4	12.87	25.46	38.15	50.89	57.25	63.08	68.91	74.74	80.57	86.40	92.23	98.06	103.89	109.72	115.55	121.38
5	13.41	26.52	39.76	52.99	59.44	65.27	71.10	76.93	82.76	88.59	94.42	100.25	106.08	111.91	117.74	123.57
5 1/4	13.95	27.58	41.35	55.13	61.56	67.39	73.22	79.05	84.88	90.71	96.54	102.37	108.20	114.03	119.86	125.69
5 1/2	14.49	28.64	42.93	57.25	63.61	69.49	75.32	81.15	86.98	92.81	98.64	104.47	110.30	116.13	121.96	127.79
5 3/4	15.03	29.69	44.53	59.44	65.73	71.56	77.39	83.22	89.05	94.88	100.71	106.54	112.37	118.20	124.03	129.86
6	15.57	30.75	46.11	61.56	67.85	73.68	79.51	85.34	91.17	96.99	102.82	108.65	114.48	120.31	126.14	131.97
6 1/4	16.11	31.81	47.70	63.61	69.90	75.73	81.56	87.39	93.22	99.05	104.88	110.71	116.54	122.37	128.20	134.03
6 1/2	16.65	32.87	49.28	65.73	71.95	77.78	83.61	89.44	95.27	101.10	106.93	112.76	118.59	124.42	130.25	136.08
6 3/4	17.19	33.93	50.87	67.85	74.07	79.90	85.73	91.56	97.39	103.22	109.05	114.88	120.71	126.54	132.37	138.20
7	17.73	34.99	52.45	69.90	76.19	82.02	87.85	93.68	99.51	105.34	111.17	117.00	122.83	128.66	134.49	140.32
7 1/4	18.27	36.05	54.03	71.95	78.21	84.04	89.87	95.70	101.53	107.36	113.19	119.02	124.85	130.68	136.51	142.34
7 1/2	18.81	37.11	55.61	74.07	80.33	86.16	91.99	97.82	103.65	109.48	115.31	121.14	126.97	132.80	138.63	144.46
7 3/4	19.35	38.17	57.20	76.19	82.45	88.28	94.11	99.94	105.77	111.60	117.43	123.26	129.09	134.92	140.75	146.58
8	19.89	39.23	58.78	78.21	84.57	90.40	96.23	102.06	107.89	113.72	119.55	125.38	131.21	137.04	142.87	148.70
8 1/4	20.43	40.28	60.37	80.33	86.69	92.52	98.35	104.18	110.01	115.84	121.67	127.50	133.33	139.16	144.99	150.82
8 1/2	20.97	41.35	61.95	82.45	88.81	94.64	100.47	106.30	112.13	117.96	123.79	129.62	135.45	141.28	147.11	152.94
8 3/4	21.51	42.41	63.53	84.57	90.93	96.76	102.59	108.42	114.25	120.08	125.91	131.74	137.57	143.40	149.23	155.06
9	22.05	43.47	65.11	86.69	93.05	98.88	104.71	110.54	116.37	122.20	128.03	133.86	139.69	145.52	151.35	157.18
9 1/4	22.59	44.53	66.69	88.81	95.17	101.00	106.83	112.66	118.49	124.32	130.15	135.98	141.81	147.64	153.47	159.30
9 1/2	23.13	45.59	68.27	90.93	97.29	103.12	108.95	114.78	120.61	126.44	132.27	138.10	143.93	149.76	155.59	161.42
9 3/4	23.67	46.65	69.85	93.05	99.41	105.24	111.07	116.90	122.73	128.56	134.39	140.22	146.05	151.88	157.71	163.54
10	24.21	47.71	71.43	95.17	101.53	107.36	113.19	119.02	124.85	130.68	136.51	142.34	148.17	153.99	159.82	165.66
10 1/4	24.75	48.77	73.01	97.29	103.65	109.48	115.31	121.14	126.97	132.80	138.63	144.46	150.29	156.12	161.95	167.78
10 1/2	25.29	49.83	74.59	99.41	105.77	111.60	117.43	123.26	129.09	134.92	140.75	146.58	152.41	158.24	164.07	169.90
10 3/4	25.83	50.89	76.17	101.53	107.89	113.72	119.55	125.38	131.21	137.04	142.87	148.70	154.53	160.36	166.19	172.02
11	26.37	51.95	77.75	103.65	109.90	115.73	121.56	127.39	133.22	139.05	144.88	150.71	156.54	162.37	168.20	174.03
11 1/4	26.91	53.01	79.33	105.77	112.02	117.85	123.68	129.51	135.34	141.17	147.00	152.83	158.66	164.49	170.32	176.15
11 1/2	27.45	54.07	80.91	107.89	114.14	120.00	125.83	131.66	137.49	143.32	149.15	154.98	160.81	166.64	172.47	178.30
11 3/4	27.99	55.13	82.49	110.02	116.26	122.09	127.92	133.75	139.58	145.41	151.24	157.07	162.90	168.73	174.56	180.39
12	28.53	56.19	84.07	112.14	118.38	124.21	130.04	135.87	141.70	147.53	153.36	159.19	165.02	170.85	176.68	182.51



# WEIGHTS OF FLAT ROLLED STEEL

## POUNDS PER LINEAL FOOT

Width, Inches	Thickness, Inches															
	1/8	3/16	1/4	5/16	3/8	7/16	1/2	9/16	5/8	3/4	7/8	1	1 1/8	1 1/4	1 3/8	1 1/2
12 1/2	2.66	3.31	3.97	4.63	5.29	5.95	6.61	7.27	7.93	8.59	9.25	9.91	10.57	11.23	11.89	12.55
13	2.76	3.42	4.08	4.74	5.40	6.06	6.72	7.38	8.04	8.70	9.36	10.02	10.68	11.34	12.00	12.66
13 1/2	2.87	3.53	4.19	4.85	5.51	6.17	6.83	7.49	8.15	8.81	9.47	10.13	10.79	11.45	12.11	12.77
14	2.98	3.64	4.30	4.96	5.62	6.28	6.94	7.60	8.26	8.92	9.58	10.24	10.90	11.56	12.22	12.88
14 1/2	3.08	3.74	4.40	5.06	5.72	6.38	7.04	7.70	8.36	9.02	9.68	10.34	11.00	11.66	12.32	12.98
15	3.19	3.85	4.51	5.17	5.83	6.49	7.15	7.81	8.47	9.13	9.79	10.45	11.11	11.77	12.43	13.09
15 1/2	3.29	3.95	4.61	5.27	5.93	6.59	7.25	7.91	8.57	9.23	9.89	10.55	11.21	11.87	12.53	13.19
16	3.40	4.06	4.72	5.38	6.04	6.70	7.36	8.02	8.68	9.34	10.00	10.66	11.32	11.98	12.64	13.30
16 1/2	3.51	4.17	4.83	5.49	6.15	6.81	7.47	8.13	8.79	9.45	10.11	10.77	11.43	12.09	12.75	13.41
17	3.61	4.27	4.93	5.59	6.25	6.91	7.57	8.23	8.89	9.55	10.21	10.87	11.53	12.19	12.85	13.51
17 1/2	3.72	4.38	5.04	5.70	6.36	7.02	7.68	8.34	9.00	9.66	10.32	10.98	11.64	12.30	12.96	13.62
18	3.83	4.49	5.15	5.81	6.47	7.13	7.79	8.45	9.11	9.77	10.43	11.09	11.75	12.41	13.07	13.73
18 1/2	3.93	4.59	5.25	5.91	6.57	7.23	7.89	8.55	9.21	9.87	10.53	11.19	11.85	12.51	13.17	13.83
19	4.04	4.70	5.36	6.02	6.68	7.34	8.00	8.66	9.32	9.98	10.64	11.30	11.96	12.62	13.28	13.94
19 1/2	4.14	4.80	5.46	6.12	6.78	7.44	8.10	8.76	9.42	10.08	10.74	11.40	12.06	12.72	13.38	14.04
20	4.25	4.91	5.57	6.23	6.89	7.55	8.21	8.87	9.53	10.19	10.85	11.51	12.17	12.83	13.49	14.15
20 1/2	4.36	5.02	5.68	6.34	7.00	7.66	8.32	8.98	9.64	10.30	10.96	11.62	12.28	12.94	13.60	14.26
21	4.46	5.12	5.78	6.44	7.10	7.76	8.42	9.08	9.74	10.40	11.06	11.72	12.38	13.04	13.70	14.36
21 1/2	4.57	5.23	5.89	6.55	7.21	7.87	8.53	9.19	9.85	10.51	11.17	11.83	12.49	13.15	13.81	14.47
22	4.68	5.34	6.00	6.66	7.32	7.98	8.64	9.30	9.96	10.62	11.28	11.94	12.60	13.26	13.92	14.58
22 1/2	4.78	5.44	6.10	6.76	7.42	8.08	8.74	9.40	10.06	10.72	11.38	12.04	12.70	13.36	14.02	14.68
23	4.89	5.55	6.21	6.87	7.53	8.19	8.85	9.51	10.17	10.83	11.49	12.15	12.81	13.47	14.13	14.79
23 1/2	4.99	5.65	6.31	6.97	7.63	8.29	8.95	9.61	10.27	10.93	11.59	12.25	12.91	13.57	14.23	14.89
24	5.10	5.76	6.42	7.08	7.74	8.40	9.06	9.72	10.38	11.04	11.70	12.36	13.02	13.68	14.34	15.00
25	5.21	5.87	6.53	7.19	7.85	8.51	9.17	9.83	10.49	11.15	11.81	12.47	13.13	13.79	14.45	15.11
26	5.32	5.98	6.64	7.30	7.96	8.62	9.28	9.94	10.60	11.26	11.92	12.58	13.24	13.90	14.56	15.22
27	5.43	6.09	6.75	7.41	8.07	8.73	9.39	10.05	10.71	11.37	12.03	12.69	13.35	14.01	14.67	15.33
28	5.54	6.20	6.86	7.52	8.18	8.84	9.50	10.16	10.82	11.48	12.14	12.80	13.46	14.12	14.78	15.44
29	5.65	6.31	6.97	7.63	8.29	8.95	9.61	10.27	10.93	11.59	12.25	12.91	13.57	14.23	14.89	15.55
30	5.76	6.42	7.08	7.74	8.40	9.06	9.72	10.38	11.04	11.70	12.36	13.02	13.68	14.34	15.00	15.66
31	5.87	6.53	7.19	7.85	8.51	9.17	9.83	10.49	11.15	11.81	12.47	13.13	13.79	14.45	15.11	15.77
32	5.98	6.64	7.30	7.96	8.62	9.28	9.94	10.60	11.26	11.92	12.58	13.24	13.90	14.56	15.22	15.88
33	6.09	6.75	7.41	8.07	8.73	9.39	10.05	10.71	11.37	12.03	12.69	13.35	14.01	14.67	15.33	15.99
34	6.20	6.86	7.52	8.18	8.84	9.50	10.16	10.82	11.48	12.14	12.80	13.46	14.12	14.78	15.44	16.10
35	6.31	6.97	7.63	8.29	8.95	9.61	10.27	10.93	11.59	12.25	12.91	13.57	14.23	14.89	15.55	16.21
36	6.42	7.08	7.74	8.40	9.06	9.72	10.38	11.04	11.70	12.36	13.02	13.68	14.34	15.00	15.66	16.32
37	6.53	7.19	7.85	8.51	9.17	9.83	10.49	11.15	11.81	12.47	13.13	13.79	14.45	15.11	15.77	16.43
38	6.64	7.30	7.96	8.62	9.28	9.94	10.60	11.26	11.92	12.58	13.24	13.90	14.56	15.22	15.88	16.54
39	6.75	7.41	8.07	8.73	9.39	10.05	10.71	11.37	12.03	12.69	13.35	14.01	14.67	15.33	15.99	16.65
40	6.86	7.52	8.18	8.84	9.50	10.16	10.82	11.48	12.14	12.80	13.46	14.12	14.78	15.44	16.10	16.76
41	6.97	7.63	8.29	8.95	9.61	10.27	10.93	11.59	12.25	12.91	13.57	14.23	14.89	15.55	16.21	16.87
42	7.08	7.74	8.40	9.06	9.72	10.38	11.04	11.70	12.36	13.02	13.68	14.34	15.00	15.66	16.32	16.98
43	7.19	7.85	8.51	9.17	9.83	10.49	11.15	11.81	12.47	13.13	13.79	14.45	15.11	15.77	16.43	17.09
44	7.30	7.96	8.62	9.28	9.94	10.60	11.26	11.92	12.58	13.24	13.90	14.56	15.22	15.88	16.54	17.20
45	7.41	8.07	8.73	9.39	10.05	10.71	11.37	12.03	12.69	13.35	14.01	14.67	15.33	15.99	16.65	17.31
46	7.52	8.18	8.84	9.50	10.16	10.82	11.48	12.14	12.80	13.46	14.12	14.78	15.44	16.10	16.76	17.42
47	7.63	8.29	8.95	9.61	10.27	10.93	11.59	12.25	12.91	13.57	14.23	14.89	15.55	16.21	16.87	17.53
48	7.74	8.40	9.06	9.72	10.38	11.04	11.70	12.36	13.02	13.68	14.34	15.00	15.66	16.32	16.98	17.64



# WEIGHTS OF FLAT ROLLED STEEL

## POUNDS PER LINEAL FOOT

Width, Inches	Thickness, Inches															
	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	$\frac{15}{16}$	1	1 1/8	1 1/4	1 1/2
49	10.4	20.8	31.2	41.7	52.1	62.5	72.9	83.3	93.7	104.1	114.5	125.0	135.4	145.8	156.2	166.6
50	10.6	21.3	31.9	42.5	53.1	63.8	74.4	85.0	95.6	106.3	116.9	127.5	138.1	148.8	159.4	170.0
51	10.8	21.7	32.5	43.4	54.2	65.0	75.9	86.7	97.5	108.4	119.2	130.1	140.9	151.7	162.6	173.4
52	11.1	22.1	33.2	44.2	55.3	66.3	77.4	88.4	99.5	110.5	121.6	132.6	143.7	154.7	165.8	176.8
53	11.3	22.5	33.8	45.1	56.3	67.6	78.8	90.1	101.4	112.6	123.9	135.2	146.4	157.7	168.9	180.2
54	11.5	23.0	34.4	45.9	57.4	68.9	80.3	91.8	103.3	114.8	126.3	137.7	149.2	160.7	172.1	183.6
55	11.7	23.4	35.1	46.8	58.4	70.1	81.8	93.5	105.2	116.9	128.6	140.3	151.9	163.6	175.3	187.0
56	11.9	23.8	35.7	47.6	59.5	71.4	83.3	95.2	107.1	119.0	130.9	142.8	154.7	166.6	178.5	190.4
57	12.1	24.2	36.3	48.5	60.6	72.7	84.8	96.9	109.0	121.1	133.2	145.4	157.5	169.6	181.7	193.8
58	12.3	24.7	37.0	49.3	61.6	74.0	86.3	98.6	110.9	123.3	135.6	147.9	160.2	172.6	184.9	197.2
59	12.5	25.1	37.6	50.2	62.7	75.2	87.8	100.3	112.8	125.4	137.9	150.5	163.0	175.5	188.1	200.6
60	12.8	25.5	38.3	51.0	63.8	76.5	89.3	102.0	114.8	127.5	140.3	153.0	165.8	178.5	191.3	204.0
61	13.0	25.9	38.9	51.9	64.8	77.8	90.7	103.7	116.7	129.6	142.6	155.6	168.5	181.5	194.4	207.4
62	13.2	26.4	39.5	52.7	65.9	79.1	92.2	105.4	118.6	131.8	144.9	158.1	171.3	184.5	197.6	210.8
63	13.4	26.8	40.2	53.6	66.9	80.3	93.7	107.1	120.5	133.9	147.3	160.7	174.0	187.4	200.8	214.2
64	13.6	27.2	40.8	54.4	68.0	81.6	95.2	108.8	122.4	136.0	149.6	163.2	176.8	190.4	204.0	217.6
65	13.8	27.6	41.4	55.3	69.1	82.9	96.7	110.5	124.3	138.1	151.9	165.8	179.6	193.4	207.2	221.0
66	14.0	28.1	42.1	56.1	70.1	84.2	98.2	112.2	126.2	140.3	154.3	168.3	182.3	196.4	210.4	224.4
67	14.2	28.5	42.7	57.0	71.2	85.4	99.7	113.9	128.1	142.4	156.6	170.9	185.1	199.3	213.6	227.8
68	14.5	28.9	43.4	57.8	72.3	86.7	101.2	115.6	130.1	144.5	159.0	173.4	187.9	202.3	216.8	231.2
69	14.7	29.3	44.0	58.7	73.3	88.0	102.6	117.3	132.0	146.6	161.3	176.0	190.6	205.3	219.9	234.6
70	14.9	29.8	44.6	59.5	74.4	89.3	104.1	119.0	133.9	148.8	163.6	178.5	193.4	208.3	223.1	238.0
71	15.1	30.2	45.3	60.4	75.4	90.5	105.6	120.7	135.8	150.9	166.0	181.1	196.1	211.2	226.3	241.4
72	15.3	30.6	45.9	61.2	76.5	91.8	107.1	122.4	137.7	153.0	168.3	183.6	198.9	214.2	229.5	244.8
73	15.5	31.0	46.5	62.1	77.6	93.1	108.6	124.1	139.6	155.1	170.6	186.2	201.7	217.2	232.7	248.3
74	15.7	31.5	47.2	62.9	78.6	94.4	110.1	125.8	141.5	157.3	173.0	188.7	204.4	220.2	235.9	251.6
75	15.9	31.9	47.8	63.8	79.7	95.6	111.6	127.5	143.4	159.4	175.3	191.3	207.2	223.1	239.1	255.0
76	16.2	32.3	48.5	64.6	80.8	96.9	113.1	129.2	145.4	161.5	177.7	193.8	210.0	226.1	242.3	258.4
77	16.4	32.7	49.1	65.5	81.8	98.2	114.5	130.9	147.3	163.6	180.0	196.4	212.7	229.1	245.4	261.8
78	16.6	33.2	49.7	66.3	82.9	99.5	116.0	132.6	149.2	165.8	182.3	198.9	215.5	232.1	248.6	265.2
79	16.8	33.6	50.4	67.2	83.9	100.7	117.5	134.3	151.1	167.9	184.7	201.5	218.2	235.0	251.8	268.6
80	17.0	34.0	51.0	68.0	85.0	102.0	119.0	136.0	153.0	170.0	187.0	204.0	221.0	238.0	255.0	272.0
81	17.2	34.4	51.6	68.9	86.1	103.3	120.5	137.7	154.9	172.1	189.3	206.6	223.8	241.0	258.2	275.4
82	17.4	34.8	52.3	69.7	87.1	104.6	122.0	139.4	156.8	174.3	191.7	209.1	226.5	244.0	261.4	278.8
83	17.6	35.3	52.9	70.6	88.2	105.8	123.5	141.1	158.7	176.4	194.0	211.7	229.3	246.9	264.6	282.2
84	17.9	35.7	53.6	71.4	89.3	107.1	125.0	142.8	160.7	178.5	196.4	214.2	232.1	249.9	267.8	285.6
85	18.1	36.1	54.2	72.3	90.3	108.4	126.4	144.5	162.6	180.6	198.7	216.8	234.8	252.9	270.9	289.0
86	18.3	36.6	54.8	73.1	91.4	109.7	127.9	146.2	164.5	182.8	201.0	219.3	237.6	255.9	274.1	292.4
87	18.5	37.0	55.5	74.0	92.4	110.9	129.4	147.9	166.4	184.9	203.4	221.9	240.3	258.8	277.3	295.8
88	18.7	37.4	56.1	74.8	93.5	112.2	130.9	149.6	168.3	187.0	205.7	224.4	243.1	261.8	280.5	299.2
89	18.9	37.8	56.7	75.7	94.6	113.5	132.4	151.3	170.2	189.1	208.0	227.0	245.9	264.8	283.7	302.6
90	19.1	38.3	57.4	76.5	95.6	114.8	133.9	153.0	172.1	191.3	210.4	229.5	248.6	267.8	286.9	306.0
91	19.3	38.7	58.0	77.4	96.7	116.0	135.4	154.7	174.0	193.4	212.7	232.1	241.4	270.7	290.1	309.4
92	19.5	39.1	58.7	78.2	97.8	117.3	136.9	156.4	176.0	195.5	215.1	234.6	254.2	273.7	293.3	312.8
93	19.8	39.5	59.3	79.1	98.8	118.6	138.3	158.1	177.9	197.6	217.4	237.2	256.9	276.7	296.4	316.2
94	20.0	40.0	59.9	79.9	99.9	119.9	139.8	159.8	179.8	199.8	219.7	239.7	259.7	279.7	299.6	319.6
95	20.2	40.4	60.6	80.8	100.9	121.1	141.3	161.3	181.7	201.9	222.1	242.3	262.4	282.6	302.8	323.0
96	20.4	40.8	61.2	81.6	102.0	122.4	142.8	163.2	183.6	204.4	224.4	244.8	265.2	285.6	306.0	326.4
97	20.6	41.2	61.8	82.5	103.1	123.7	144.3	164.9	185.5	206.1	226.7	247.4	268.0	288.6	309.6	329.8
98	20.8	41.7	62.5	83.3	104.1	125.0	145.8	166.6	187.4	208.3	229.1	249.9	270.7	291.6	312.8	333.2
99	21.0	42.1	63.1	84.2	105.2	126.2	147.3	168.3	189.3	210.4	231.4	252.5	273.7	294.5	315.6	336.6
100	21.3	42.5	63.8	85.0	106.3	127.5	148.8	170.0	191.3	212.7	233.8	255.0	276.3	297.5	318.8	340.0

Steel  
reasons  
suppliesWeight  
per  
Yard,  
Lbs60  
55  
50  
45  
40  
35  
30  
25  
20  
16  
14  
12  
10  
8



## A.S.C.E. RAILS AND LIGHT RAILS



Fig. 1—Cross-section of rail

Steel railway rails in all sizes and weights, new and relaying, available for reasonable delivery. Fish plates, bolting system, frogs, switches and switch stands supplied.

Weight lb/yd	Head inches	Head width inches	Weight lb/yd	Head inches	Head width inches	Weight lb/yd	Weight of One Rail from 100 ft		
							100 ft	100 ft	100 ft
30	4 1/2	4 1/2	25 1/2	3 1/2	3 1/2	24	4 1/2	4 1/2	4 1/2
32	4 3/4	4 3/4	27 1/2	3 3/4	3 3/4	26	4 3/4	4 3/4	4 3/4
34	4 7/8	4 7/8	29 1/2	3 7/8	3 7/8	28	4 7/8	4 7/8	4 7/8
36	5 1/8	5 1/8	31 1/2	4 1/8	4 1/8	30	5 1/8	5 1/8	5 1/8
38	5 3/8	5 3/8	33 1/2	4 3/8	4 3/8	32	5 3/8	5 3/8	5 3/8
40	5 1/2	5 1/2	35 1/2	4 1/2	4 1/2	34	5 1/2	5 1/2	5 1/2
42	5 5/8	5 5/8	37 1/2	4 5/8	4 5/8	36	5 5/8	5 5/8	5 5/8
44	5 7/8	5 7/8	39 1/2	4 7/8	4 7/8	38	5 7/8	5 7/8	5 7/8
46	6 1/8	6 1/8	41 1/2	5 1/8	5 1/8	40	6 1/8	6 1/8	6 1/8
48	6 3/8	6 3/8	43 1/2	5 3/8	5 3/8	42	6 3/8	6 3/8	6 3/8
50	6 1/2	6 1/2	45 1/2	5 1/2	5 1/2	44	6 1/2	6 1/2	6 1/2
52	6 5/8	6 5/8	47 1/2	5 5/8	5 5/8	46	6 5/8	6 5/8	6 5/8
54	6 7/8	6 7/8	49 1/2	5 7/8	5 7/8	48	6 7/8	6 7/8	6 7/8
56	7 1/8	7 1/8	51 1/2	6 1/8	6 1/8	50	7 1/8	7 1/8	7 1/8
58	7 3/8	7 3/8	53 1/2	6 3/8	6 3/8	52	7 3/8	7 3/8	7 3/8
60	7 1/2	7 1/2	55 1/2	6 1/2	6 1/2	54	7 1/2	7 1/2	7 1/2
62	7 5/8	7 5/8	57 1/2	6 5/8	6 5/8	56	7 5/8	7 5/8	7 5/8
64	7 7/8	7 7/8	59 1/2	6 7/8	6 7/8	58	7 7/8	7 7/8	7 7/8
66	8 1/8	8 1/8	61 1/2	7 1/8	7 1/8	60	8 1/8	8 1/8	8 1/8
68	8 3/8	8 3/8	63 1/2	7 3/8	7 3/8	62	8 3/8	8 3/8	8 3/8
70	8 1/2	8 1/2	65 1/2	7 1/2	7 1/2	64	8 1/2	8 1/2	8 1/2
72	8 5/8	8 5/8	67 1/2	7 5/8	7 5/8	66	8 5/8	8 5/8	8 5/8
74	8 7/8	8 7/8	69 1/2	7 7/8	7 7/8	68	8 7/8	8 7/8	8 7/8
76	9 1/8	9 1/8	71 1/2	8 1/8	8 1/8	70	9 1/8	9 1/8	9 1/8
78	9 3/8	9 3/8	73 1/2	8 3/8	8 3/8	72	9 3/8	9 3/8	9 3/8
80	9 1/2	9 1/2	75 1/2	8 1/2	8 1/2	74	9 1/2	9 1/2	9 1/2
82	9 5/8	9 5/8	77 1/2	8 5/8	8 5/8	76	9 5/8	9 5/8	9 5/8
84	9 7/8	9 7/8	79 1/2	8 7/8	8 7/8	78	9 7/8	9 7/8	9 7/8
86	10 1/8	10 1/8	81 1/2	9 1/8	9 1/8	80	10 1/8	10 1/8	10 1/8
88	10 3/8	10 3/8	83 1/2	9 3/8	9 3/8	82	10 3/8	10 3/8	10 3/8
90	10 1/2	10 1/2	85 1/2	9 1/2	9 1/2	84	10 1/2	10 1/2	10 1/2
92	10 5/8	10 5/8	87 1/2	9 5/8	9 5/8	86	10 5/8	10 5/8	10 5/8
94	10 7/8	10 7/8	89 1/2	9 7/8	9 7/8	88	10 7/8	10 7/8	10 7/8
96	11 1/8	11 1/8	91 1/2	10 1/8	10 1/8	90	11 1/8	11 1/8	11 1/8
98	11 3/8	11 3/8	93 1/2	10 3/8	10 3/8	92	11 3/8	11 3/8	11 3/8
100	11 1/2	11 1/2	95 1/2	10 1/2	10 1/2	94	11 1/2	11 1/2	11 1/2
102	11 5/8	11 5/8	97 1/2	10 5/8	10 5/8	96	11 5/8	11 5/8	11 5/8
104	11 7/8	11 7/8	99 1/2	10 7/8	10 7/8	98	11 7/8	11 7/8	11 7/8
106	12 1/8	12 1/8	101 1/2	11 1/8	11 1/8	100	12 1/8	12 1/8	12 1/8
108	12 3/8	12 3/8	103 1/2	11 3/8	11 3/8	102	12 3/8	12 3/8	12 3/8
110	12 1/2	12 1/2	105 1/2	11 1/2	11 1/2	104	12 1/2	12 1/2	12 1/2
112	12 5/8	12 5/8	107 1/2	11 5/8	11 5/8	106	12 5/8	12 5/8	12 5/8
114	12 7/8	12 7/8	109 1/2	11 7/8	11 7/8	108	12 7/8	12 7/8	12 7/8
116	13 1/8	13 1/8	111 1/2	12 1/8	12 1/8	110	13 1/8	13 1/8	13 1/8
118	13 3/8	13 3/8	113 1/2	12 3/8	12 3/8	112	13 3/8	13 3/8	13 3/8
120	13 1/2	13 1/2	115 1/2	12 1/2	12 1/2	114	13 1/2	13 1/2	13 1/2
122	13 5/8	13 5/8	117 1/2	12 5/8	12 5/8	116	13 5/8	13 5/8	13 5/8
124	13 7/8	13 7/8	119 1/2	12 7/8	12 7/8	118	13 7/8	13 7/8	13 7/8
126	14 1/8	14 1/8	121 1/2	13 1/8	13 1/8	120	14 1/8	14 1/8	14 1/8
128	14 3/8	14 3/8	123 1/2	13 3/8	13 3/8	122	14 3/8	14 3/8	14 3/8
130	14 1/2	14 1/2	125 1/2	13 1/2	13 1/2	124	14 1/2	14 1/2	14 1/2
132	14 5/8	14 5/8	127 1/2	13 5/8	13 5/8	126	14 5/8	14 5/8	14 5/8
134	14 7/8	14 7/8	129 1/2	13 7/8	13 7/8	128	14 7/8	14 7/8	14 7/8
136	15 1/8	15 1/8	131 1/2	14 1/8	14 1/8	130	15 1/8	15 1/8	15 1/8
138	15 3/8	15 3/8	133 1/2	14 3/8	14 3/8	132	15 3/8	15 3/8	15 3/8
140	15 1/2	15 1/2	135 1/2	14 1/2	14 1/2	134	15 1/2	15 1/2	15 1/2
142	15 5/8	15 5/8	137 1/2	14 5/8	14 5/8	136	15 5/8	15 5/8	15 5/8
144	15 7/8	15 7/8	139 1/2	14 7/8	14 7/8	138	15 7/8	15 7/8	15 7/8
146	16 1/8	16 1/8	141 1/2	15 1/8	15 1/8	140	16 1/8	16 1/8	16 1/8
148	16 3/8	16 3/8	143 1/2	15 3/8	15 3/8	142	16 3/8	16 3/8	16 3/8
150	16 1/2	16 1/2	145 1/2	15 1/2	15 1/2	144	16 1/2	16 1/2	16 1/2
152	16 5/8	16 5/8	147 1/2	15 5/8	15 5/8	146	16 5/8	16 5/8	16 5/8
154	16 7/8	16 7/8	149 1/2	15 7/8	15 7/8	148	16 7/8	16 7/8	16 7/8
156	17 1/8	17 1/8	151 1/2	16 1/8	16 1/8	150	17 1/8	17 1/8	17 1/8
158	17 3/8	17 3/8	153 1/2	16 3/8	16 3/8	152	17 3/8	17 3/8	17 3/8
160	17 1/2	17 1/2	155 1/2	16 1/2	16 1/2	154	17 1/2	17 1/2	17 1/2
162	17 5/8	17 5/8	157 1/2	16 5/8	16 5/8	156	17 5/8	17 5/8	17 5/8
164	17 7/8	17 7/8	159 1/2	16 7/8	16 7/8	158	17 7/8	17 7/8	17 7/8
166	18 1/8	18 1/8	161 1/2	17 1/8	17 1/8	160	18 1/8	18 1/8	18 1/8
168	18 3/8	18 3/8	163 1/2	17 3/8	17 3/8	162	18 3/8	18 3/8	18 3/8
170	18 1/2	18 1/2	165 1/2	17 1/2	17 1/2	164	18 1/2	18 1/2	18 1/2
172	18 5/8	18 5/8	167 1/2	17 5/8	17 5/8	166	18 5/8	18 5/8	18 5/8
174	18 7/8	18 7/8	169 1/2	17 7/8	17 7/8	168	18 7/8	18 7/8	18 7/8
176	19 1/8	19 1/8	171 1/2	18 1/8	18 1/8	170	19 1/8	19 1/8	19 1/8
178	19 3/8	19 3/8	173 1/2	18 3/8	18 3/8	172	19 3/8	19 3/8	19 3/8
180	19 1/2	19 1/2	175 1/2	18 1/2	18 1/2	174	19 1/2	19 1/2	19 1/2
182	19 5/8	19 5/8	177 1/2	18 5/8	18 5/8	176	19 5/8	19 5/8	19 5/8
184	19 7/8	19 7/8	179 1/2	18 7/8	18 7/8	178	19 7/8	19 7/8	19 7/8
186	20 1/8	20 1/8	181 1/2	19 1/8	19 1/8	180	20 1/8	20 1/8	20 1/8
188	20 3/8	20 3/8	183 1/2	19 3/8	19 3/8	182	20 3/8	20 3/8	20 3/8
190	20 1/2	20 1/2	185 1/2	19 1/2	19 1/2	184	20 1/2	20 1/2	20 1/2
192	20 5/8	20 5/8	187 1/2	19 5/8	19 5/8	186	20 5/8	20 5/8	20 5/8
194	20 7/8	20 7/8	189 1/2	19 7/8	19 7/8	188	20 7/8	20 7/8	20 7/8
196	21 1/8	21 1/8	191 1/2	20 1/8	20 1/8	190	21 1/8	21 1/8	21 1/8
198	21 3/8	21 3/8	193 1/2	20 3/8	20 3/8	192	21 3/8	21 3/8	21 3/8
200	21 1/2	21 1/2	195 1/2	20 1/2	20 1/2	194	21 1/2	21 1/2	21 1/2
202	21 5/8	21 5/8	197 1/2	20 5/8	20 5/8	196	21 5/8	21 5/8	21 5/8
204	21 7/8	21 7/8	199 1/2	20 7/8	20 7/8	198	21 7/8	21 7/8	21 7/8
206	22 1/8	22 1/8	201 1/2	21 1/8	21 1/8	200	22 1/8	22 1/8	22 1/8
208	22 3/8	22 3/8	203 1/2	21 3/8	21 3/8	202	22 3/8	22 3/8	22 3/8
210	22 1/2	22 1/2	205 1/2	21 1/2	21 1/2	204	22 1/2	22 1/2	22 1/2
212	22 5/8	22 5/8	207 1/2	21 5/8	21 5/8	206	22 5/8	22 5/8	22 5/8
214	22 7/8	22 7/8	209 1/2	21 7/8	21 7/8	208	22 7/8	22 7/8	22 7/8
216	23 1/8	23 1/8	211 1/2	22 1/8	22 1/8	210	23 1/8	23 1/8	23 1/8
218	23 3/8	23 3/8	213 1/2	22 3/8	22 3/8	212	23 3/8	23 3/8	23 3/8
220	23 1/2	23 1/2	215 1/2	22 1/2	22 1/2	214	23 1/2	23 1/2	23 1/2
222	23 5/8	23 5/8	217 1/2	22 5/8	22 5/8	216	23 5/8	23 5/8	23 5/8
224	23 7/8	23 7/8	219 1/2	22 7/8	22 7/8	218	23 7/8	23 7/8	23 7/8
226	24 1/8	24 1/8	221 1/2	23 1/8	23 1/8	220	24 1/8	24 1/8	24 1/8
228	24 3/8	24 3/8	223 1/2	23 3/8	23 3/8	222	24 3/8	24 3/8	24 3/8
230	24 1/2	24 1/2	225 1/2	23 1/2	23 1/2	224	24 1/2	24 1/2	24 1/2
232	24 5/8	24 5/8	227 1/2	23 5/8	23 5/8	226	24 5/8	24 5/8	24 5/8
234	24 7/8	24 7/8	229 1/2	23 7/8	23 7/8	228	24 7/8	24 7/8	24 7/8
236	25 1/8	25 1/8	231 1/2	24 1/8	24 1/8	230	25 1/8	25 1/8	25 1/8
238	25 3/8	25 3/8	233 1/2	24 3/8	24 3/8	232	25 3/8	25 3/8	25 3/8
240	25 1/2	25 1/2	235 1/2	24 1/2	24 1/2	234	25 1/2	25 1/2	25 1/2
242	25 5/8	25 5/8	237 1/2	24 5/8	24 5/8	236	25 5/8	25 5/8	25 5/8
244	25 7/8	25 7/8</							

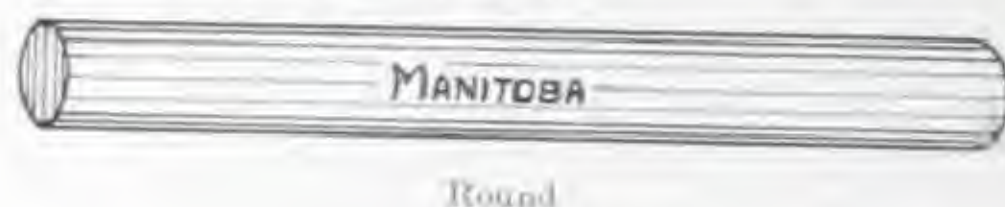


## MERCHANT BARS

We own and operate at Selkirk, Manitoba, our own Steel Plant comprised of a basic open hearth furnace of twenty tons capacity per heat (80 tons daily) and three rolling mills, a 9-inch, a 12-inch and a 16-inch.

The furnace is of the basic type as in this kind it is possible to produce steel of uniform quality from a wider range of raw material. Fuel oil is used to generate the high temperatures necessary for melting and refining.

All the rolling mills are of the Belgian type, driven by electric motors of 500, 350 and 800 h.p. capacity.



Round



Square



Flat



Band



Half-Round

No. 8—Types of Merchant Bars

Merchant grades in both high and extremely low carbons have been supplied for all of the manufacturing processes at present being carried on in Western Canada and we can furnish any of these grades in rounds, squares, flats, bands, half rounds and ovals within the following limits:

- ROUNDS } —From  $\frac{3}{8}$  inch diameter up to and including 3 inch diameter.  
 HALF ROUNDS }  
 SQUARES—From  $\frac{3}{8}$  inch square up to and including 3-inch square.  
 FLATS—From  $\frac{3}{16}$  inch x  $\frac{3}{4}$  inch up to and including 1½ inch x 6 inch.  
 BANDS—From  $\frac{3}{4}$  inch to 3 inch in width, and  $\frac{1}{8}$  inch thick.

The refined molten steel from the open hearth furnace is poured into ingots, each ingot being marked with its respective heat number. Our laboratory makes a careful analysis of each heat and this information is recorded in the office for future reference. The records will therefore show in a moment the physical properties of all of the steel which we have on hand at any time and from these we draw those suitable to customer's specifications as orders are received.

If suitable qualities are not available from storage, the furnace is operated on the grade required to enable completion of the orders as required.

We are able to supply steel to any of the standard specifications and over a period of years have enjoyed the confidence of our customers who all agree as to the uniformity and workability of the bars which we supply.

See  
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# SQUARE AND ROUND BARS

## WEIGHTS AND AREAS

Size Inches	Weights, Lbs. per Foot		Area, Square Inches		Size Inches	Weights, Lbs. per Foot		Area, Square Inches	
	□	○	□	○		□	○	□	○
1	10.2	10.0	0.804	0.785	1	30.0	29.7	7.068	7.068
1 1/8	13.0	12.8	1.061	1.032	1 1/8	31.8	31.5	7.489	7.489
1 1/4	15.0	14.8	1.227	1.200	1 1/4	33.9	33.6	7.910	7.910
1 3/8	17.3	17.1	1.405	1.376	1 3/8	36.3	36.0	8.341	8.341
1 1/2	19.7	19.5	1.594	1.564	1 1/2	38.8	38.5	8.782	8.782
1 5/8	22.3	22.1	1.794	1.764	1 5/8	41.4	41.1	9.233	9.233
1 3/4	25.0	24.8	2.005	1.975	1 3/4	44.1	43.8	9.694	9.694
2	28.7	28.5	2.250	2.220	2	46.9	46.6	10.165	10.165
2 1/8	32.6	32.4	2.509	2.479	2 1/8	49.8	49.5	10.646	10.646
2 1/4	36.7	36.5	2.781	2.751	2 1/4	52.8	52.5	11.137	11.137
2 3/8	41.0	40.8	3.067	3.037	2 3/8	55.9	55.6	11.638	11.638
2 1/2	45.5	45.3	3.367	3.337	2 1/2	59.1	58.8	12.149	12.149
2 5/8	50.2	50.0	3.681	3.651	2 5/8	62.4	62.1	12.670	12.670
2 3/4	55.1	54.9	4.009	3.979	2 3/4	65.8	65.5	13.201	13.201
3	60.2	60.0	4.350	4.320	3	69.3	69.0	13.742	13.742
3 1/8	65.5	65.3	4.705	4.675	3 1/8	72.9	72.6	14.293	14.293
3 1/4	71.0	70.8	5.074	5.044	3 1/4	76.6	76.3	14.854	14.854
3 3/8	76.7	76.5	5.457	5.427	3 3/8	80.4	80.1	15.425	15.425
3 1/2	82.6	82.4	5.854	5.824	3 1/2	84.3	84.0	16.006	16.006
3 5/8	88.7	88.5	6.265	6.235	3 5/8	88.3	88.0	16.597	16.597
3 3/4	95.0	94.8	6.690	6.660	3 3/4	92.4	92.1	17.198	17.198
4	101.5	101.3	7.129	7.099	4	96.6	96.3	17.809	17.809
4 1/8	108.2	108.0	7.582	7.552	4 1/8	100.9	100.6	18.430	18.430
4 1/4	115.1	114.9	8.049	8.019	4 1/4	105.3	105.0	19.061	19.061
4 3/8	122.3	122.1	8.530	8.500	4 3/8	109.8	109.5	19.702	19.702
4 1/2	129.7	129.5	9.025	8.995	4 1/2	114.4	114.1	20.353	20.353
4 5/8	137.4	137.2	9.534	9.504	4 5/8	119.1	118.8	21.014	21.014
4 3/4	145.3	145.1	10.057	10.027	4 3/4	123.9	123.6	21.685	21.685
5	153.5	153.3	10.594	10.564	5	128.8	128.5	22.366	22.366
5 1/8	161.9	161.7	11.145	11.115	5 1/8	133.8	133.5	23.057	23.057
5 1/4	170.5	170.3	11.710	11.680	5 1/4	138.9	138.6	23.758	23.758
5 3/8	179.4	179.2	12.289	12.259	5 3/8	144.1	143.8	24.469	24.469
5 1/2	188.5	188.3	12.882	12.852	5 1/2	149.4	149.1	25.190	25.190
5 5/8	197.9	197.7	13.489	13.459	5 5/8	154.8	154.5	25.921	25.921
5 3/4	207.5	207.3	14.110	14.080	5 3/4	160.3	160.0	26.662	26.662
6	217.4	217.2	14.745	14.715	6	165.9	165.6	27.413	27.413
6 1/8	227.5	227.3	15.394	15.364	6 1/8	171.6	171.3	28.174	28.174
6 1/4	237.9	237.7	16.057	16.027	6 1/4	177.4	177.1	28.945	28.945
6 3/8	248.5	248.3	16.734	16.704	6 3/8	183.3	183.0	29.726	29.726
6 1/2	259.4	259.2	17.425	17.395	6 1/2	189.3	189.0	30.517	30.517
6 5/8	270.5	270.3	18.130	18.100	6 5/8	195.4	195.1	31.318	31.318
6 3/4	281.8	281.6	18.849	18.819	6 3/4	201.6	201.3	32.129	32.129
7	293.4	293.2	19.582	19.552	7	207.9	207.6	32.950	32.950
7 1/8	305.2	305.0	20.329	20.299	7 1/8	214.3	214.0	33.781	33.781
7 1/4	317.3	317.1	21.090	21.060	7 1/4	220.8	220.5	34.622	34.622
7 3/8	329.6	329.4	21.865	21.835	7 3/8	227.4	227.1	35.473	35.473
7 1/2	342.1	341.9	22.654	22.624	7 1/2	234.1	233.8	36.334	36.334
7 5/8	354.8	354.6	23.457	23.427	7 5/8	240.9	240.6	37.205	37.205
7 3/4	367.7	367.5	24.274	24.244	7 3/4	247.8	247.5	38.086	38.086
8	380.9	380.7	25.105	25.075	8	254.8	254.5	38.977	38.977
8 1/8	394.3	394.1	25.950	25.920	8 1/8	261.9	261.6	39.878	39.878
8 1/4	407.9	407.7	26.809	26.779	8 1/4	269.1	268.8	40.789	40.789
8 3/8	421.7	421.5	27.682	27.652	8 3/8	276.4	276.1	41.710	41.710
8 1/2	435.7	435.5	28.569	28.539	8 1/2	283.8	283.5	42.641	42.641
8 5/8	449.9	449.7	29.470	29.440	8 5/8	291.3	291.0	43.582	43.582
8 3/4	464.3	464.1	30.385	30.355	8 3/4	298.9	298.6	44.533	44.533
9	478.9	478.7	31.314	31.284	9	306.6	306.3	45.494	45.494
9 1/8	493.7	493.5	32.257	32.227	9 1/8	314.4	314.1	46.465	46.465
9 1/4	508.7	508.5	33.214	33.184	9 1/4	322.3	322.0	47.446	47.446
9 3/8	523.9	523.7	34.185	34.155	9 3/8	330.3	330.0	48.437	48.437
9 1/2	539.3	539.1	35.170	35.140	9 1/2	338.4	338.1	49.438	49.438
9 5/8	554.9	554.7	36.169	36.139	9 5/8	346.6	346.3	50.449	50.449
9 3/4	570.7	570.5	37.182	37.152	9 3/4	354.9	354.6	51.470	51.470
10	586.7	586.5	38.209	38.179	10	363.3	363.0	52.501	52.501
10 1/8	602.9	602.7	39.250	39.220	10 1/8	371.8	371.5	53.542	53.542
10 1/4	619.3	619.1	40.305	40.275	10 1/4	380.4	380.1	54.593	54.593
10 3/8	635.9	635.7	41.374	41.344	10 3/8	389.1	388.8	55.654	55.654
10 1/2	652.7	652.5	42.457	42.427	10 1/2	397.9	397.6	56.725	56.725
10 5/8	669.7	669.5	43.554	43.524	10 5/8	406.8	406.5	57.806	57.806
10 3/4	686.9	686.7	44.665	44.635	10 3/4	415.8	415.5	58.897	58.897
11	704.3	704.1	45.790	45.760	11	424.9	424.6	59.998	59.998
11 1/8	721.9	721.7	46.929	46.899	11 1/8	434.1	433.8	61.109	61.109
11 1/4	739.7	739.5	48.082	48.052	11 1/4	443.4	443.1	62.230	62.230
11 3/8	757.7	757.5	49.249	49.219	11 3/8	452.8	452.5	63.361	63.361
11 1/2	775.9	775.7	50.430	50.400	11 1/2	462.3	462.0	64.502	64.502
11 5/8	794.3	794.1	51.625	51.595	11 5/8	471.9	471.6	65.653	65.653
11 3/4	812.9	812.7	52.834	52.804	11 3/4	481.6	481.3	66.814	66.814
12	831.7	831.5	54.057	54.027	12	491.4	491.1	67.985	67.985
12 1/8	850.7	850.5	55.294	55.264	12 1/8	501.3	501.0	69.166	69.166
12 1/4	869.9	869.7	56.545	56.515	12 1/4	511.3	511.0	70.357	70.357
12 3/8	889.3	889.1	57.809	57.779	12 3/8	521.4	521.1	71.558	71.558
12 1/2	908.9	908.7	59.087	59.057	12 1/2	531.6	531.3	72.769	72.769
12 5/8	928.7	928.5	60.379	60.349	12 5/8	541.9	541.6	73.990	73.990
12 3/4	948.7	948.5	61.684	61.654	12 3/4	552.3	552.0	75.221	75.221
13	968.9	968.7	62.994	62.964	13	562.8	562.5	76.462	76.462
13 1/8	989.3	989.1	64.317	64.287	13 1/8	573.4	573.1	77.713	77.713
13 1/4	1009.9	1009.7	65.654	65.624	13 1/4	584.1	583.8	78.974	78.974
13 3/8	1030.7	1030.5	67.005	66.975	13 3/8	594.9	594.6	80.245	80.245
13 1/2	1051.7	1051.5	68.369	68.339	13 1/2	605.8	605.5	81.526	81.526
13 5/8	1072.9	1072.7	69.747	69.717	13 5/8	616.8	616.5	82.817	82.817
13 3/4	1094.3	1094.1	71.139	71.109	13 3/4	627.9	627.6	84.118	84.118
14	1115.9	1115.7	72.545	72.515	14	639.1	638.8	85.429	85.429
14 1/8	1137.7	1137.5	73.965	73.935	14 1/8	650.4	650.1	86.750	86.750
14 1/4	1159.7	1159.5	75.399	75.369	14 1/4	661.8	661.5	88.081	88.081
14 3/8	1181.9	1181.7	76.847	76.817	14 3/8	673.3	673.0	89.422	89.422
14 1/2	1204.3	1204.1	78.309	78.279	14 1/2	684.9	684.6	90.773	90.773
14 5/8	1226.9	1226.7	79.784	79.754	14 5/8	696.6	696.3	92.134	92.134
14 3/4	1249.7	1249.5	81.272	81.242	14 3/4	708.4	708.1	93.505	93.505
15	1272.7	1272.5	82.774	82.744	15	720.3	720.0	94.886	94.886

For weights of flats, see pages 18 to 22.



# SQUARE AND ROUND BARS

## WEIGHTS AND AREAS

Size, Inches	Weight, Lbs. per Foot		Area, Square Inches		Size, Inches	Weight, Lbs. per Foot		Area, Square Inches	
	□	○	□	○		□	○	□	○
6	122.40	96.13	36.000	28.274	9	275.40	216.30	81.000	63.617
$\frac{1}{16}$	124.96	98.15	36.754	28.866	$\frac{1}{16}$	279.24	219.31	82.129	64.504
$\frac{1}{8}$	127.55	100.18	37.516	29.465	$\frac{1}{8}$	283.10	222.35	83.266	65.397
$\frac{3}{16}$	130.17	102.23	38.285	30.069	$\frac{3}{16}$	286.99	225.41	84.410	66.296
$\frac{1}{4}$	132.81	104.31	39.063	30.680	$\frac{1}{4}$	290.91	228.48	85.563	67.201
$\frac{5}{16}$	135.48	106.41	39.848	31.296	$\frac{5}{16}$	294.86	231.58	86.723	68.112
$\frac{3}{8}$	138.18	108.53	40.641	31.919	$\frac{3}{8}$	298.83	234.70	87.891	69.029
$\frac{7}{8}$	140.90	110.66	41.441	32.548	$\frac{7}{8}$	302.83	237.84	89.066	69.953
$\frac{1}{2}$	143.65	112.82	42.250	33.183	$\frac{1}{2}$	306.85	241.00	90.250	70.882
$\frac{3}{4}$	146.43	115.00	43.066	33.824	$\frac{3}{4}$	310.90	244.18	91.441	71.818
$\frac{5}{8}$	149.23	117.20	43.891	34.472	$\frac{5}{8}$	314.98	247.38	92.641	72.760
$\frac{3}{4}$	152.06	119.43	44.723	35.125	$\frac{3}{4}$	319.08	250.61	93.848	73.708
$\frac{7}{8}$	154.91	121.67	45.563	35.785	$\frac{7}{8}$	323.21	253.85	95.063	74.662
$\frac{1}{2}$	157.79	123.93	46.410	36.450	$\frac{1}{2}$	327.37	257.12	96.285	75.622
$\frac{3}{4}$	160.70	126.22	47.260	37.122	$\frac{3}{4}$	331.55	260.40	97.516	76.589
$\frac{7}{8}$	163.64	128.52	48.129	37.800	$\frac{7}{8}$	335.76	263.71	98.754	77.561
7	166.60	130.85	49.000	38.485	10	340.00	267.04	100.000	78.540
$\frac{1}{16}$	169.59	133.19	49.879	39.175	$\frac{1}{16}$	344.26	270.38	101.254	79.525
$\frac{1}{8}$	172.60	135.56	50.766	39.871	$\frac{1}{8}$	348.55	273.75	102.516	80.516
$\frac{3}{16}$	175.64	137.95	51.660	40.574	$\frac{3}{16}$	352.87	277.14	103.785	81.513
$\frac{1}{4}$	178.71	140.36	52.563	41.282	$\frac{1}{4}$	357.21	280.55	105.063	82.516
$\frac{5}{16}$	181.81	142.79	53.473	41.997	$\frac{5}{16}$	361.58	283.99	106.348	83.525
$\frac{3}{8}$	184.93	145.24	54.391	42.718	$\frac{3}{8}$	365.98	287.44	107.641	84.541
$\frac{7}{8}$	188.07	147.71	55.316	43.445	$\frac{7}{8}$	370.40	290.91	108.941	85.563
$\frac{1}{2}$	191.25	150.21	56.250	44.179	$\frac{1}{2}$	374.85	294.41	110.250	86.590
$\frac{3}{4}$	194.45	152.72	57.191	44.918	$\frac{3}{4}$	379.33	297.92	111.566	87.624
$\frac{5}{8}$	197.68	155.26	58.141	45.661	$\frac{5}{8}$	383.83	301.46	112.891	88.664
$\frac{3}{4}$	200.93	157.81	59.098	46.415	$\frac{3}{4}$	388.36	305.02	114.223	89.710
$\frac{7}{8}$	204.21	160.39	60.063	47.173	$\frac{7}{8}$	392.91	308.59	115.563	90.763
$\frac{1}{2}$	207.52	162.99	61.035	47.937	$\frac{1}{2}$	397.49	312.19	116.910	91.821
$\frac{3}{4}$	210.85	165.60	62.016	48.707	$\frac{3}{4}$	402.10	315.81	118.266	92.886
$\frac{7}{8}$	214.21	168.24	63.004	49.483	$\frac{7}{8}$	406.74	319.45	119.629	93.957
8	217.60	170.90	64.000	50.265	11	411.40	323.11	121.000	95.033
$\frac{1}{16}$	221.01	173.58	65.004	51.054	$\frac{1}{16}$	416.09	326.80	122.379	96.116
$\frac{1}{8}$	224.45	176.29	66.016	51.849	$\frac{1}{8}$	420.80	330.50	123.766	97.205
$\frac{3}{16}$	227.92	179.01	67.035	52.649	$\frac{3}{16}$	425.54	334.22	125.160	98.301
$\frac{1}{4}$	231.41	181.75	68.063	53.456	$\frac{1}{4}$	430.31	337.97	126.563	99.402
$\frac{5}{16}$	234.93	184.52	69.098	54.269	$\frac{5}{16}$	435.11	341.73	127.973	100.510
$\frac{3}{8}$	238.48	187.30	70.141	55.088	$\frac{3}{8}$	439.93	345.52	129.391	101.623
$\frac{7}{8}$	242.05	190.11	71.191	55.914	$\frac{7}{8}$	444.78	349.33	130.816	102.743
$\frac{1}{2}$	245.65	192.93	72.250	56.745	$\frac{1}{2}$	449.65	353.16	132.250	103.869
$\frac{3}{4}$	249.28	195.78	73.316	57.583	$\frac{3}{4}$	454.55	357.01	133.691	105.001
$\frac{5}{8}$	252.93	198.65	74.391	58.426	$\frac{5}{8}$	459.48	360.87	135.141	106.139
$\frac{3}{4}$	256.61	201.54	75.473	59.276	$\frac{3}{4}$	464.43	364.76	136.598	107.284
$\frac{7}{8}$	260.31	204.45	76.563	60.132	$\frac{7}{8}$	469.41	368.68	138.063	108.434
$\frac{1}{2}$	264.04	207.38	77.660	60.994	$\frac{1}{2}$	474.42	372.61	139.535	109.591
$\frac{3}{4}$	267.80	210.33	78.766	61.863	$\frac{3}{4}$	479.45	376.56	141.016	110.754
$\frac{7}{8}$	271.59	213.31	79.879	62.737	$\frac{7}{8}$	484.51	380.54	142.504	111.923
					12	489.60	384.53	144.000	113.088

For weights of flats, see pages 18 to 20.



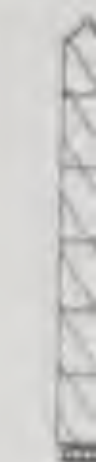




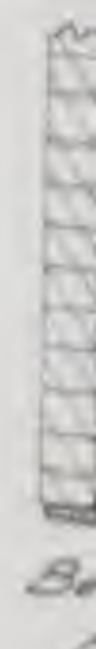


FIG. 3.—STEEL BRIDGE OVER ASSUMPTION RIVER AT COLUMBUS, IOWA. BRIDGE FABRICATED AND ERECTED BY THE MANITOBA BRIDGE AND IRON WORKS, LIMITED.

In de  
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## LINTELS

In determining the loads imposed on lintels, the clear width of opening, thickness of wall, material of which constructed, and whatever any weight above the wall above is carried, must be taken into consideration. If the wall is solid, with no window openings above the lintel, the wall will arch and exert a great deal of load on the adjoining wall which supports the lintel, without coming on the lintel. The portion for which the lintel should be designed would be a triangle whose length will be one-half the span. This is true only when the adjoining wall is sufficient to take the thrust due to the arch effect.



*Single Angle  
section shown*



*Double  
Channel*



*Channel and Plate  
with Angle for Reinforcement*



*Beam and  
Plate*



*Double  
Channel*



*Angle Section for  
Reinforcement (shown  
for Plate and Beam)*

Fig. 18. Types of Steel Lintels.

Each individual case must stand on its own merits and the lintel be designed accordingly. If the loads are undetermined, cracks are liable to appear in walls.

The diagrams above illustrate some different types of steel lintels. Lintels made of cast iron are not in general use in modern-day construction, although we have a number of patterns, and can supply cast iron lintels if desired.



## FLOORS AND FLOOR LOADS

**Kinds of Loads.**—Two kinds of loads are carried by structures. Live loads consist of the weight of machinery, merchandise, persons or other moving objects, or of cranes or other handling devices and their loads, the support of which is the purpose of the structure, including also wind stresses. Dead loads consist of the actual weight of the structure itself with the walls, floors, partitions, roofs, and all other permanent construction and fixtures. The dead loads stress the structure at all times and it must, therefore, be proportioned to sustain them at all times without reduction. The live loads may be taken at their full values or reduced in accordance with the probabilities that the structure as a whole or its principal members will not be subject at all times to the full theoretical live loading.

**Dead Loads.**—The permanent load should be calculated from known weights per unit of the material composing floors, partitions, walls, or other permanent construction. The weight assumed for the steel frame itself should be checked after the sections are determined and then the sizes readjusted if necessary.

**Live Loads.**—Live loads vary with the character of the structures. In buildings they consist of uniform loads per square foot of floor area, concentrated loads such as heavy safes, which may be applied at any point of the floor, and uniform loads per lineal foot of beams or girders. The load which produces the maximum bending moment or reaction is to be used in proportioning sections. The floor system between beams must of course be of sufficient strength to transmit any concentrated load to the beam.

In cities the minimum live loads to be used on the various classes of buildings are fixed by public ordinances, and are given on page 31 for the principal cities of the United States in accordance with the most recent building laws, which are intended to cover general conditions and do not include machinery or other concentrations. If such concentrations, like safes, armatures, generators, or printing presses, occur on floors, special provision should be made for them in the floor framing. Flat roofs of buildings which may be loaded with people, should be treated the same as floors and the same uniform live loads used as given in the table for dwellings, hotels or assembly rooms.

**Reduced Live Loads.**—Floor beams in buildings should be computed to sustain floor by floor the full live and dead loads. It is not probable that all the floors will be fully loaded at all times, and, therefore, good practice permits a reduction of the theoretical live load in the computations of column sections. See pages 54 and 55.

## BEARING PLATES

In the case where beams rest on walls, the table on page 51 gives sizes and thicknesses which depend on the end reaction, length of bearing and safe unit pressure for the different constructions of walls, and the dimensions given are for beams of usual spans.

Apartment  
Asylums,  
Detention  
Factories  
Light  
Heavy  
Hotels, I  
Office Bu  
Public B  
Munici  
Church  
Librar  
Theatre  
Schools  
Stores, li  
Warehou

Floor

Auditoria  
Armories

Garages,  
Corridor  
Stairway  
Sidewalk  
Roofs:  
Flat,  
Steep,  
Wind Pr

\*First  
Circum

\*Wind  
2 1/2 lbs.  
to 35 lbs







### EXPLANATION OF TABLES OF SAFE LOADS

The following tables give the greatest safe load (uniformly distributed over the entire length) which the steel shapes used as beams will carry.

These loads include the weight of the beam, which must be deducted to obtain the net load.

The loads given are based on a fiber stress of 16,000 pounds per square inch, and are entirely reliable for ordinary conditions where loads are quiescent, as in buildings.

For fluctuating loads causing vibration, especially if the beams are long as compared to their depth, the tabular loads should be reduced one-fifth; for rapidly moving loads, or where loads are suddenly applied with slight impact, the tabular loads should be reduced one-third.

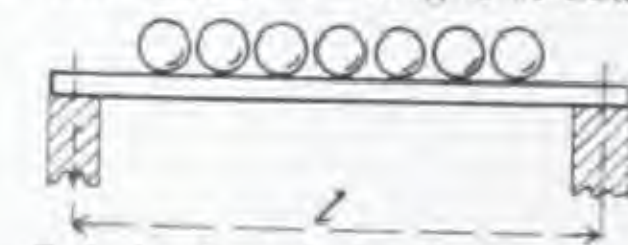
It is assumed that the beams are stiffened sideways to prevent buckling in the compression flange, otherwise tabular load must be reduced as follows.

Unbraced Length of Beam	Proportion to be used	Unbraced Length of Beam	Proportion to be used
10 × flange width	Full tabular load	30 × flange width	63% tabular load
15 × flange width	91% tabular load	35 × flange width	53% tabular load
20 × flange width	81% tabular load	40 × flange width	44% tabular load
25 × flange width	72% tabular load	45 × flange width	

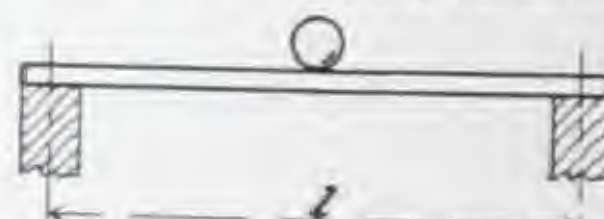
In many cases deflection will govern. The allowable deflection for plastered ceilings is 1/360 of the span. The deflection will be reduced in the same ratio as the load on the beam.

The bending moments and deflections of beams under various systems of loading are given below:

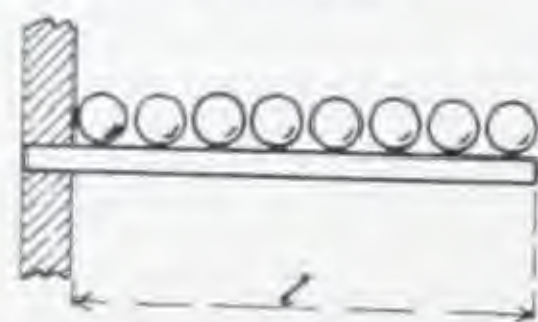
W = total load. l = length of beam. M = maximum bending moment.



Safe load = tabular load.  
M at center =  $\frac{1}{8} Wl$   
Deflection as in tables.



Safe load =  $\frac{1}{2}$  tabular load.  
M =  $\frac{1}{4} Wl$   
Deflection = .8 tabular deflection.



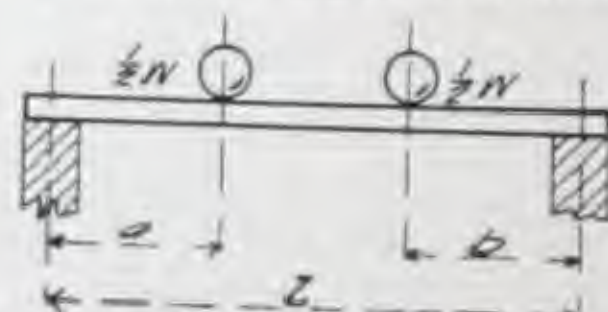
Safe load =  $\frac{1}{4}$  tabular load.  
M =  $\frac{1}{2} Wl$   
Deflection = 2.4 tabular deflection.



Safe load =  $\frac{1}{8}$  tabular load.  
M at point of support = W.  
Deflection = 3.2 tabular deflection.



Safe load = tabular load  $\times \frac{l}{8ab}$   
M =  $\frac{Wab}{l}$



Safe load = tabular load  $\times \frac{1}{4a}$   
M between loads =  $\frac{1}{2} Wa$



# SEAFS

## ALLOWABLE UNIT LOADS IN TENSILES OF STEEL

Maximum Working Stress 16,000 Pounds per Square Inch.

Nom. Size	Working Stress in Tensiles												Area
	Stress												
	1/2"	3/4"	1"	1 1/4"	1 1/2"	2"	2 1/2"	3"	3 1/2"	4"	4 1/2"	5"	
1/2"	10,000	15,000	20,000	25,000	30,000	40,000	50,000	60,000	70,000	80,000	90,000	100,000	0.75
3/4"	15,000	22,500	30,000	37,500	45,000	60,000	75,000	90,000	105,000	120,000	135,000	150,000	1.13
1"	20,000	30,000	40,000	50,000	60,000	80,000	100,000	120,000	140,000	160,000	180,000	200,000	1.57
1 1/4"	25,000	37,500	50,000	62,500	75,000	100,000	125,000	150,000	175,000	200,000	225,000	250,000	2.17
1 1/2"	30,000	45,000	60,000	75,000	90,000	120,000	150,000	180,000	210,000	240,000	270,000	300,000	2.81
2"	40,000	60,000	80,000	100,000	120,000	160,000	200,000	240,000	280,000	320,000	360,000	400,000	4.71
2 1/2"	50,000	75,000	100,000	125,000	150,000	200,000	250,000	300,000	350,000	400,000	450,000	500,000	6.46
3"	60,000	90,000	120,000	150,000	180,000	240,000	300,000	360,000	420,000	480,000	540,000	600,000	9.00
3 1/2"	70,000	105,000	140,000	175,000	210,000	280,000	350,000	420,000	490,000	560,000	630,000	700,000	12.57
4"	80,000	120,000	160,000	200,000	240,000	320,000	400,000	480,000	560,000	640,000	720,000	800,000	17.36
4 1/2"	90,000	135,000	180,000	225,000	270,000	360,000	450,000	540,000	630,000	720,000	810,000	900,000	21.66
5"	100,000	150,000	200,000	250,000	300,000	400,000	500,000	600,000	700,000	800,000	900,000	1,000,000	26.01
6"	120,000	180,000	240,000	300,000	360,000	480,000	600,000	720,000	840,000	960,000	1,080,000	1,200,000	37.71
7"	140,000	210,000	280,000	350,000	420,000	560,000	700,000	840,000	980,000	1,120,000	1,260,000	1,400,000	50.67
8"	160,000	240,000	320,000	400,000	480,000	640,000	800,000	960,000	1,120,000	1,280,000	1,440,000	1,600,000	63.43
9"	180,000	270,000	360,000	450,000	540,000	720,000	900,000	1,080,000	1,260,000	1,440,000	1,620,000	1,800,000	79.51
10"	200,000	300,000	400,000	500,000	600,000	800,000	1,000,000	1,200,000	1,400,000	1,600,000	1,800,000	2,000,000	101.31
11"	220,000	330,000	440,000	550,000	660,000	880,000	1,100,000	1,320,000	1,540,000	1,760,000	1,980,000	2,200,000	122.70
12"	240,000	360,000	480,000	600,000	720,000	960,000	1,200,000	1,440,000	1,680,000	1,920,000	2,160,000	2,400,000	144.17
14"	280,000	420,000	560,000	700,000	840,000	1,120,000	1,400,000	1,680,000	1,960,000	2,240,000	2,520,000	2,800,000	200.48
16"	320,000	480,000	640,000	800,000	960,000	1,280,000	1,600,000	1,920,000	2,240,000	2,560,000	2,880,000	3,200,000	261.21
18"	360,000	540,000	720,000	900,000	1,080,000	1,440,000	1,800,000	2,160,000	2,520,000	2,880,000	3,240,000	3,600,000	318.24
20"	400,000	600,000	800,000	1,000,000	1,200,000	1,600,000	2,000,000	2,400,000	2,800,000	3,200,000	3,600,000	4,000,000	377.00
22"	440,000	660,000	880,000	1,100,000	1,320,000	1,760,000	2,200,000	2,640,000	3,080,000	3,520,000	3,960,000	4,400,000	437.42
24"	480,000	720,000	960,000	1,200,000	1,440,000	1,920,000	2,400,000	2,880,000	3,360,000	3,840,000	4,320,000	4,800,000	499.44
26"	520,000	780,000	1,040,000	1,300,000	1,560,000	2,080,000	2,600,000	3,120,000	3,640,000	4,160,000	4,680,000	5,200,000	563.00
28"	560,000	840,000	1,120,000	1,400,000	1,680,000	2,240,000	2,800,000	3,360,000	3,920,000	4,480,000	5,040,000	5,600,000	628.16
30"	600,000	900,000	1,200,000	1,500,000	1,800,000	2,400,000	3,000,000	3,600,000	4,200,000	4,800,000	5,400,000	6,000,000	694.80
32"	640,000	960,000	1,280,000	1,600,000	1,920,000	2,560,000	3,200,000	3,840,000	4,480,000	5,120,000	5,760,000	6,400,000	763.04
36"	720,000	1,080,000	1,440,000	1,800,000	2,160,000	2,880,000	3,600,000	4,320,000	5,040,000	5,760,000	6,480,000	7,200,000	878.88
40"	800,000	1,200,000	1,600,000	2,000,000	2,400,000	3,200,000	4,000,000	4,800,000	5,600,000	6,400,000	7,200,000	8,000,000	996.00
44"	880,000	1,320,000	1,760,000	2,200,000	2,640,000	3,520,000	4,400,000	5,280,000	6,160,000	7,040,000	7,920,000	8,800,000	1,114.56
48"	960,000	1,440,000	1,920,000	2,400,000	2,880,000	3,840,000	4,800,000	5,760,000	6,720,000	7,680,000	8,640,000	9,600,000	1,234.56
52"	1,040,000	1,560,000	2,080,000	2,600,000	3,120,000	4,160,000	5,200,000	6,240,000	7,280,000	8,320,000	9,360,000	10,400,000	1,356.00
56"	1,120,000	1,680,000	2,240,000	2,800,000	3,360,000	4,480,000	5,600,000	6,720,000	7,840,000	8,960,000	10,080,000	11,200,000	1,478.56
60"	1,200,000	1,800,000	2,400,000	3,000,000	3,600,000	4,800,000	6,000,000	7,200,000	8,400,000	9,600,000	10,800,000	12,000,000	1,603.20
64"	1,280,000	1,920,000	2,560,000	3,200,000	3,840,000	5,120,000	6,400,000	7,680,000	8,960,000	10,240,000	11,520,000	12,800,000	1,729.92
68"	1,360,000	2,040,000	2,720,000	3,400,000	4,080,000	5,440,000	6,800,000	8,160,000	9,520,000	10,880,000	12,240,000	13,600,000	1,857.60
72"	1,440,000	2,160,000	2,880,000	3,600,000	4,320,000	5,760,000	7,200,000	8,640,000	10,080,000	11,520,000	13,000,000	14,400,000	1,987.20
76"	1,520,000	2,280,000	3,040,000	3,800,000	4,560,000	6,080,000	7,600,000	9,120,000	10,640,000	12,160,000	13,680,000	15,200,000	2,118.56
80"	1,600,000	2,400,000	3,200,000	4,000,000	4,800,000	6,400,000	8,000,000	9,600,000	11,200,000	12,800,000	14,400,000	16,000,000	2,251.20
84"	1,680,000	2,520,000	3,360,000	4,200,000	5,040,000	6,720,000	8,400,000	10,080,000	11,760,000	13,440,000	15,120,000	16,800,000	2,385.12
88"	1,760,000	2,640,000	3,520,000	4,400,000	5,280,000	7,040,000	8,800,000	10,560,000	12,320,000	14,080,000	15,840,000	17,600,000	2,520.32
92"	1,840,000	2,760,000	3,680,000	4,600,000	5,520,000	7,360,000	9,120,000	10,880,000	12,640,000	14,400,000	16,160,000	18,400,000	2,657.12
96"	1,920,000	2,880,000	3,840,000	4,800,000	5,760,000	7,680,000	9,600,000	11,520,000	13,120,000	14,880,000	16,640,000	19,200,000	2,794.56
100"	2,000,000	3,000,000	4,000,000	5,000,000	6,000,000	8,000,000	10,000,000	12,000,000	14,000,000	16,000,000	18,000,000	20,000,000	2,933.60
104"	2,080,000	3,120,000	4,160,000	5,200,000	6,240,000	8,320,000	10,400,000	12,480,000	14,560,000	16,640,000	18,560,000	20,800,000	3,074.24
108"	2,160,000	3,240,000	4,320,000	5,400,000	6,480,000	8,640,000	10,800,000	12,960,000	15,040,000	17,120,000	19,040,000	21,600,000	3,216.00
112"	2,240,000	3,360,000	4,480,000	5,600,000	6,720,000	8,960,000	11,200,000	13,440,000	15,520,000	17,600,000	19,520,000	22,400,000	3,358.88
116"	2,320,000	3,480,000	4,640,000	5,800,000	6,960,000	9,280,000	11,600,000	13,920,000	16,000,000	18,080,000	20,000,000	23,200,000	3,502.88
120"	2,400,000	3,600,000	4,800,000	6,000,000	7,200,000	9,600,000	12,000,000	14,400,000	16,480,000	18,560,000	20,480,000	24,000,000	3,648.00
124"	2,480,000	3,720,000	4,960,000	6,200,000	7,440,000	9,920,000	12,400,000	14,880,000	16,960,000	19,040,000	20,960,000	24,800,000	3,794.24
128"	2,560,000	3,840,000	5,120,000	6,400,000	7,680,000	10,240,000	12,800,000	15,360,000	17,440,000	19,520,000	21,440,000	25,600,000	3,941.12
132"	2,640,000	3,960,000	5,280,000	6,600,000	7,920,000	10,560,000	13,200,000	15,840,000	17,920,000	20,000,000	21,920,000	26,400,000	4,089.60
136"	2,720,000	4,080,000	5,440,000	6,800,000	8,160,000	10,880,000	13,600,000	16,320,000	18,400,000	20,480,000	22,400,000	27,200,000	4,239.36
140"	2,800,000												



## BEAMS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Bending Stress: 16,000 Pounds per Square Inch

Span in Feet	Depth and Weight of Sections												Coefficient of Deflection
	20-Inch						18-Inch						
	100 lbs.	95 lbs.	90 lbs.	85 lbs.	81.4 lbs.	75 lbs.	70 lbs.	65.4 lbs.	60 lbs.	55 lbs.	50 lbs.	45.6 lbs.	
6	349.2	320.0	290.4	261.2	240.0	224.6	215.9	200.0	248.2	240.3	227.5	201.6	0.60
7	293.0	284.4	275.6	261.2	243.4	224.6	215.9	200.0	248.2	240.3	227.5	201.6	0.81
8	251.2	243.8	236.2	228.8	223.4	192.5	185.0	178.2	212.7	205.9	199.2	193.3	1.00
9	219.8	213.3	206.7	200.2	195.5	168.5	161.9	155.9	186.2	180.2	174.3	169.2	1.34
10	195.4	189.6	183.8	178.0	173.8	149.7	143.9	138.6	165.5	160.2	155.0	150.4	1.66
11	175.8	170.6	165.4	160.2	156.4	134.8	129.5	124.7	148.9	144.2	139.5	135.3	2.00
12	159.9	155.1	150.3	145.6	142.2	122.5	117.7	113.4	135.4	131.1	126.7	123.0	2.38
13	146.3	142.2	137.8	133.5	130.3	112.3	107.9	104.0	124.1	120.2	116.2	112.8	2.80
14	135.2	131.2	127.2	123.2	120.3	103.7	99.6	96.0	114.5	110.9	107.3	104.1	3.24
15	125.6	121.9	118.1	114.4	111.7	96.3	92.5	89.1	106.4	103.0	99.6	96.7	3.72
16	117.2	113.7	110.3	106.8	104.3	89.9	86.3	83.2	99.3	96.1	93.0	90.2	4.24
17	109.9	106.6	103.4	100.1	97.8	84.2	81.0	78.0	93.1	90.1	87.2	84.6	4.78
18	103.4	100.4	97.3	94.2	92.0	79.3	76.2	73.4	87.6	84.8	82.0	79.6	5.36
19	97.7	94.8	91.9	89.0	86.9	74.9	72.0	69.3	82.7	80.1	77.5	75.2	5.98
20	92.5	89.8	87.0	84.3	82.3	70.9	68.2	65.7	78.4	75.9	73.4	71.2	6.62
21	87.9	85.3	82.7	80.1	78.2	67.4	64.8	62.4	74.5	72.1	69.7	67.7	7.30
22	83.7	81.3	78.8	76.3	74.5	64.2	61.7	59.4	70.9	68.7	66.4	64.4	8.01
23	79.9	77.6	75.2	72.8	71.1	61.3	58.9	56.7	67.7	65.5	63.4	61.5	8.76
24	76.4	74.2	71.9	69.7	68.0	58.6	56.3	54.2	64.7	62.7	60.6	58.8	9.53
25	73.3	71.1	68.9	66.7	65.2	56.2	54.0	52.0	62.1	60.1	58.1	56.4	10.35
26	70.3	68.3	66.2	64.1	62.6	53.9	51.8	49.9	59.6	57.7	55.8	54.1	11.19
27	67.6	65.6	63.6	61.6	60.2	51.8	49.8	48.0	57.3	55.4	53.6	52.0	12.07
28	65.1	63.2	61.2	59.3	57.9	49.9	48.0	46.2	55.2	53.4	51.6	50.1	12.98
29	62.8	60.9	59.0	57.2	55.9	48.1	46.3	44.6	53.2	51.5	49.8	48.3	13.92
30	60.6	58.8	57.0	55.2	53.9	46.5	44.7	43.0	51.4	49.7	48.1	46.7	14.90
31	58.6	56.9	55.1	53.4	52.1	44.9	43.2	41.6	49.6	48.1	46.5	45.1	15.91
32	56.7	55.0	53.4	51.7	50.5	43.5	41.8	40.2	48.5	46.9	45.0	43.7	16.95
33	54.9	53.3	51.7	50.1	48.9	42.1	40.5	39.0	46.0	45.1	43.6	42.3	18.03
34	53.3	51.7	50.1	48.5	47.4	40.8	39.2	37.8	45.1	43.7	42.3	41.0	19.13
35	51.7	50.2	48.6	47.1	46.0	39.6	38.1	36.7	43.8	42.4	41.0	39.8	20.28
36	50.2	48.8	47.2	45.8	44.7	38.5	37.0	35.6	42.5	41.2	39.9	38.7	21.45
37	48.8	47.4	45.9	44.5	43.4	37.4	36.0	34.7	41.4	40.0	38.7	37.6	22.66
38	47.5	46.1	44.7	43.3	42.3	36.4	35.0	33.7	40.2	38.9	37.7	36.6	23.90
39	46.3	44.9	43.5	42.1	41.2	35.5	34.1	32.8	39.2	37.9	36.7	35.6	25.18
40	45.1	43.8	42.4	41.1	40.1	34.6	33.2	32.0	38.2	36.9	35.7	34.6	26.48
41	44.0	42.7	41.3	40.0	39.1	33.7	32.4	31.2	37.4	36.1	34.9	33.8	27.82
42	42.9	41.6	40.3	39.0	38.1	32.9	31.6	30.4	36.6	35.3	34.1	33.0	29.20

Loads in "heavy" type will produce maximum allowable shear in webs.  
 Loads in "light" type will produce excessive deflections.



## BEAMS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

(Maximum Bending Moment = 10000 Pounds per Square Foot)

M	Depth of Beam in Inches												Weight of Beam per Foot
	12 in. deep						14 in. deep						
	12	14	16	18	20	22	12	14	16	18	20	22	
1	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
2	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
3	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
4	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
5	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
6	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
7	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
8	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
9	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
10	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
11	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
12	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
13	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
14	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
15	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
16	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
17	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
18	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
19	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
20	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
21	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
22	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
23	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
24	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000
25	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000	10000

Note: "Beam" means the whole structure, including the ends.

Note: "Load" means the weight of the structure.



## BEAMS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Bending Stress: 16,000 Pounds per Square Inch

Span in Feet	Depth and Weight of Sections													Coefficient of Deflection
	15 in.		12-Inch						10-Inch					
	37.3 lbs.	55 lbs.	50 lbs.	45 lbs.	40.8 lbs.	35 lbs.	31.8 lbs.	27.9 lbs.	40 lbs.	35 lbs.	30 lbs.	25.4 lbs.	22.4 lbs.	
3		194.4							148.2	118.8				
4		189.2	164.9	135.6		102.7			112.4	103.7	89.4			0.15
5		141.9	134.1	126.3	110.4	100.9	84.0		84.3	77.7	71.2	62.0	50.4	0.27
6		113.5	107.2	101.0	95.6	80.7	76.7		67.4	62.2	57.0	52.1	48.5	0.41
7	99.6							68.2						
8	96.1	94.6	89.4	84.2	79.7	67.3	63.9	59.1	56.2	51.8	47.5	43.4	40.4	0.60
9	82.4	81.1	76.6	72.1	68.3	57.6	54.8	50.6	48.1	44.4	40.7	37.2	34.6	0.81
10	72.1	71.0	67.0	63.1	59.8	50.5	48.0	44.3	42.1	38.9	35.6	32.6	30.3	1.06
11	64.1	63.1	59.6	56.1	53.1	44.9	42.0	39.4	37.5	34.6	31.6	28.9	26.9	1.34
12	57.7	56.8	53.6	50.5	47.8	40.4	38.4	35.5	33.7	31.1	28.5	26.0	24.2	1.66
13	52.4	51.6	48.7	45.9	43.5	36.7	34.9	32.2	30.6	28.3	25.9	23.7	22.0	2.00
14	48.1	47.3	44.7	42.1	39.8	33.6	32.0	29.5	28.1	25.9	23.7	21.7	20.2	2.38
15	44.4	43.7	41.2	38.8	36.8	31.0	29.5	27.3	25.9	23.9	21.9	20.0	18.6	2.80
16	41.2	40.6	38.3	36.1	34.2	28.8	27.4	25.3	24.1	22.2	20.3	18.6	17.3	3.24
17	38.4	37.8	35.7	33.7	31.9	26.9	25.6	23.6	22.5	20.7	19.0	17.4	16.2	3.72
18	36.0	35.5	33.5	31.6	29.9	25.2	24.0	22.2	21.1	19.4	17.8	16.3	15.1	4.24
19	33.9	33.4	31.5	29.7	28.1	23.7	22.6	20.9	19.8	18.3	16.8	15.3	14.3	4.78
20	32.0	31.5	29.8	28.1	26.6	22.4	21.3	19.7	18.7	17.3	15.8	14.5	13.5	5.36
21	30.4	29.9	28.2	26.6	25.2	21.2	20.2	18.7	17.7	16.4	15.0	13.7	12.8	5.98
22	28.8	28.4	26.8	25.3	23.9	20.2	19.2	17.7	16.9	15.5	14.2	13.0	12.1	6.62
23	27.5	27.0	25.5	24.0	22.8	19.2	18.3	16.9	16.1	14.8	13.6	12.4	11.6	7.30
24	26.2	25.8	24.4	23.0	21.7	18.3	17.4	16.1	15.3	14.1	12.9	11.8	11.0	8.01
25	25.1	24.7	23.3	22.0	20.8	17.5	16.7	15.4						8.76
26	24.0	23.7	22.3	21.0	19.9	16.8	16.0	14.8						9.53
27	23.1	22.7	21.4	20.2	19.1	16.1	15.3	14.2						10.35
28	22.2	21.8	20.6	19.4	18.4	15.5	14.8	13.6						
29	21.4													11.19
30	20.6													12.07
31	19.9													12.98
32	19.2													13.92
33														14.90
34	18.6													
35	18.0													15.91
36														16.95

Loads in "heavy" type will produce maximum allowable shear in webs.  
 Loads in "static" type will produce excessive deflections.



## THE AIMS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Sampling Rate: 10000 Samples per Second (Hz)

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## H - BEAMS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Pending Stress: 16,000 Pounds per Square Inch

Span in Feet	Depth and Weight of Sections								Coeffi- cients of Deflection
	8-Inch			6-Inch			5-Inch	4-Inch	
	37.7 lb.	34.3 lb.	32.6 lb.	26.7 lb.	24.1 lb.	22.8 lb.	18.9 lb.	13.8 lb.	
3				52.5			31.3	25.0	0.15
4	80.0			42.1	37.5		25.4	19.0	0.27
5	64.4	60.0		33.7	32.1	30.0	20.3	14.3	0.41
6	53.7	51.4	50.0	28.1	26.7	26.1	16.9	11.4	0.60
7	46.0	44.0	43.0	24.1	22.9	22.3	14.5	9.5	0.81
8	40.3	38.5	37.6	21.1	20.4	19.6	12.7	8.1	1.06
9	35.8	34.2	33.4	18.7	17.8	17.4	11.3	7.1	1.34
10	32.2	30.8	30.1	16.8	16.0	15.6	10.1	6.3	1.66
11	29.3	28.0	27.3	15.3	14.6	14.2	9.2	5.7	2.00
12	26.8	25.7	25.1	14.0	13.4	13.0	8.5		2.38
13	24.8	23.7	23.1	13.0	12.3	12.0			2.80
14	23.0	22.0	21.5	12.0	11.5	11.2			3.24
15	21.5	20.5	20.1						3.72
16	20.1	19.3	18.8						4.24
17	18.9	18.1	17.7						4.78
18	17.9	17.1	16.7						5.36

Loads in "heavy" type will produce maximum allowable shear in webs.

Loads in "light" type will produce excessive deflections.



## CHANNELS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Bending Stress: 16,000 Pounds per Square Inch

Span in Feet	Depth and Weight of Sections												Coefficient of Deflection
	15-Inch						13-Inch						
	55 lbs.	50 lbs.	45 lbs.	40 lbs.	35 lbs.	33.9 lbs.	50 lbs.	45 lbs.	40 lbs.	37 lbs.	35 lbs.	31.8 lbs.	
	244.2	214.8	185.4				204.6	175.0					
3	203.4	190.4	177.2	156.0	126.6	120.0	171.2	159.8	145.6	127.9	116.2	97.5	0.15
4	152.5	142.8	132.9	123.1	113.3	111.1	128.4	119.8	111.3	106.2	102.8	97.4	0.27
5	122.0	114.3	106.3	98.5	90.7	88.9	102.7	95.9	89.1	85.0	82.3	77.9	0.41
6	101.7	95.2	88.6	82.1	75.6	74.1	85.6	79.9	74.2	70.8	68.6	65.0	0.60
7	87.1	81.6	75.9	70.3	64.7	63.5	73.3	68.4	63.6	60.6	58.8	55.7	0.81
8	76.3	71.4	66.5	61.6	56.7	55.6	64.2	59.9	55.7	53.1	51.4	48.7	1.06
9	67.8	63.5	59.1	54.7	50.4	49.4	57.1	53.2	49.5	47.2	45.7	43.3	1.34
10	61.0	57.1	53.2	49.3	45.3	44.5	51.3	47.9	44.5	42.5	41.1	39.0	1.66
11	55.5	51.9	48.3	44.8	41.2	40.4	46.7	43.6	40.5	38.6	37.4	35.4	2.00
12	50.9	47.6	44.3	41.1	37.7	37.0	42.8	39.9	37.1	35.4	34.3	32.5	2.38
13	47.0	44.0	40.9	37.9	34.9	34.2	39.5	36.9	34.3	32.7	31.6	30.0	2.80
14	43.6	40.8	38.0	35.2	32.4	31.8	36.7	34.2	31.8	30.3	29.4	27.8	3.24
15	40.7	38.1	35.5	32.8	30.2	29.6	34.2	31.9	29.7	28.3	27.4	26.0	3.72
16	38.1	35.7	33.2	30.8	28.3	27.8	32.1	30.0	27.8	26.6	25.7	24.4	4.24
17	35.9	33.6	31.3	29.0	26.7	26.1	30.2	28.2	26.2	25.0	24.2	22.9	4.78
18	33.9	31.7	29.5	27.4	25.2	24.7	28.5	26.6	24.7	23.6	22.9	21.7	5.36
19	32.1	30.1	28.0	25.9	23.9	23.4	27.0	25.2	23.4	22.4	21.6	20.5	5.98
20	30.5	28.6	26.6	24.6	22.7	22.2	25.7	24.0	22.3	21.2	20.6	19.5	6.62
21	29.1	27.2	25.3	23.5	21.6	21.2	24.5	22.8	21.2	20.2	19.6	18.6	7.30
22	27.7	26.0	24.2	22.4	20.6	20.2	23.3	21.8	20.2	19.3	18.7	17.7	8.01
23	26.5	24.8	23.1	21.4	19.7	19.3	22.3	20.8	19.4	18.5	17.9	16.9	8.76
24	25.4	23.8	22.2	20.5	18.9	18.5	21.4	20.0	18.6	17.7	17.1	16.2	9.53
25	24.4	22.9	21.3	19.7	18.1	17.8	20.5	19.2	17.8	17.0	16.5	15.6	10.35
26	23.5	22.0	20.5	18.9	17.4	17.1	19.8	18.4	17.1	16.3	15.8	15.0	11.19
27	22.6	21.2	19.7	18.2	16.8	16.5	18.4	17.7	16.5	15.7	15.2	14.4	12.07
28	21.8	20.4	19.0	17.6	16.2	15.9	18.3	17.1	15.9	15.2	14.7	13.9	12.98
29	21.0	19.7	18.3	17.0	15.6	15.3							13.92
30	20.3	19.0	17.7	16.4	15.1	14.8							14.90
31	19.7	18.4	17.2	15.9	14.6	14.3							15.91
32	19.1	17.9	16.6	15.4	14.2	13.9							16.95

Loads in "heavy" type will produce maximum allowable shear in webs.

Loads in "static" type will produce excessive deflections.



## CHANNELS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Bending Stress: 16,000 Pounds per Square Inch

Span in Feet	Depth and Weight of Sections										Coefficient of Deflection
	12-Inch					10-Inch					
	40 lbs.	35 lbs.	30 lbs.	25 lbs.	20.7 lbs.	35 lbs.	30 lbs.	25 lbs.	20 lbs.	15.8 lbs.	
2	181.2					164.0	134.6	105.2			0.07
3	174.7	151.7	122.4	92.9		122.9	100.8	96.8	75.8	48.0	0.15
4	116.4	105.9	95.5	85.0	67.2	81.9	73.2	64.5	55.8	47.6	0.27
5	87.3	79.3	71.7	63.8	56.9	61.4	54.9	48.4	41.8	35.7	0.41
6	69.9	63.6	57.3	51.0	45.5	49.2	43.9	38.7	33.5	28.5	0.60
7	58.2	53.0	47.8	42.5	38.0	41.0	36.6	32.3	27.9	23.8	0.81
8	49.9	45.4	40.9	36.4	32.5	35.1	31.4	27.6	23.9	20.4	1.06
9	43.7	39.7	35.8	31.9	28.5	30.7	27.5	24.2	20.9	17.8	1.34
10	38.8	35.3	31.8	28.3	25.3	27.3	24.4	21.5	18.6	15.9	1.66
	34.9	31.8	28.7	25.5	22.8	24.6	22.0	19.4	16.7	14.3	2.00
11	31.7	28.9	26.1	23.2	20.7	22.3	20.0	17.6	15.2	13.0	2.38
12	29.1	26.5	23.9	21.3	19.0	20.5	18.3	16.1	13.9	11.9	2.80
13	26.9	24.5	22.0	19.6	17.5	18.9	16.9	14.9	12.9	11.0	3.24
14	25.0	22.7	20.3	18.2	16.3	17.6	15.7	13.8	12.0	10.2	3.72
15	23.3	21.2	19.1	17.0	15.2	16.4	14.6	12.9	11.2	9.5	4.24
16	21.8	19.9	17.8	15.9	14.2	15.4	13.7	12.1	10.5	8.9	4.78
17	20.6	18.7	16.9	15.0	13.4	14.5	12.9	11.4	9.9	8.4	5.36
18	19.4	17.7	15.9	14.2	12.7	13.7	12.2	10.7	9.3	7.9	5.98
19	18.4	16.7	15.1	13.4	12.0	12.9	11.6	10.2	8.8	7.5	6.62
20	17.5	15.9	14.3	12.8	11.4	12.3	11.0	9.7	8.4	7.1	7.30
21	16.6	15.1	13.6	12.1	10.8	11.7	10.5	9.3	8.0	6.8	8.01
22	15.9	14.4	13.0	11.6	10.4	11.3	10.2	9.0	7.8	6.5	8.76
23	15.2	13.8	12.5	11.1	9.9						9.53
24	14.6	13.2	11.9	10.6	9.5						10.35
25	14.0	12.7	11.3	10.0	9.1						11.10
26	13.4	12.3	11.0	9.8	8.8						11.90

Loads in "heavy" type will produce maximum allowable shear in webs.  
 Loads in "light" type will produce excessive deflections.



## CHANNELS

## ALLOWABLE UNIFORM LOAD IN THOUSANDS OF POUNDS

Maximum Bending Stress: 16,000 Pounds per Square Inch

Span in Feet	Depth and Weight of Sections																Coefficient of Deflection
	9-inch				8-inch					7-inch							
	25 lbs.	20 lbs.	15 lbs.	10.4 lbs.	21.25 lbs.	18.75 lbs.	16.25 lbs.	13.75 lbs.	11.5 lbs.	19.75 lbs.	17.25 lbs.	14.75 lbs.	12.25 lbs.	9.8 lbs.			
	110.2	80.6			92.6	77.9	63.2	48.5			88.1	73.4	58.7	44.0			
2	83.6	71.8	51.3	41.4	63.0	54.3	45.0	35.8	26.2		59.4	50.8	41.5	32.7	23.4	13.07	
3	55.7	47.8	40.0	32.4	42.3	36.8	30.3	23.0	15.7		39.6	33.7	27.5	21.4	15.0	8.0	
4	41.8	35.9	29.0	23.0	31.7	27.1	22.0	16.9	11.0		29.2	24.9	20.0	15.3	10.7	5.27	
5	33.4	28.7	24.0	19.4	25.4	21.8	18.2	14.1	9.7		23.2	19.8	16.3	12.7	9.0	4.11	
6	27.9	23.9	20.0	16.7	21.2	18.4	15.7	12.9	8.4		19.4	16.5	13.7	10.2	7.7	3.40	
7	23.6	20.3	17.2	13.6	18.1	15.6	13.1	10.7	7.0		16.4	13.9	11.7	9.0	6.2	2.81	
8	20.9	17.9	15.0	11.9	15.9	13.6	11.3	9.0	6.0		14.6	12.4	10.3	8.0	5.0	2.34	
9	18.6	16.0	13.3	10.5	14.1	12.0	10.0	8.0	5.6		12.8	10.9	9.2	7.2	4.3	1.94	
10	16.7	14.4	12.0	9.7	12.7	11.7	10.0	8.6	6.6		11.1	9.2	7.8	6.0	3.8	1.66	
11	15.2	13.1	10.9	9.0	11.5	10.6	9.0	7.7	5.8		9.2	7.8	6.7	5.0	3.4	1.48	
12	13.9	12.0	10.0	8.3	10.6	9.7	8.3	6.9	5.2		8.4	7.0	6.0	4.5	3.0	1.34	
13	12.9	11.0	9.2	7.6	9.8	9.0	7.2	5.4	4.0		7.8	6.5	5.6	4.2	2.7	1.22	
14	11.9	10.3	8.6	6.9	9.1	8.3	6.6	4.8	3.6		7.2	6.0	5.2	3.9	2.4	1.12	
15	11.1	9.6	8.0	6.3	8.5	7.8	6.1	4.4	3.3		6.7	5.6	4.8	3.6	2.2	1.04	
16	10.4	9.0	7.5	5.9	7.9	7.3	5.6	4.0	3.1		6.2	5.2	4.4	3.3	2.0	0.97	
17	9.8	8.4	7.1	5.6	7.5	6.9	5.2	3.7	2.8		5.8	4.9	4.1	3.0	1.9	0.91	
18	9.3	8.0	6.7	5.2	7.1	6.5	4.9	3.5	2.6		5.4	4.5	3.8	2.7	1.8	0.86	
19	8.8	7.6	6.3	4.9												0.82	
20	8.4	7.2	6.0	4.6												0.78	

Span in Feet	Depth and Weight of Sections												Coefficient of Deflection (1/16 inch)	
	6-inch				5-inch			4-inch			3-inch			
	15.5 lbs.	13 lbs.	10.5 lbs.	8.2 lbs.	11.5 lbs.	9 lbs.	6.7 lbs.	7.25 lbs.	6.25 lbs.	5.4 lbs.	6 lbs.	5 lbs.		4.3 lbs.
					47.2			25.6			21.4	15.5		
1	67.1	62.4	37.7	24.0	44.3	32.8	19.0	24.3	19.8	14.4	14.7	13.0	10.2	0.002
2	44.6	40.7	26.8	17.3	29.1	21.8	13.4	16.1	13.1	10.1	7.3	6.5	5.3	0.007
3	33.1	30.5	19.8	13.4	21.7	16.5	10.0	12.1	9.4	7.7	5.3	4.7	3.9	0.014
4	27.3	25.3	16.4	11.6	18.0	13.8	8.4	10.1	8.0	6.5	4.7	4.2	3.5	0.027
5	23.8	22.3	14.7	10.2	15.8	12.3	7.3	8.9	7.1	5.8	4.2	3.7	3.1	0.044
6	21.3	19.8	13.0	8.9	14.4	11.0	6.5	8.1	6.6	5.3	3.9	3.4	2.8	0.060
7	19.9	18.4	11.9	7.6	13.1	9.9	5.4	7.5	6.2	5.0	3.7	3.2	2.6	0.084
8	18.6	17.2	11.0	6.7	12.0	9.1	4.7	6.9	5.7	4.6	3.5	3.0	2.4	0.106
9	17.7	16.3	10.4	6.1	11.0	8.2	4.3	6.7	5.5	4.4	3.3	2.8	2.2	0.134
10	16.9	15.6	9.9	5.4	10.4	7.8	3.9	6.3	5.2	4.1	3.1	2.6	2.0	0.160
11	16.3	15.0	9.4	4.9	9.8	7.4	3.6	5.9	4.9	3.8	2.9	2.4	1.9	0.188
12	15.8	14.5	9.0	4.5	9.3	7.0	3.3	5.6	4.6	3.6	2.7	2.2	1.8	0.214
13	15.3	14.1	8.6	4.1	8.9	6.7	3.0	5.3	4.4	3.3	2.5	2.0	1.6	0.240
14	14.9	13.7	8.3	3.8	8.5	6.4	2.8	5.1	4.2	3.1	2.3	1.8	1.5	0.264

Loads in "heavy" type will produce maximum allowable stress in web.

Loads in "light" type will produce excessive deflection.



## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Equal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Neutral Axis Parallel to Either Leg

For safe loads and deflections under various systems of loading, see explanation on page 32.

Size of Angle, Inches	Weight per Foot	Distance between Supports in Feet														
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
8 x 8 x 1 1/8	51.00		84240	56160	42120	33700	28080	24070	21060	18720	16850	15320	14040	12960	12030	11230
	45.00		74740	49840	37370	29000	24920	21360	18690	16610	14950	13590	12460	11500	10680	9970
	38.90		64980	43320	32490	25990	21660	18570	16250	14440	13000	11820	10830	10000	9280	8660
	32.70		54940	36620	27470	21980	18310	15700	13740	12210	10990	9990	9160	8450	7850	7330
	26.40	89240	44620	29760	22310	17850	14880	12750	11160	9920	8930	8110	7440	6870	6380	5950
6 x 6 x 1 1/8	33.10	81440	40720	27150	20360	16290	13570	11630	10180	9050	8140	7400	6790	6260	5820	5430
	28.70	71180	35540	23690	17770	14220	11850	10150	8890	7900	7110	6460	5920	5470	5080	4740
	24.20	60340	30170	20120	15090	12070	10060	8620	7540	6710	6030	5490	5030	4640	4310	4020
	19.60	49220	24610	16400	12300	9840	8200	7030	6150	5470	4920	4470	4100	3790	3520	3280
	14.90	37640	18820	12550	9410	7530	6270	5380	4700	4180	3760	3420	3140	2900	2690	2510
5 x 5 x 3/4	23.60	48320	24160	16100	12080	9660	8050	6900	6040	5360	4830	4390	4020	3710	3450	3220
	20.00	41140	20570	13710	10280	8230	6860	5880	5140	4570	4110	3740	3430	3160	2940	2740
	16.20	33660	16830	11220	8410	6730	5610	4810	4210	3740	3370	3060	2800	2590	2400	2240
	12.30	25820	12910	8610	6460	5170	4310	3690	3230	2780	2580	2350	2150	1990	1850	1720
	15.70	25620	12810	8540	6410	5130	4270	3660	3200	2850	2560	2330	2140	1970	1830	1710
4 x 4 x 3/4	12.80	21060	10530	7020	5270	4210	3510	3010	2630	2340	2110	1910	1760	1620	1500	1400
	9.80	16240	8120	5420	4060	3250	2710	2320	2030	1810	1620	1480	1350	1250	1160	1080
	8.20	13740	6870	4580	3430	2750	2290	1960	1720	1530	1370	1250	1140	1060	980	920

For lengths in "light" type, deflection will be less than  $\frac{1}{16}$ " in "heavy" type, more than  $\frac{1}{16}$ " in "diagonal" type more than  $\frac{1}{8}$ ".

## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Equal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.



## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Equal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Neutral Axis Parallel to Either Leg

For safe loads and deflections under various systems of loading, see explanation on page 32.

Size of Angle, Inches	Weight per Foot	Distance between Supports in Feet														
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
3½×3½×½	11.10	15880	7940	5290	3970	3180	2650	2270	1098	1760	1590	1440	1320	1220	1130	1060
	8.50	12280	6140	4100	3070	2460	2050	1760	1540	1370	1239	1120	1020	950	880	820
	5.80	8640	4320	2880	2160	1720	1440	1230	1080	960	860	780	720	660	610	570
3×3×½	9.40	11440	5720	3810	2860	2290	1910	1630	1430	1270	1140	1040	950	880	820	770
	7.20	8880	4440	2960	2220	1780	1480	1270	1110	990	890	810	740	680	630	590
	6.10	7540	3770	2510	1890	1510	1260	1080	940	840	750	690	630	580	540	510
2¾×2¾×½	4.90	6160	3080	2050	1540	1230	1030	880	770	680	620	560	510	470	430	400
	8.50	9480	4740	3160	2370	1900	1580	1360	1190	1050	950	860	790	730	680	640
	5.60	6280	3140	2090	1570	1260	1050	900	790	700	630	570	520	480	440	410
2½×2½×¾	3.39	3940	1970	1310	980	790	660	560	490	440	390	360	330	300	270	250
	5.90	6040	3020	2010	1510	1210	1010	860	760	670	600	550	500	460	420	390
	3.07	3220	1610	1080	810	650	540	460	400	360	320	290	270	240	220	200
2¼×2¼×¾	5.30	4820	2410	1610	1210	960	800	690	600	540	480	440	400	360	320	290
	2.75	2600	1300	870	650	520	430	370	320	290	260	240	220	200	180	160
	4.70	3740	1870	1250	940	750	620	540	470	420	370	340	310	280	250	230
2×2×¾	2.44	2040	1020	680	510	410	340	290	250	230	200	180	160	140	120	110

For lengths in "light" type, deflection will be less than  $\frac{3}{16}$ "; in "heavy" type, more than  $\frac{3}{16}$ "; in "italic" type, more than  $\frac{3}{8}$ ".



## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Unequal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Long Leg Vertical

For safe loads and deflections under various systems of loading, see explanation on page 32.

Size of Angle, Inches	Weight per Foot	Distance between Supports in Feet														
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
8 × 6 × $\frac{3}{4}$	33.80	62220	41480	31110	24890	20740	17770	15550	13820	12440	11310	10370	9570	8880	8290	
	28.50	52620	35080	26310	21050	17540	15040	13150	11690	10520	9570	8770	8090	7510	7010	
	23.00	42740	28490	21370	17090	14250	12210	10680	9500	8550	7770	7120	6570	6100	5700	
7 × 3½ × $\frac{5}{8}$	21.00	37140	24760	18570	14850	12380	10610	9280	8250	7430	6750	6190	5710	5310	4950	
	17.00	30280	20180	15140	12120	10100	8650	7570	6730	6060	5510	5050	4660	4330	4040	
	13.00	23090	15390	11540	9230	7690	6590	5770	5130	4610	4190	3840	3550	3290	3070	
6 × 4 × $\frac{5}{8}$	20.00	28320	18880	14160	11330	9440	8090	7080	6290	5660	5150	4720	4360	4050	3780	
	16.20	23120	15410	11560	9250	7710	6600	5780	5140	4620	4200	3850	3560	3300	3080	
	12.30	17700	11800	8850	7080	5900	5060	4420	3930	3540	3220	2950	2720	2530	2360	
6 × 3½ × $\frac{1}{2}$	18.90	27670	18450	13840	11070	9220	7910	6920	6150	5530	5030	4610	4260	3950	3690	
	15.30	22600	15060	11300	9040	7530	6460	5650	5020	4520	4110	3770	3480	3230	3010	
	11.70	17300	11540	8650	6920	5770	4940	4330	3850	3460	3150	2880	2660	2470	2310	
5 × 4 × $\frac{1}{2}$	14.70	16280	10850	8140	6510	5430	4650	4070	3620	3260	2960	2710	2500	2330	2170	
	11.00	12500	8330	6250	5000	4170	3570	3120	2780	2500	2270	2080	1920	1790	1670	
	8.60	15930	10620	7960	6370	5310	4550	3980	3540	3190	2900	2650	2450	2280	2120	
5 × 3½ × $\frac{1}{2}$	8.70	10320	6880	5160	4130	3440	2950	2580	2290	2060	1880	1720	1590	1470	1380	
	12.80	15510	10340	7760	6210	5170	4430	3880	3450	3100	2820	2590	2390	2220	2070	
	8.20	10160	6710	5030	4020	3350	2870	2520	2240	2010	1830	1680	1560	1440	1340	
For lengths in "heavy" type, the deflection is																

For lengths in "heavy" type, the deflection will be greater than  $\frac{1}{16}$ " ; in "light" type, greater than  $\frac{3}{8}$ ".

## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Unequal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Long Leg Vertical



## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Unequal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Long Leg Vertical

For safe loads and deflections under various systems of loading, see explanation on page 32.

Size of Angle, Inches	Weight per Foot	Distance between Supports in Feet														
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
4½×3 × ½ 16	11.90	25320	12660	8440	6330	5060	4220	3620	3170	2810	2530	2300	2110	1950	1810	1690
	7.70	16420	8210	5470	4100	3280	2730	2340	2050	1820	1640	1490	1360	1260	1170	1090
4 × 3½× ½ 16	11.90	20640	10320	6880	5160	4130	3440	2950	2580	2290	2060	1880	1720	1590	1470	1380
	7.70	13480	6740	4490	3370	2690	2250	1920	1680	1500	1350	1220	1120	1040	960	900
4 × 3 × ½ 16	11.10	20140	10070	6710	5040	4030	3360	2880	2520	2240	2010	1830	1680	1550	1440	1340
	7.20	13160	6580	4390	3290	2630	2190	1880	1640	1460	1320	1200	1100	1010	940	880
3½×3 × ½ 14	10.20	15500	7750	5170	3880	3100	2580	2220	1940	1720	1550	1410	1290	1190	1110	1030
	5.40	8420	4210	2800	2100	1680	1400	1200	1050	930	840	760	700	640	600	560
3½×2½× ½ 14	9.40	15060	7530	5020	3760	3010	2510	2150	1880	1670	1510	1370	1250	1160	1080	1000
	4.90	8040	4020	2680	2010	1610	1340	1150	1010	890	800	730	670	620	570	540
3 × 2½× ¾ 14	6.60	8640	4320	2880	2160	1730	1440	1230	1080	960	860	790	720	660	620	580
	4.50	5980	2990	2000	1500	1200	1000	860	750	670	600	540	500	460	430	400
3 × 2 × ¾ 14	5.90	8340	4170	2780	2080	1670	1390	1190	1040	930	830	760	690	640	600	560
	4.10	5780	2890	1930	1440	1160	960	830	720	640	580	530	480	440	410	380

For lengths in "heavy" type, the deflection will be greater than ⅜"; in "light" type greater than ⅜".



## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Unequal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Short Leg Vertical

For safe loads and deflections under various systems of loading, see explanation on page 32.

Size of Angle, Inches	Weight per Foot	Distance between Supports in Feet														
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
8 × 6 × $\frac{3}{4}$	33.80	73840	36920	24610	18460	14770	12310	10550	9320	8200	7380	6710	6150	5680	5270	4920
	28.50	62680	31340	20890	15670	12530	10440	8950	7830	6960	6260	5690	5220	4820	4470	4170
	23.00	55080	27540	18360	12770	10210	8510	7290	6380	5670	5100	4640	4250	3920	3640	3400
7 × 3½ × $\frac{5}{8}$	21.00	21040	10520	7010	5260	4210	3510	3010	2630	2340	2100	1910	1750	1620	1500	1400
	17.00	17280	8640	5760	4320	3460	2880	2470	2160	1920	1730	1570	1440	1330	1230	1150
	13.00	13970	6980	4650	3490	2790	2320	1990	1740	1550	1390	1270	1160	1070	990	930
6 × 4 × $\frac{5}{8}$	20.00	27040	13520	9020	6760	5410	4510	3860	3380	3010	2700	2460	2250	2080	1930	1800
	16.20	22200	11100	7400	5550	4440	3700	3170	2770	2470	2220	2020	1850	1710	1590	1480
	12.30	17100	8550	5700	4280	3420	2850	2440	2140	1900	1710	1550	1430	1320	1220	1140
6 × 3½ × $\frac{5}{8}$	18.90	20680	10340	6890	5170	4140	3450	2950	2580	2300	2070	1880	1720	1590	1480	1380
	15.30	17000	8500	5670	4250	3400	2830	2430	2120	1890	1700	1550	1420	1310	1210	1130
	11.70	13140	6570	4380	3280	2630	2190	1880	1640	1460	1310	1190	1090	1010	940	870
5 × 4 × $\frac{1}{2}$	14.50	21720	10860	7240	5430	4340	3620	3100	2710	2410	2170	1970	1810	1670	1550	1450
	11.00	16740	8370	5580	4180	3350	2790	2390	2090	1860	1670	1520	1390	1290	1200	1120
	8.60	16640	8320	5550	4160	3330	2770	2380	2080	1850	1660	1510	1390	1280	1190	1110
5 × 3½ × $\frac{1}{2}$	8.70	10900	5450	3630	2720	2180	1820	1560	1360	1210	1090	990	910	840	780	730
	12.80	12220	6110	4070	3060	2440	2040	1750	1530	1360	1220	1110	1020	940	870	810
	8.20	8040	4020	2680	2010	1610	1340	1150	1000	890	800	730	670	620	570	530

For lengths in "heavy" type, the deflection will be greater than  $\frac{3}{16}$ "; in "italic" type greater than  $\frac{3}{8}$ ".

## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Unequal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Short Leg Vertical



## STANDARD STEEL ANGLES

## SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED—For Unequal Leg Angles

Safe loads are figured for a fiber stress of 16,000 pounds per square inch, and include the weight of angle.

## Short Leg Vertical

For safe loads and deflections under various systems of loading, see explanation on page 32.

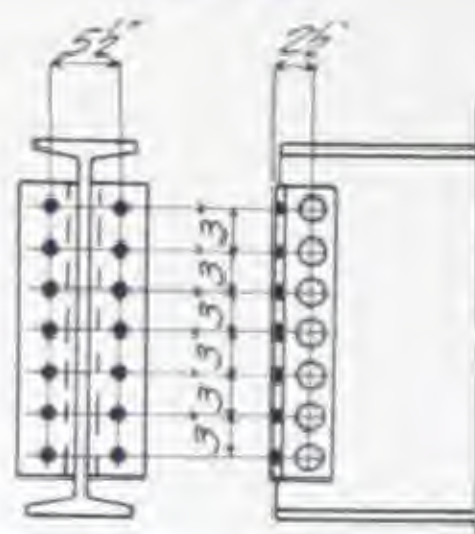
Size of Angle, Inches	Weight per Foot	Distance between Supports in Feet.														
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
4½×3 × ½ 16	11.90	12080	6040	4020	3020	2410	2010	1720	1510	1340	1210	1100	1010	930	860	
	7.70	8106	4050	2700	2020	1620	1350	1150	1010	900	810	730	670	620	570	
4 × 3½× ½ 16	11.90	16180	8090	5390	4040	3240	2700	2310	2020	1800	1620	1470	1350	1240	1160	
	7.70	10600	5300	3530	2650	2120	1770	1510	1320	1180	1060	960	880	820	760	
4 × 3 × ½ 16	11.10	11900	5950	3960	2970	2380	1980	1700	1490	1320	1190	1080	990	910	850	
	7.20	7840	3920	2610	1960	1570	1310	1120	980	870	780	710	650	600	560	
3½×3 × ½ 14	10.20	11680	5840	3900	2920	2340	1950	1670	1460	1300	1170	1060	970	900	830	
	5.40	7700	3850	2570	1930	1540	1280	1100	960	860	770	700	640	590	550	
3½×2½× ½ 14	9.40	8100	4050	2700	2030	1620	1350	1160	1010	900	810	740	680			
	4.90	4400	2200	1460	1100	880	730	630	550	490	440	400	370			
3 × 2½× ¾ 14	6.60	6200	3100	2060	1550	1240	1030	880	770	690	620	560	520			
	4.50	4320	2160	1440	1080	860	720	620	540	480	430	390	360			
3 × 2 × ¾ 14	5.90	3960	1980	1320	990	790	660	570	500	440	400	360	330			
	4.10	2780	1390	920	690	550	460	400	350	310	280	250	230			

For lengths in "heavy" type, the deflection will be greater than  $\frac{1}{16}$ "; in "dialic" type greater than  $\frac{3}{8}$ ".



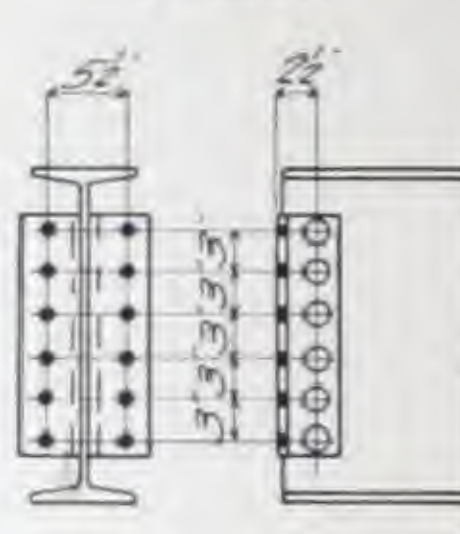
## STANDARD BEAM CONNECTIONS

27-INCH



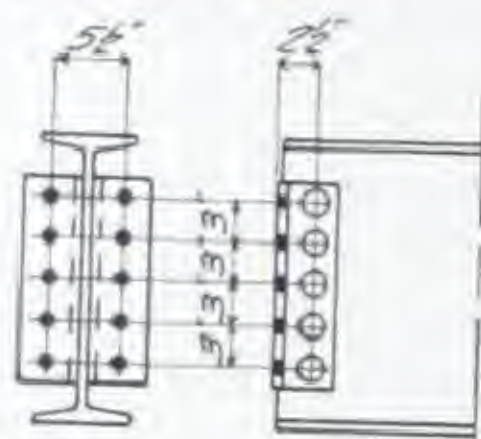
2 Angles 4" x 4" x 1/2" x 1'-8 1/2"  
Weight 46 lbs.

24-INCH



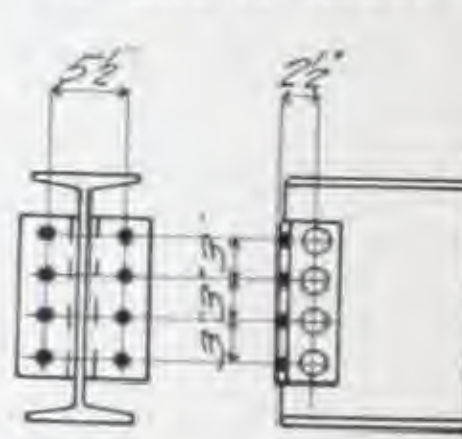
2 Angles 4" x 4" x 3/8" x 1'-5 1/2"  
Weight 30 lbs.

21- and 20-INCH



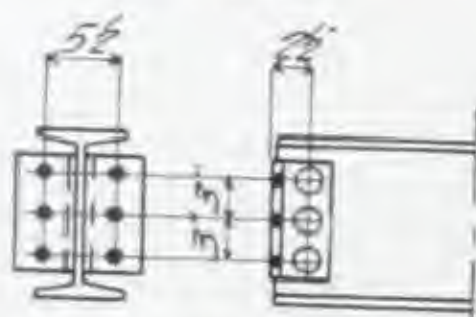
2 Angles 4" x 4" x 3/8" x 1'-2 1/2"  
Weight 25 lbs.

18- and 15-INCH



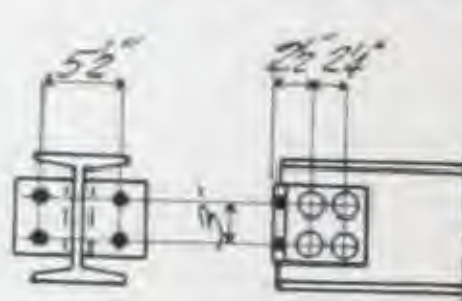
2 Angles 4" x 4" x 3/8" x 0'-11 1/2"  
Weight 20 lbs.

12-INCH



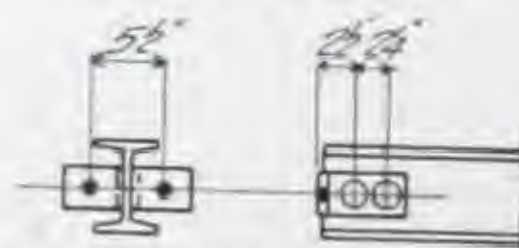
2 Angles 4" x 4" x 3/8" x 0'-8 1/2"  
Weight 15 lbs.

10-, 9- and 8-INCH



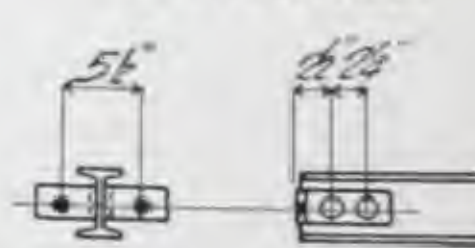
2 Angles 6" x 4" x 3/8" x 0'-5 1/2"  
Weight 13 lbs.

7-, 6- and 5-INCH



2 Angles 6" x 4" x 3/8" x 0'-3"  
Weight 7 lbs.

4- and 3-Inch



2 Angles 6" x 4" x 3/8" x 0'-2"  
Weight 5 lbs.

Rivets and bolts 3/4" diameter.

Weights given are for 3/4-inch shop rivets and angle connections; about 20 per cent should be added for field rivets or bolts.



### LIMITING VALUES OF CONNECTIONS FOR UNIFORMLY LOADED BEAMS

I-Beam		Strength of Web Connection with $\frac{3}{4}$ " Shop Rivets.		Strength of Outstanding Legs of Connection Angles with $\frac{3}{4}$ " Field Rivets	Minimum Span of Beam in feet.	$\frac{1}{16}$ " in inches
Depth in inches	Weight in lbs. per foot	Bearing in lbs.	Double Shear in lbs.	Single Shear in lbs.		
24	100		63,600	53,040	19.9	$\frac{5}{8}$
	79.9	56,250		53,040	17.5	$\frac{5}{8}$
20	81.4		42,400	35,360	22.1	$\frac{5}{8}$
	65.4	37,500		35,360	17.6	$\frac{5}{8}$
18	70		42,400	35,360	15.5	$\frac{5}{8}$
	54.7	34,500		35,360	13.7	$\frac{5}{8}$
15	81.3		42,400	35,360	16.0	$\frac{5}{8}$
	42.9	30,750		35,360	10.2	$\frac{9}{16}$
12	55		31,800	26,520	10.8	$\frac{9}{16}$
	31.8	19,665		26,520	9.8	$\frac{7}{16}$
10	40		42,400	17,680	9.6	$\frac{9}{16}$
	25.4	23,250		17,680	7.4	$\frac{5}{8}$
9	35		42,400	17,680	7.5	$\frac{5}{8}$
	21.8	21,750		17,680	5.7	$\frac{5}{8}$
8	25.5	40,575		17,680	5.2	$\frac{5}{8}$
	18.4	20,250		17,680	4.3	$\frac{3}{8}$
7	15.3	9,415		8,840	6.3	$\frac{5}{8}$
6	12.5	8,665		8,840	4.5	$\frac{5}{8}$
5	10	7,915		8,840	3.2	$\frac{9}{16}$
4	7.7	7,125		8,840	2.2	$\frac{1}{2}$
3	5.7	6,375		8,840	1.4	$\frac{7}{16}$

t = web thickness, for bearing if beams frame opposite, to develop strength of connection angles.

#### ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH:

##### Single Shear

Shop rivets—12,000

Field rivets—10,000

##### Bearing

Shop rivets—25,000

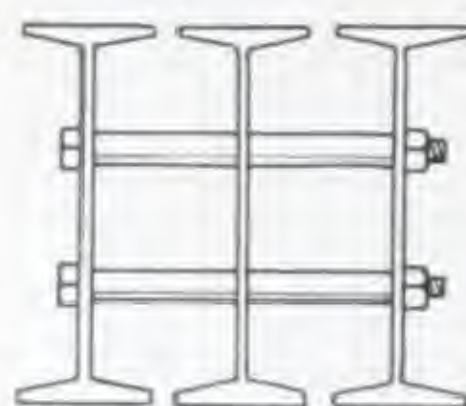
Field rivets—20,000



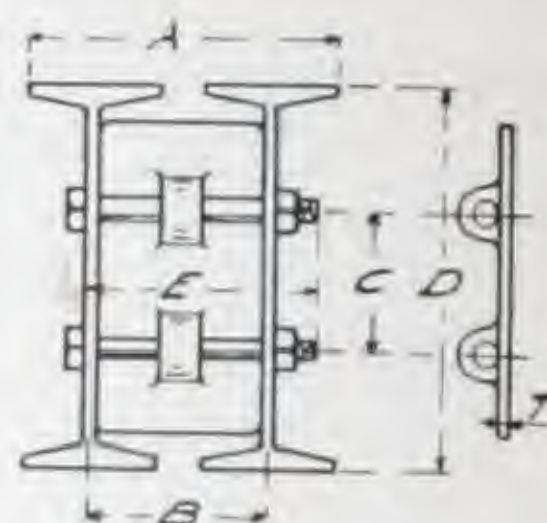
## BEAM SEPARATORS

Beam separators may be cast iron separators, pipe separators, or sometimes steel channels.

Pipe separators are used in many cases owing to their convenience of adjustment to any necessary size. Channels are limited in use, owing to the fact that they are obtainable only in exact inch sizes. Specifications for cast iron separators are given in the table below.



No. 11—Compound Beam with Pipe Separators



No. 12—Compound Beam with Cast Iron Separator

## SPECIFICATIONS FOR CAST IRON SEPARATORS

	BEAMS				SEPS.		BOLTS		
	D In.	Weight, Ft., Lbs.	A In.	B In.	T In.	Weight, Lbs.	C In.	E In.	Wt., Bolts & Nuts, Lbs.
ONE-BOLT SEPARATORS	3	5.7	5 $\frac{3}{8}$	3	3 $\frac{3}{8}$	1.1	...	4	.95
	4	7.7	5 $\frac{7}{8}$	3 $\frac{1}{4}$	3 $\frac{3}{8}$	1.6	...	4 $\frac{1}{2}$	1.01
	5	10.0	6 $\frac{1}{2}$	3 $\frac{1}{2}$	3 $\frac{3}{8}$	2.0	...	4 $\frac{3}{4}$	1.04
	6	12.5	7 $\frac{1}{8}$	4	3 $\frac{3}{8}$	3.3	...	5 $\frac{1}{4}$	1.11
	7	15.3	7 $\frac{3}{8}$	4 $\frac{1}{4}$	3 $\frac{3}{8}$	3.9	...	5 $\frac{1}{2}$	1.14
	8	18.4	8 $\frac{1}{2}$	4 $\frac{1}{2}$	3 $\frac{3}{8}$	4.7	...	5 $\frac{3}{4}$	1.17
	9	21.8	9 $\frac{1}{8}$	5	3 $\frac{3}{8}$	5.9	...	6 $\frac{1}{4}$	1.23
	10	25.4	9 $\frac{3}{8}$	5 $\frac{1}{4}$	3 $\frac{3}{8}$	6.8	...	6 $\frac{1}{2}$	1.26
	12	31.8	10 $\frac{3}{4}$	5 $\frac{3}{4}$	3 $\frac{3}{8}$	8.8	...	7	1.32
	12	40.8	11 $\frac{3}{4}$	6	3 $\frac{3}{8}$	8.9	...	7 $\frac{1}{2}$	1.38
TWO-BOLT SEPARATORS	12	31.8	10 $\frac{3}{4}$	5 $\frac{3}{4}$	3 $\frac{3}{8}$	9.5	6 $\frac{1}{2}$	7	2.64
	12	40.8	11 $\frac{3}{4}$	6	3 $\frac{3}{8}$	9.5	6 $\frac{1}{2}$	7 $\frac{1}{2}$	2.76
	15	42.9	11 $\frac{3}{4}$	6 $\frac{1}{4}$	3 $\frac{3}{8}$	12.5	7	7 $\frac{3}{4}$	2.82
	15	60.8	12 $\frac{3}{4}$	6 $\frac{3}{4}$	3 $\frac{3}{8}$	13.0	7	8 $\frac{1}{4}$	2.95
	15	65	13 $\frac{3}{8}$	7 $\frac{1}{4}$	3 $\frac{3}{8}$	13.2	7	9	3.13
	18	54.7	12 $\frac{3}{4}$	6 $\frac{3}{4}$	3 $\frac{3}{8}$	19.8	9	8 $\frac{1}{4}$	2.95
	20	65.4	13 $\frac{1}{4}$	7	3 $\frac{3}{8}$	22.9	10	8 $\frac{1}{2}$	3.01
	20	81.4	14 $\frac{3}{4}$	7 $\frac{3}{4}$	3 $\frac{3}{8}$	24.6	10	9 $\frac{1}{4}$	3.19
	24	79.9	14 $\frac{3}{4}$	7 $\frac{3}{4}$	3 $\frac{3}{8}$	30.3	12	9 $\frac{3}{4}$	3.19

Dimensions given in above table refer to cut No. 12. Square head bolts,  $\frac{3}{4}$ -inch diameter, with nuts are used. Lengths and weights of separator bolts in above table are for girders composed of two beams of minimum section as shown.



## STEEL BEARING PLATES

BEAM		Wall Bear- ing, Inches	Size in inches	Weight in Pounds	Common brick with lime mortar 100 lbs. per sq. in. bearing pressure		Hard common select- brick, mortar 1 part Portland cement, 1 lime, 3 torpedo sand, 175 lbs. per sq. in. bearing pressure.		Portland cement concrete 1-2-4 mix. Machine mixed, 400 lbs. per sq. in. bear- ing pressure.		Common Size C. I. Bearing Plates	
Depth, In.	Wt., Lbs., per Ft.				Safe Load in 1000 lbs. on one Plate	Limiting Span in feet and inches	Safe Load in 1000 lbs. on one Plate	Limiting Span in feet and inches	Safe Load in 1000 lbs. on one Plate	Limiting Span in feet and inches	Size in inches	Weight including 2 per cent for over- weight
24	79.9	16	16x16x1	73	25.6	36'0"	44.8	20'9"	67.3	13'6"	16x16x2	136
20	65.4	16	16x16x1	73	25.6	24'6"	44.8	14'0"	60.5	10'3"	16x16x1 $\frac{3}{4}$	119
18	54.7	16	16x16x1	73	25.6	18'6"	44.8	10'6"	54.8	8'6"	16x16x1 $\frac{3}{4}$	119
15	42.9	12	12x16x $\frac{3}{4}$	41	19.2	16'0"	20.9	15'0"	20.9	15'0"	12x16x1 $\frac{1}{4}$	64
12	31.8	12	12x12x $\frac{3}{4}$	31	14.4	13'3"	25.2	7'6"	35.3	5'3"	12x12x1 $\frac{1}{4}$	48
10	25.4	8	8x12x $\frac{5}{8}$	17	9.6	13'6"	14.9	8'9"	14.9	8'9"	8x12x1	25
9	21.8	8	8x12x $\frac{5}{8}$	17	9.6	10'6"	13.6	7'6"	13.6	7'6"	8x12x1	25
8	18.4	8	8x8x $\frac{5}{8}$	12	6.4	11'9"	11.2	6'9"	25.6	3'0"	8x8x1	17
7	15.3	8	8x8x $\frac{5}{8}$	12	6.4	8'9"	11.2	4'9"	25.6	3'0"	8x8x1	17
6	12.5	6	6x6x $\frac{1}{2}$	5	3.6	10'9"	6.3	6'3"	14.4	2'0"	6x6x $\frac{3}{4}$	7
5	10	6	6x6x $\frac{1}{2}$	5	3.6	7'0"	6.3	4'0"	14.4	2'0"	6x6x $\frac{3}{4}$	7

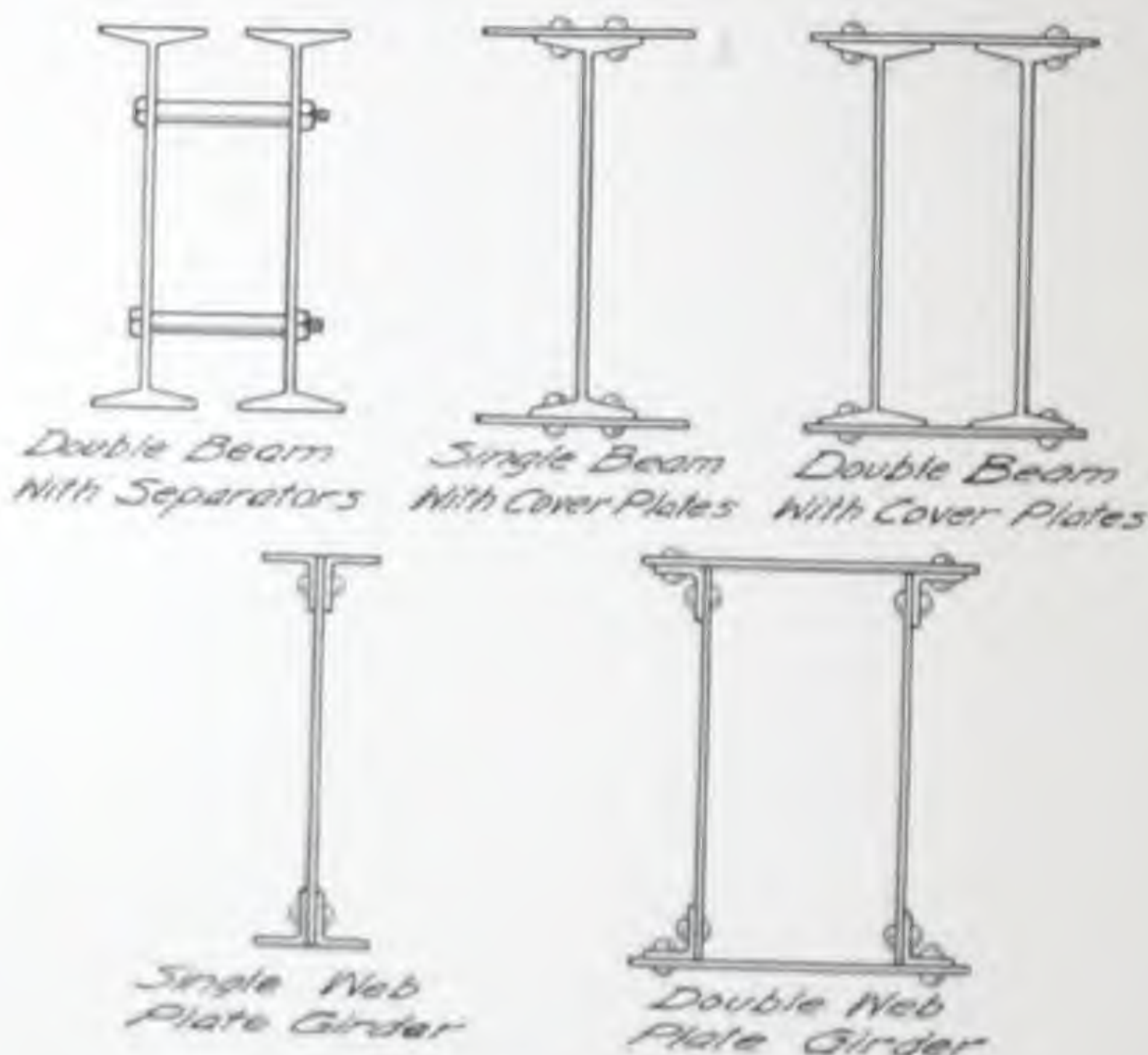


## BEAM AND PLATE AND ANGLE GIRDERS

Where single rolled beams are insufficient to carry the loads, the required capacity may be obtained by various methods.

Two beams, connected with bolts and cast iron separators, or, for greater rigidity, with rivetted plate and angle separators, can be used. The total strength of these is twice that of the single beam provided that the loads are applied equally on the two sections, otherwise their strength must be computed separately.

Single beam girders with plates rivetted on top and bottom are often more economical than two beams connected with separators.



No. 12—Typical Girder Sections

Box girders formed of two beams with plates rivetted across the beam flanges are frequently used for supporting interior walls in buildings, but they are not so economical as single beams with flange plates or as plate girders. Box girders should not be used in exposed places, as their interior surfaces do not admit of repainting.

The most economical section is the single web plate girder, if not of sufficient strength, two single web plate girders may be used, with tie plates extending across the angles, or box girders may be made of four flange angles, two web plates and top and bottom flange plates. If the loads are not equally distributed, the two half-girders must be figured as separate units.

In the design of beam or plate girders the web must be of sufficient thickness to resist buckling stress or angle stiffeners must be provided. We will be pleased to supply designs for rivetted girders to take any specified loading.



## FOUNDATIONS

**Foundation Loads.**—Footings should be so designed that the loads they sustain per unit of area shall be as nearly uniform as possible, and the dead loads carried by the footings should include the actual weight of the superstructure and foundations down to the bottom of the footing. The live load should be assumed to be the same as the live load in the lowest tier of columns or in the footings under walls. The area of the footing is determined by dividing the total load by the unit resistance of the soil. From the area thus calculated all the other footings of the building are proportioned according to the ratios of their respective dead loads only. In no case should the load per square foot under any portion of any footing due to the combined dead, live and wind loads, exceed the safe sustaining power of the soil upon which the footing rests.

**Bearing Power of Soils.**—The bearing power of a soil depends upon the character of the soil, its freedom from water, and its lateral support. The downward pressure of the surrounding soil prevents lateral displacement of the material under the foundation and adds materially to the bearing power of treacherous soils.

The allowable pressures given in the table below may be used as an aid to the judgment in determining on a safe load for a foundation. However, no important foundations should be built without making careful soundings and bearing tests.

A soil incapable of supporting the required loads may have its supporting power increased (1) by increasing the depth of the foundation; (2) by draining the site; (3) by compacting the soil; (4) by adding a layer of sand or gravel; (5) by using grillages to increase the bearing area; (6) by driving piles through the soft stratum, or far enough into it to support the loads.

When foundations are placed on sand, gravel or clay, it is usually only necessary to dig a trench and start the foundation below frost. If the soil is somewhat yielding or if the load is heavy, the foundation should be carried to a greater depth, or the footing should be made wider than for greater depths.

The placing of three or four reinforcing rods continuous around wall footings is advantageous as it prevents the common cracking in foundation walls due to unequal settlement caused by the fact that soil is not uniform in any area.

**Allowable Foundation Pressures.**—The following unit pressures for foundations have been proposed by Schneider in "Structural Design of Buildings":

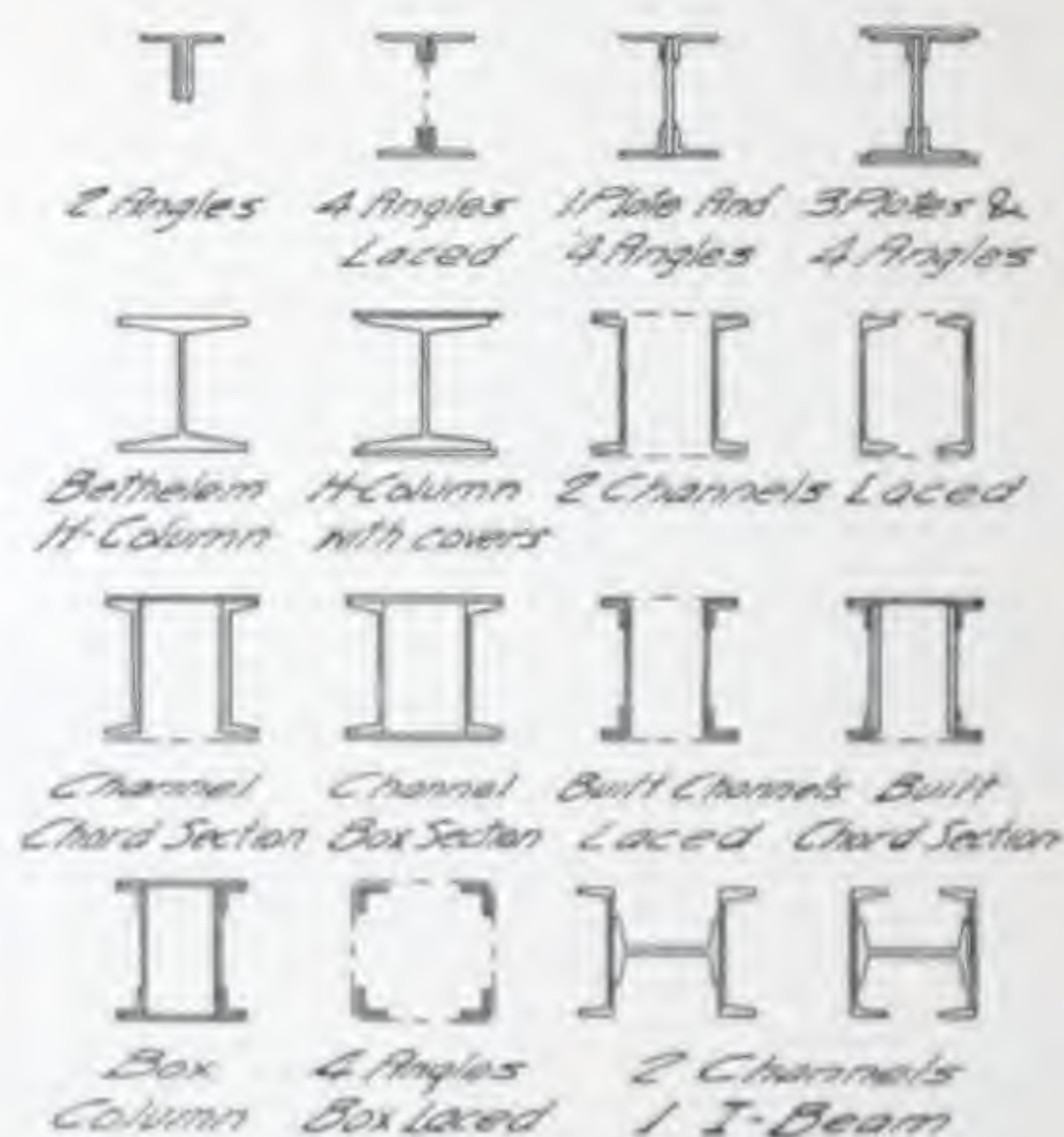
MAXIMUM FOUNDATION PRESSURES

Kind of Material	Tons per Square Foot
Alluvial Soils.....	.5
Soft clay.....	1
Ordinary clay and dry sand mixed with clay.....	2
Dry sand and dry clay.....	3
Hard clay and firm, coarse sand.....	4
Firm, coarse sand and gravel.....	6
Rock.....	5 to 200



## STEEL COLUMNS

**Form and Size of Section.**—Important as it may be to have the metal of the column section distributed as far as possible from the neutral axis, that is with as large a radius of gyration as possible, considerations of ease in fabrication and simplicity in connections are of greater weight. The economical column section is not that which affords the least weight of metal in the shaft, but that which, with a reasonable radius of gyration, provides the least weight of member, shaft and details with the minimum amount of riveting. Modern practice therefore, eliminates earlier forms of construction which represented the minimum amount of metal for the maximum radius of gyration, such, for example, as the column composed of three I-beams or one I-beam and two channels placed either with the flanges in or the flanges out. The Z-bar column has also fallen into disuse likewise a number of patented sections. The column sections should be of such size as to permit ready framing of beams and girders thereto and so



No. 14—Common Forms of Cross Section for Steel Columns and Struts.

placed in the construction as to permit the simplest details. Experience indicates that eight inches is the smallest desirable dimension in ordinary building work. For struts and light loads, smaller angle columns are still in use, while H-beams are excellent for such purposes. I-beams and single angles may be used with economy where the conditions of lengths and loading permit.

**Design.**—Column loads to be calculated in the design of ordinary columns for buildings are dead loads, including snow loads, and live loads. There are other loads such as impact, wind load etc., which are for particular cases and need not be considered here. The dead load is the load produced by the weight of floors, curtain walls, roof, steel etc., and can be accurately calculated. The live load depends on the use of which the building is to be put, and includes the weight of persons, furniture, goods and equipment. In determining the loads due to occupancy of stores and office buildings considerable judgment must be exercised. Since it is very improbable that the full live load will be imposed on all floors simultaneously, the loads used in calculating the strength of floor beams may be reduced for the calculation of column stresses.

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For columns carrying more than five floors, live loads may be reduced as follows.

For roof and top floor, no reduction.

For each succeeding floor a reduction of 5% until 50% is reached, which load shall be used for all succeeding floors. This reduction does not apply for warehouses, which are likely to be loaded on all floors simultaneously.

**Radius of Gyration.**—As the strength of a column depends on its ability to resist flexural stress, the moment of inertia of its cross section is an important factor in the determination of its carrying capacity. For the purpose of calculation, however, it is much more convenient to use the radius of gyration which depends on the moment of inertia.

**Ratio of Slenderness.**—The ratio of slenderness is ratio of the unsupported length of a compression member to its radius of gyration; generally the least radius prevailing when the unsupported length of a column is rigidly fixed in such a manner as to prevent deflection of the column in the direction which corresponds to the least radius of gyration. Columns, excepting those of square or circular section, have two principal radii of gyration. It is, therefore, necessary to determine the radii of gyration of such columns and to use the proper ratio of slenderness in any particular case. The unsupported length of a compression member should never exceed 200 times its least radius of gyration. The following are generally recognized as the upper limits of the value of  $L/r$  where  $L$  = unsupported length in inches and  $r$  = least radius of gyration.

For lateral struts carrying wind stresses only, in buildings.	120 to 200
For lateral struts carrying wind stresses only, in bridges.	120 to 150
For columns in buildings with girders or beams.	120 to 150
For compression members in bridges.	100 to 120

**Explanation of Tables.**—The tables which immediately follow give the safe loads in thousands of pounds on I-beam columns which, in the light of experience, are most desirable for use in ordinary building construction. In addition to the safe loads, they give least radii of gyration, areas of sections, and weights in pounds per foot. For safe loads on I-beam columns and Carnegie H-sections, see page 9. For Bethlehem columns see pages 50 to 55.

**Combined Bending and Compression Stresses.**—It is assumed in the tables that the loads are direct and axially distributed over the cross section of the column or balanced on opposite sides thereof. In the case of loads carried on brackets or other forms of eccentric loading, bending stresses are produced which should be taken into consideration and the column sections so proportioned that the resultant fiber stresses do not exceed the allowable axial compressive stresses.



SAFE LOADS, IN TONS OF 2000 LBS., FOR  
BETHLEHEM ROLLED STEEL  
8 In. H COLUMNS—SQUARE ENDS

Allowable stress per square inch:

13,000 lbs. for lengths under 55 radii. 16,000—55-1/r for lengths over 55 radii.



Dimensions, Inches				Area of Section, Square Inches	Least Radius of Gyration, Inches	UNSUPPORTED LENGTH OF COLUMNS												Weight of Section, Lbs. per Foot			
D	T	B				8	9	10	11	12	13	14	15	16	17	18	20		22	24	26
Weight of Section, Lbs. per Foot																					
32.0	7 7/8	1 1/8	8.00	9.17	1.08	59.7	59.7	58.1	56.5	55.0	53.5	52.0	50.4	48.9	47.4	45.9	42.8	39.7	36.7	32.0	
34.5	8	1 1/2	8.00	10.17	2.01	66.1	66.1	64.7	63.0	61.3	59.7	58.0	56.3	54.6	53.0	51.3	48.0	44.6	41.3	38.0	34.5
39.0	8 1/8	1 5/8	8.04	11.50	2.03	74.8	74.8	73.3	71.4	69.6	67.7	65.8	64.0	62.1	60.2	58.4	54.6	50.9	47.1	43.4	39.0
43.5	8 1/4	1 3/4	8.08	12.83	2.04	83.4	83.4	81.9	79.8	77.7	75.7	73.6	71.5	69.4	67.4	65.3	61.1	57.0	52.8	48.7	43.5
48.0	8 3/8	1 1/2	8.12	14.18	2.05	92.2	92.2	90.6	88.3	86.1	83.8	81.5	79.2	76.9	74.6	72.4	67.8	63.2	58.7	54.1	48.0
53.0	8 1/2	1 3/4	8.16	15.53	2.07	101.0	101.0	99.5	97.0	94.5	92.1	89.6	87.1	84.6	82.2	79.7	74.7	69.8	64.8	59.9	53.0
57.5	8 5/8	1 1/2	8.20	16.90	2.08	109.9	109.9	108.4	105.7	103.0	100.3	97.7	95.0	92.3	89.6	86.9	81.6	76.2	70.9	65.5	57.5
62.0	8 3/4	1 3/8	8.24	18.27	2.09	118.8	118.8	117.3	114.4	111.5	108.7	105.8	102.9	100.0	97.1	94.2	88.5	82.7	76.9	71.2	62.0
67.0	8 7/8	1 1/4	8.28	19.66	2.11	127.8	127.8	126.5	123.5	120.4	117.3	114.2	111.1	108.0	105.0	101.9	95.8	89.6	83.5	77.3	67.0
71.5	9	1	8.32	21.05	2.12	136.8	136.8	135.6	132.4	129.1	125.8	122.5	119.2	116.0	112.7	109.4	102.9	96.3	89.8	83.2	71.5
76.5	9 1/8	1 1/8	8.36	22.46	2.13	146.0	146.0	144.9	141.4	137.9	134.4	131.0	127.5	124.0	120.5	117.0	110.1	103.1	96.2	89.2	76.5
81.0	9 1/4	1 1/8	8.39	23.78	2.14	154.6	154.6	153.6	149.9	146.4	142.9	139.4	135.9	132.4	128.9	125.4	118.6	111.6	104.6	97.6	81.0
85.5	9 3/8	1 3/8	8.43	25.20	2.16	163.8	163.8	163.3	159.3	155.8	152.3	148.8	145.3	141.8	138.3	134.8	128.0	121.0	114.0	107.0	85.5
90.5	9 1/2	1 1/4	8.47	26.64	2.17	173.2	173.2	172.2	168.2	164.7	161.2	157.7	154.2	150.7	147.2	143.7	136.9	129.9	122.9	115.9	90.5

Loads in "light" type are for lengths less than 125 radii; loads in "heavy" type are for lengths greater than 125 radii.

For loads on Carnegie 4" to 8" H columns, see page 9.

SAFE LOADS, IN TONS OF 2000 LBS., FOR  
BETHLEHEM ROLLED STEEL  
10 In. H-COLUMNS—SQUARE ENDS





SAFE LOADS, IN TONS OF 2000 LBS., FOR  
BETHLEHEM ROLLED STEEL  
NO. 16, H-COLUMNS, SQUARE ENDS

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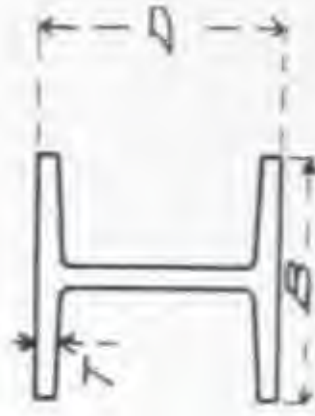
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SAFE LOADS, IN TONS OF 2000 LBS., FOR  
BETHLEHEM ROLLED STEEL  
12 In. H-COLUMNS—SQUARE ENDS

Allowable stress per square inch:

13,000 lbs. for lengths under 55 radii,      16,000—55-1/r for lengths over 55 radii.



Weight of Section, Lbs. per Foot.	Dimensions, Inches			Area of Section, Square Inches.	Least Radius of Gyration, Inches.	UNSUPPORTED LENGTH OF COLUMNS												Weight of Section, Lbs. per Foot.			
	D	T	B			12 Ft.	12 Ft.	14 Ft.	16 Ft.	18 Ft.	20 Ft.	22 Ft.	24 Ft.	26 Ft.	28 Ft.	30 Ft.	32 Ft.		34 Ft.	36 Ft.	38 Ft.
64.5	11 3/4	3/8	11.92	19.00	2.98	123.5	123.5	5123.5	122.5	118.3	114.1	109.9	105.7	101.5	97.3	93.1	88.9	84.7	80.5	76.3	64.5
71.5	11 3/4	1/2	11.96	20.96	3.00	136.2	136.2	2136.2	135.4	130.8	126.2	121.6	117.0	112.4	107.8	103.1	98.5	93.9	89.3	84.7	71.5
78.0	12	3/4	12.00	22.94	3.01	149.1	149.1	1149.1	148.3	143.3	138.3	133.2	128.2	123.2	118.1	113.1	108.1	103.0	98.0	93.0	78.0
84.5	12 1/8	1	12.04	24.92	3.03	162.0	162.0	162.0	161.4	155.9	150.5	145.1	139.7	134.2	128.8	123.4	117.9	112.5	107.1	101.7	84.5
91.5	12 1/4	1 1/8	12.08	26.92	3.04	175.0	175.0	175.0	174.5	168.8	162.8	156.9	151.1	145.2	139.4	133.5	127.7	121.9	116.0	110.2	91.5
98.5	12 3/8	1 1/4	12.12	28.92	3.06	188.0	188.0	188.0	187.7	181.5	175.5	169.9	164.2	158.6	153.0	147.4	141.8	136.2	130.6	125.0	98.5
105.0	12 1/2	1 1/2	12.16	30.94	3.07	201.0	201.0	201.0	201.0	194.3	187.7	181.1	174.5	167.9	161.3	154.7	148.1	141.5	134.9	128.3	105.0
112.0	12 5/8	1 3/4	12.20	32.96	3.08	214.0	214.0	2214.2	2207.2	2200.1	2193.1	2186.0	2178.9	2171.8	2164.7	2157.6	2150.5	2143.4	2136.3	2129.2	112.0
118.5	12 3/4	1 3/8	12.23	34.87	3.10	226.0	226.0	7226.7	7219.6	7212.4	7205.2	7197.9	7190.7	7183.5	7176.3	7169.1	7161.9	7154.7	7147.5	7140.3	118.5
125.5	12 7/8	1 3/4	12.27	36.91	3.11	239.0	239.0	9239.9	9232.8	9225.6	9218.4	9211.2	9204.0	9196.8	9189.6	9182.4	9175.2	9168.0	9160.8	9153.6	125.5
132.5	13	1 3/4	12.31	38.97	3.13	253.0	253.0	3253.3	3246.0	3238.7	3231.4	3224.1	3216.8	3209.5	3202.2	3194.9	3187.6	3180.3	3173.0	3165.7	132.5
139.5	13 1/8	1 3/8	12.35	41.03	3.14	266.0	266.0	7266.7	7259.3	7251.9	7244.5	7237.1	7229.7	7222.3	7214.9	7207.5	7199.9	7192.4	7184.9	7177.4	139.5
146.5	13 1/4	1 3/8	12.39	43.10	3.15	280.0	280.0	2280.2	2272.6	2265.0	2257.4	2249.8	2242.2	2234.6	2227.0	2219.4	2211.8	2204.2	2196.6	2189.0	146.5
153.5	13 3/8	1 3/8	12.43	45.19	3.16	293.0	293.0	7293.7	7286.0	7278.3	7270.6	7262.9	7255.2	7247.5	7239.8	7232.1	7224.4	7216.7	7209.0	7201.3	153.5
161.0	13 1/2	1 3/2	12.47	47.28	3.18	307.0	307.0	3307.3	3299.7	3292.0	3284.3	3276.6	3268.9	3261.2	3253.5	3245.8	3238.1	3230.4	3222.7	3215.0	161.0

Loads in "light" type are for lengths less than 125 radii; loads in "heavy" type are for lengths greater than 125 radii.

SAFE LOADS, IN TONS OF 2000 LBS., FOR  
BETHLEHEM ROLLED STEEL  
14 In. H-COLUMNS—SQUARE ENDS

Allowable stress per square inch:





SAFE LOADS, IN TONS OF 2000 LBS., FOR  
BETHLEHEM ROLLED STEEL  
14 IN. H-COLUMNS—SQUARE ENDS

Allowable stress per square inch:

13,000 lbs. for lengths under 55 radii, 16,000—55-1/2 for lengths over 55 radii.

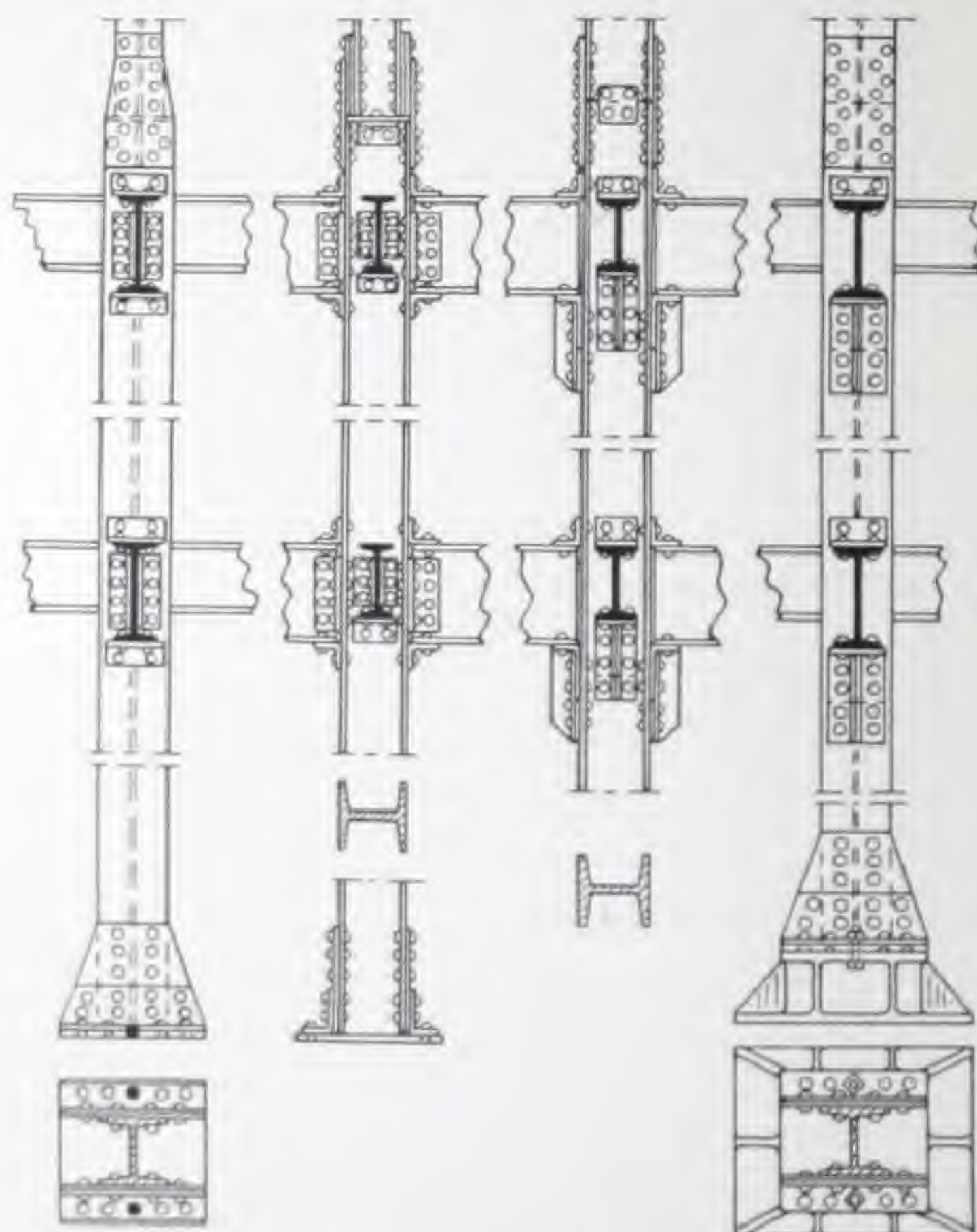


Weight of Section, Lbs. per Foot	Dimensions, In.			Area of Square Ends, Sq. In.	Least radius of Gy- ration, Inches	UNSUPPORTED LENGTH OF COLUMNS													Weight of Section, Lbs. per Foot	
	D	T	B			10 In.	12 In.	14 In.	16 In.	18 In.	20 In.	22 In.	24 In.	26 In.	28 In.	30 In.	32 In.	36 In.		40 In.
83.0	10 1/4	1 1/2	14 1/2	24.46	3.47	170.0	150.0	135.0	120.0	105.0	90.0	75.0	60.0	45.0	30.0	15.0	12.0	11.0	10.2	8.3
91.0	11 1/4	1 1/2	15 1/2	26.76	3.49	175.0	155.0	140.0	125.0	110.0	95.0	80.0	65.0	50.0	35.0	20.0	13.0	12.2	11.2	9.1
99.0	12 1/4	1 1/2	16 1/2	29.06	3.50	180.0	160.0	145.0	130.0	115.0	100.0	85.0	70.0	55.0	40.0	25.0	14.0	13.0	12.2	10.0
106.0	13 1/4	1 1/2	17 1/2	31.36	3.52	185.0	165.0	150.0	135.0	120.0	105.0	90.0	75.0	60.0	45.0	30.0	15.0	14.0	13.0	106.0
114.0	14 1/4	1 1/2	18 1/2	33.70	3.53	190.0	170.0	155.0	140.0	125.0	110.0	95.0	80.0	65.0	50.0	35.0	16.0	15.0	14.0	114.0
122.0	15 1/4	1 1/2	19 1/2	36.04	3.55	195.0	175.0	160.0	145.0	130.0	115.0	100.0	85.0	70.0	55.0	40.0	17.0	16.0	15.0	122.0
130.0	16 1/4	1 1/2	20 1/2	38.38	3.56	200.0	180.0	165.0	150.0	135.0	120.0	105.0	90.0	75.0	60.0	45.0	18.0	17.0	16.0	130.0
138.0	17 1/4	1 1/2	21 1/2	40.72	3.58	205.0	185.0	170.0	155.0	140.0	125.0	110.0	95.0	80.0	65.0	50.0	19.0	18.0	17.0	138.0
146.0	18 1/4	1 1/2	22 1/2	43.06	3.59	210.0	190.0	175.0	160.0	145.0	130.0	115.0	100.0	85.0	70.0	55.0	20.0	19.0	18.0	146.0
154.0	19 1/4	1 1/2	23 1/2	45.40	3.61	215.0	195.0	180.0	165.0	150.0	135.0	120.0	105.0	90.0	75.0	60.0	21.0	20.0	19.0	154.0
162.0	20 1/4	1 1/2	24 1/2	47.74	3.62	220.0	200.0	185.0	170.0	155.0	140.0	125.0	110.0	95.0	80.0	65.0	22.0	21.0	20.0	162.0
170.0	21 1/4	1 1/2	25 1/2	50.08	3.64	225.0	205.0	190.0	175.0	160.0	145.0	130.0	115.0	100.0	85.0	70.0	23.0	22.0	21.0	170.0
178.0	22 1/4	1 1/2	26 1/2	52.42	3.65	230.0	210.0	195.0	180.0	165.0	150.0	135.0	120.0	105.0	90.0	75.0	24.0	23.0	22.0	178.0
186.0	23 1/4	1 1/2	27 1/2	54.76	3.66	235.0	215.0	200.0	185.0	170.0	155.0	140.0	125.0	110.0	95.0	80.0	25.0	24.0	23.0	186.0
194.0	24 1/4	1 1/2	28 1/2	57.10	3.68	240.0	220.0	205.0	190.0	175.0	160.0	145.0	130.0	115.0	100.0	85.0	26.0	25.0	24.0	194.0
202.0	25 1/4	1 1/2	29 1/2	59.44	3.69	245.0	225.0	210.0	195.0	180.0	165.0	150.0	135.0	120.0	105.0	90.0	27.0	26.0	25.0	202.0
210.0	26 1/4	1 1/2	30 1/2	61.78	3.70	250.0	230.0	215.0	200.0	185.0	170.0	155.0	140.0	125.0	110.0	95.0	28.0	27.0	26.0	210.0
218.0	27 1/4	1 1/2	31 1/2	64.12	3.71	255.0	235.0	220.0	205.0	190.0	175.0	160.0	145.0	130.0	115.0	100.0	29.0	28.0	27.0	218.0
226.0	28 1/4	1 1/2	32 1/2	66.46	3.72	260.0	240.0	225.0	210.0	195.0	180.0	165.0	150.0	135.0	120.0	105.0	30.0	29.0	28.0	226.0
234.0	29 1/4	1 1/2	33 1/2	68.80	3.74	265.0	245.0	230.0	215.0	200.0	185.0	170.0	155.0	140.0	125.0	110.0	31.0	30.0	29.0	234.0
242.0	30 1/4	1 1/2	34 1/2	71.14	3.75	270.0	250.0	235.0	220.0	205.0	190.0	175.0	160.0	145.0	130.0	115.0	32.0	31.0	30.0	242.0
250.0	31 1/4	1 1/2	35 1/2	73.48	3.76	275.0	255.0	240.0	225.0	210.0	195.0	180.0	165.0	150.0	135.0	120.0	33.0	32.0	31.0	250.0
258.0	32 1/4	1 1/2	36 1/2	75.82	3.77	280.0	260.0	245.0	230.0	215.0	200.0	185.0	170.0	155.0	140.0	125.0	34.0	33.0	32.0	258.0
266.0	33 1/4	1 1/2	37 1/2	78.16	3.78	285.0	265.0	250.0	235.0	220.0	205.0	190.0	175.0	160.0	145.0	130.0	35.0	34.0	33.0	266.0
274.0	34 1/4	1 1/2	38 1/2	80.50	3.79	290.0	270.0	255.0	240.0	225.0	210.0	195.0	180.0	165.0	150.0	135.0	36.0	35.0	34.0	274.0
282.0	35 1/4	1 1/2	39 1/2	82.84	3.80	295.0	275.0	260.0	245.0	230.0	215.0	200.0	185.0	170.0	155.0	140.0	37.0	36.0	35.0	282.0
290.0	36 1/4	1 1/2	40 1/2	85.18	3.81	300.0	280.0	265.0	250.0	235.0	220.0	205.0	190.0	175.0	160.0	145.0	38.0	37.0	36.0	290.0
298.0	37 1/4	1 1/2	41 1/2	87.52	3.82	305.0	285.0	270.0	255.0	240.0	225.0	210.0	195.0	180.0	165.0	150.0	39.0	38.0	37.0	298.0
306.0	38 1/4	1 1/2	42 1/2	89.86	3.83	310.0	290.0	275.0	260.0	245.0	230.0	215.0	200.0	185.0	170.0	155.0	40.0	39.0	38.0	306.0
314.0	39 1/4	1 1/2	43 1/2	92.20	3.84	315.0	295.0	280.0	265.0	250.0	235.0	220.0	205.0	190.0	175.0	160.0	41.0	40.0	39.0	314.0
322.0	40 1/4	1 1/2	44 1/2	94.54	3.85	320.0	300.0	285.0	270.0	255.0	240.0	225.0	210.0	195.0	180.0	165.0	42.0	41.0	40.0	322.0
330.0	41 1/4	1 1/2	45 1/2	96.88	3.86	325.0	305.0	290.0	275.0	260.0	245.0	230.0	215.0	200.0	185.0	170.0	43.0	42.0	41.0	330.0
338.0	42 1/4	1 1/2	46 1/2	99.22	3.87	330.0	310.0	295.0	280.0	270.0	255.0	240.0	225.0	210.0	195.0	180.0	44.0	43.0	42.0	338.0
346.0	43 1/4	1 1/2	47 1/2	101.56	3.88	335.0	315.0	300.0	285.0	275.0	260.0	245.0	230.0	215.0	200.0	185.0	45.0	44.0	43.0	346.0
354.0	44 1/4	1 1/2	48 1/2	103.90	3.89	340.0	320.0	305.0	290.0	280.0	265.0	250.0	235.0	220.0	205.0	190.0	46.0	45.0	44.0	354.0
362.0	45 1/4	1 1/2	49 1/2	106.24	3.90	345.0	325.0	310.0	295.0	285.0	270.0	255.0	240.0	225.0	210.0	195.0	47.0	46.0	45.0	362.0
370.0	46 1/4	1 1/2	50 1/2	108.58	3.91	350.0	330.0	315.0	300.0	290.0	275.0	260.0	245.0	230.0	215.0	200.0	48.0	47.0	46.0	370.0
378.0	47 1/4	1 1/2	51 1/2	110.92	3.92	355.0	335.0	320.0	305.0	295.0	280.0	265.0	250.0	235.0	220.0	205.0	49.0	48.0	47.0	378.0
386.0	48 1/4	1 1/2	52 1/2	113.26	3.93	360.0	340.0	325.0	310.0	300.0	285.0	270.0	255.0	240.0	225.0	210.0	50.0	49.0	48.0	386.0
394.0	49 1/4	1 1/2	53 1/2	115.60	3.94	365.0	345.0	330.0	315.0	305.0	290.0	275.0	260.0	245.0	230.0	215.0	51.0	50.0	49.0	394.0
402.0	50 1/4	1 1/2	54 1/2	117.94	3.95	370.0	350.0	335.0	320.0	310.0	295.0	280.0	265.0	250.0	235.0	220.0	52.0	51.0	50.0	402.0
410.0	51 1/4	1 1/2	55 1/2	120.28	3.96	375.0	355.0	340.0	325.0	315.0	300.0	285.0	270.0	255.0	240.0	225.0	53.0	52.0	51.0	410.0
418.0	52 1/4	1 1/2	56 1/2	122.62	3.97	380.0	360.0	345.0	330.0	320.0	305.0	290.0	275.0	260.0	245.0	230.0	54.0	53.0	52.0	418.0
426.0	53 1/4	1 1/2	57 1/2	124.96	3.98	385.0	365.0	350.0	335.0	325.0	310.0	295.0	280.0	265.0	250.0	235.0	55.0	54.0	53.0	426.0
434.0	54 1/4	1 1/2	58 1/2	127.30	3.99	390.0	370.0	355.0	340.0	330.0	315.0	300.0	285.0	270.0	255.0	240.0	56.0	55.0	54.0	434.0
442.0	55 1/4	1 1/2	59 1/2	129.64	4.00	395.0	375.0	360.0	345.0	335.0	320.0	305.0	290.0	275.0	260.0	245.0	57.0	56.0	55.0	442.0
450.0	56 1/4	1 1/2	60 1/2	131.98	4.01	400.0	380.0	365.0	350.0	340.0	325.0	310.0	295.0	280.0	265.0	250.0	58.0	57.0	56.0	450.0
458.0	57 1/4	1 1/2	61 1/2	134.32	4.02	405.0	385.0	370.0	355.0	345.0	330.0	315.0	300.0	285.0	270.0	255.0	59.0	5		



## STEEL COLUMN DETAILS

Steel columns are usually made long enough to extend two stories in height in one section. At all joints splice plates should be provided connecting the two sections. The joints are faced and a good bearing insured, only sufficient splice being used to take care of the bending moment at the point and to hold the parts in position.



No. 15.—Types of B-Column and Base Details

The use of column caps should be avoided if possible. The beams or trusses connecting to columns should generally be rivetted to the webs or flanges with connection angles and not set on the top of a cap plate. It is necessary to put a base on a column large enough to distribute the loads to the masonry footings. This base may be built up of rolled shapes and plates; or a cast iron or cast steel sub-base may be interposed between the column base proper and the masonry. In some cases a grillage of beams and concrete is used for distributing the load over the soil. This has its advantages as it eliminates deep excavation and large masses of concrete.

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## CAST IRON COLUMNS

Cast iron columns are suitable only for small buildings of non-fireproof construction. They offer greater resistance to fire than unprotected steel columns, and occupy a minimum of space in the building; but cast iron is not as reliable as steel and should not be used where there is eccentric loading.

SAFE LOADS IN TONS OF 2,000 POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS WITH SQUARE ENDS

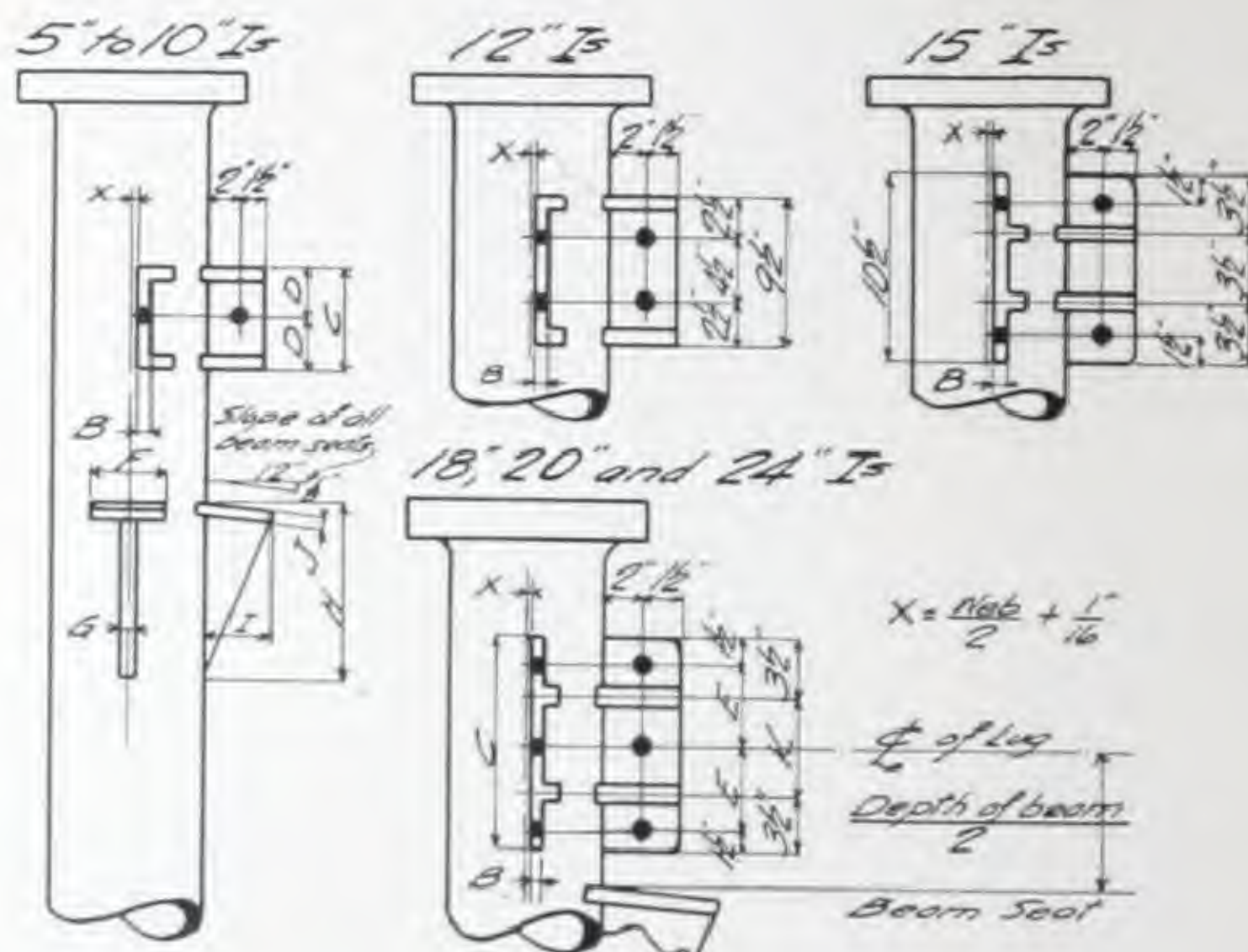
Diam. In.	Thick- ness, In.	LENGTH OF COLUMN IN FEET										Area, Metal, In.	Wt. per Foot of Length
		6	8	10	12	14	16	18	20	22	24		
5	$\frac{3}{4}$	39	34	29	24							10.0	31.3
	$\frac{7}{8}$	45	38	32	27							11.3	35.3
5½	$\frac{3}{4}$	46	40	35	30	26						11.2	35.0
	$\frac{7}{8}$	52	46	40	34	29						12.7	39.7
6	$\frac{3}{4}$	52	47	41	36	31	27	24				12.4	38.7
	$\frac{7}{8}$	60	53	47	41	36	31	27				14.1	44.0
	1	66	59	52	45	39	34	30				15.7	49.0
7	$\frac{3}{4}$	65	60	54	48	43	38	34				14.7	46.0
	$\frac{7}{8}$	74	68	62	55	49	43	38				16.8	52.6
	1	83	76	68	61	54	48	43				18.8	58.9
8	$\frac{3}{4}$	78	72	67	61	55	50	45	40	36	31	17.1	53.4
	$\frac{7}{8}$	89	83	76	70	63	57	51	46	41	37	19.6	61.2
	1	100	93	86	79	71	64	58	52	47	42	22.0	68.7
9	$\frac{7}{8}$	103	98	91	85	80	71	65	59	54	49	22.3	69.8
	1	117	110	103	95	90	80	73	67	61	55	25.1	78.5
	1½	129	122	114	105	99	89	81	74	67	61	27.8	87.0
10	$\frac{7}{8}$	118	112	106	100	93	86	79	73	67	62	25.1	78.4
	1	133	127	120	112	105	97	89	82	76	69	28.3	88.4
	1½	147	141	133	125	116	107	99	91	84	77	31.4	98.0
	1¾	161	154	146	136	127	118	109	100	92	84	34.4	107.4
11	1	149	143	137	129	122	114	106	98	91	85	31.4	98.2
	1½	165	159	152	144	135	126	118	109	101	94	34.9	109.1
	1¾	182	175	167	158	148	139	129	120	111	103	38.3	119.7
	1½	197	190	181	171	161	151	140	130	121	112	41.6	129.9
12	1½	184	178	171	163	154	146	137	128	120	112	38.4	120.1
	1¾	202	195	188	179	170	160	150	141	132	123	42.2	131.9
	1½	220	212	204	194	184	174	163	153	143	133	45.9	143.4
	1½	237	229	220	210	199	187	176	165	154	144	49.5	154.6

**Cast Iron Column Bases**—Cast iron column bases can be supplied to suit all sizes and loadings of columns. A large range of patterns are carried in stock.



## CAST IRON COLUMN DETAILS

In the usual forms of connection of girders and beams to cast iron columns, the beam rests on the bracket-shelf, as shown in No. 16 below, and is bolted to the lug through the web. Connections should be designed with a bracket directly below the web of a single beam, or below both webs on a double beam. The bracket-shelf should be given a slope of  $\frac{1}{8}$ -inch to the foot away from the column so that the load cannot be applied at the edge of the shelf when the beam is deflected under its load.



No. 16—Standard Cast Iron Column Connections

## DIMENSIONS FOR STANDARD CAST IRON COLUMN CONNECTIONS

Size Beam In.	B In.	C In.	D In.	E In.	F In.	G In.	H In.	I In.	J In.	K In.	Max. Load Lbs.	Weight Bracket Lbs.
5	5	3	11	4	3	5	3 1/2	7/8			9000	8.50
6	5	3	11	4 1/2	3 1/2	5	3 1/2	1			9000	9.50
7	5	3	11	4 1/2	3 1/2	5	3 1/2	1			9000	9.50
8	5	4	2	4 1/2	1	6	4	1			12000	13.75
9	5	4	2	5	1 1/8	7 1/4	4	1 1/4			17000	16.00
10	5	4	2	5	1 1/8	7 1/4	4	1 1/4			17000	16.00
12	5			6	1 1/8	9 1/4	4	1 1/4			23000	24.00
15	5			6 1/2	1 1/4	10 1/4	4	1 1/4			33000	29.00
18	1	12		4 1/2	6 1/2	11 1/2	4	1 1/2	5		34000	37.00
20	1	13		5	7	11 1/2	4	1 1/2	6		38000	40.50
24	1	15		6	7 1/2	13 1/2	4	1 1/2	8		45000	46.50

All holes sized for 3/4-inch bolts.

Loads on brackets must not exceed loads shown in column marked maximum load.

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Normal Size, In.	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	42	44	46	48	50	52	54	56	58	60	62	64	66	68	70	72	74	76	78	80	82	84	86	88	90	92	94	96	98	100
External Dia. In.	10.000	12.000	14.000	16.000	18.000	20.000	22.000	24.000	26.000	28.000	30.000	32.000	34.000	36.000	38.000	40.000	42.000	44.000	46.000	48.000	50.000	52.000	54.000	56.000	58.000	60.000	62.000	64.000	66.000	68.000	70.000	72.000	74.000	76.000	78.000	80.000	82.000	84.000	86.000	88.000	90.000	92.000	94.000	96.000	98.000	100.000



## STANDARD PIPE COLUMNS

Steel pipe columns are frequently used for light loads where the loads are quiescent and there is no probability of side thrust. The caps and bases of these are usually loose cast iron with a cross projection which fits inside the pipe. The pipes are machined; also the part of the base or cap where the pipe bears.

SAFE LOADS IN THOUSANDS OF POUNDS FOR STANDARD PIPE COLUMNS

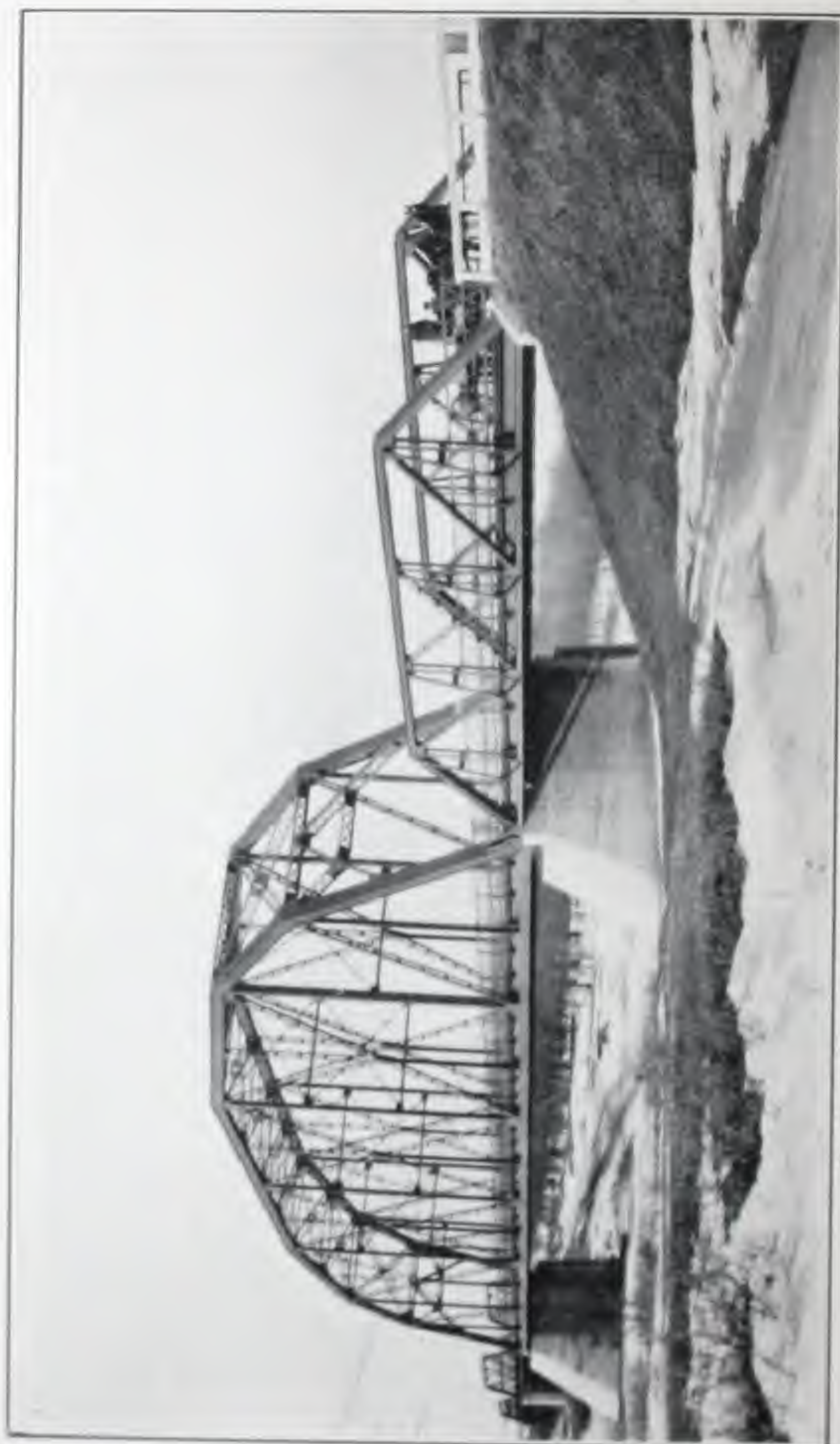
Nominal Size, In.	15	14	13	12	11	10	9	8	7	6	5	4½	4	3½	3	2½	2	1½
External Dia., In.	15.000	13.000	11.000	10.000	9.000	8.000	7.000	6.000	5.000	4.000	3.000	2.000	1.500	1.000	0.750	0.500	0.250	0.000
Thickness, In.	375	475	575	675	775	875	975	1075	1175	1275	1375	1475	1575	1675	1775	1875	1975	2075
5	239.3	224.0	208.7	193.4	178.1	162.8	147.5	132.2	116.9	101.6	86.3	71.0	55.7	40.4	25.1	9.8	4.5	0.0
6	250.3	235.0	219.7	204.4	189.1	173.8	158.5	143.2	127.9	112.6	97.3	82.0	66.7	51.4	36.1	20.8	15.5	10.2
7	259.3	244.0	228.7	213.4	198.1	182.8	167.5	152.2	136.9	121.6	106.3	91.0	75.7	60.4	45.1	29.8	24.5	19.2
8	269.3	254.0	238.7	223.4	208.1	192.8	177.5	162.2	146.9	131.6	116.3	101.0	85.7	70.4	55.1	39.8	34.5	29.2
9	279.3	264.0	248.7	233.4	218.1	202.8	187.5	172.2	156.9	141.6	126.3	111.0	95.7	80.4	65.1	49.8	44.5	39.2
10	289.3	274.0	258.7	243.4	228.1	212.8	197.5	182.2	166.9	151.6	136.3	121.0	105.7	90.4	75.1	59.8	54.5	49.2
11	299.3	284.0	268.7	253.4	238.1	222.8	207.5	192.2	176.9	161.6	146.3	131.0	115.7	100.4	85.1	69.8	64.5	59.2
12	309.3	294.0	278.7	263.4	248.1	232.8	217.5	202.2	186.9	171.6	156.3	141.0	125.7	110.4	95.1	79.8	74.5	69.2
13	319.3	304.0	288.7	273.4	258.1	242.8	227.5	212.2	196.9	181.6	166.3	151.0	135.7	120.4	105.1	89.8	84.5	79.2
14	329.3	314.0	298.7	283.4	268.1	252.8	237.5	222.2	206.9	191.6	176.3	161.0	145.7	130.4	115.1	99.8	94.5	89.2
15	339.3	324.0	308.7	293.4	278.1	262.8	247.5	232.2	216.9	201.6	186.3	171.0	155.7	140.4	125.1	109.8	104.5	99.2
16	349.3	334.0	318.7	303.4	288.1	272.8	257.5	242.2	226.9	211.6	196.3	181.0	165.7	150.4	135.1	119.8	114.5	109.2
17	359.3	344.0	328.7	313.4	298.1	282.8	267.5	252.2	236.9	221.6	206.3	191.0	175.7	160.4	145.1	129.8	124.5	119.2
18	369.3	354.0	338.7	323.4	308.1	292.8	277.5	262.2	246.9	231.6	216.3	201.0	185.7	170.4	155.1	139.8	134.5	129.2
19	379.3	364.0	348.7	333.4	318.1	302.8	287.5	272.2	256.9	241.6	226.3	211.0	195.7	180.4	165.1	149.8	144.5	139.2
20	389.3	374.0	358.7	343.4	328.1	312.8	297.5	282.2	266.9	251.6	236.3	221.0	205.7	190.4	175.1	159.8	154.5	149.2
21	399.3	384.0	368.7	353.4	338.1	322.8	307.5	292.2	276.9	261.6	246.3	231.0	215.7	200.4	185.1	169.8	164.5	159.2
22	409.3	394.0	378.7	363.4	348.1	332.8	317.5	302.2	286.9	271.6	256.3	241.0	225.7	210.4	195.1	179.8	174.5	169.2
23	419.3	404.0	388.7	373.4	358.1	342.8	327.5	312.2	296.9	281.6	266.3	251.0	235.7	220.4	205.1	189.8	184.5	179.2
24	429.3	414.0	398.7	383.4	368.1	352.8	337.5	322.2	306.9	291.6	276.3	261.0	245.7	230.4	215.1	199.8	194.5	189.2
25	439.3	424.0	408.7	393.4	378.1	362.8	347.5	332.2	316.9	301.6	286.3	271.0	255.7	240.4	225.1	209.8	204.5	199.2
26	449.3	434.0	418.7	403.4	388.1	372.8	357.5	342.2	326.9	311.6	296.3	281.0	265.7	250.4	235.1	219.8	214.5	209.2
27	459.3	444.0	428.7	413.4	398.1	382.8	367.5	352.2	336.9	321.6	306.3	291.0	275.7	260.4	245.1	229.8	224.5	219.2
28	469.3	454.0	438.7	423.4	408.1	392.8	377.5	362.2	346.9	331.6	316.3	301.0	285.7	270.4	255.1	239.8	234.5	229.2
29	479.3	464.0	448.7	433.4	418.1	402.8	387.5	372.2	356.9	341.6	326.3	311.0	295.7	280.4	265.1	249.8	244.5	239.2
30	489.3	474.0	458.7	443.4	428.1	412.8	397.5	382.2	366.9	351.6	336.3	321.0	305.7	290.4	275.1	259.8	254.5	249.2

Effective Length in feet

Allowable Fiber Stress per square inch, 13,000 pounds for lengths of 60' radius or under, reduced for lengths over 60' radii, see Construction Specifications. Weights do not include details.

Safe loads for "light" type are for radius of 1' or not over 50'; for "heavy" type, for radius up to 120' or not over 200'.





No. 17—Highway Spans, Fabricated and Erected by The Manitoba Bridge and Iron Works, Limited

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## BRIDGES

Years of experience in designing, fabricating and erecting steel bridges of all types permit us to assure satisfaction in even the most difficult undertakings in this line.

For both the Canadian Pacific Railway and the Canadian National Railways we have constructed numerous railway bridges throughout the western provinces.

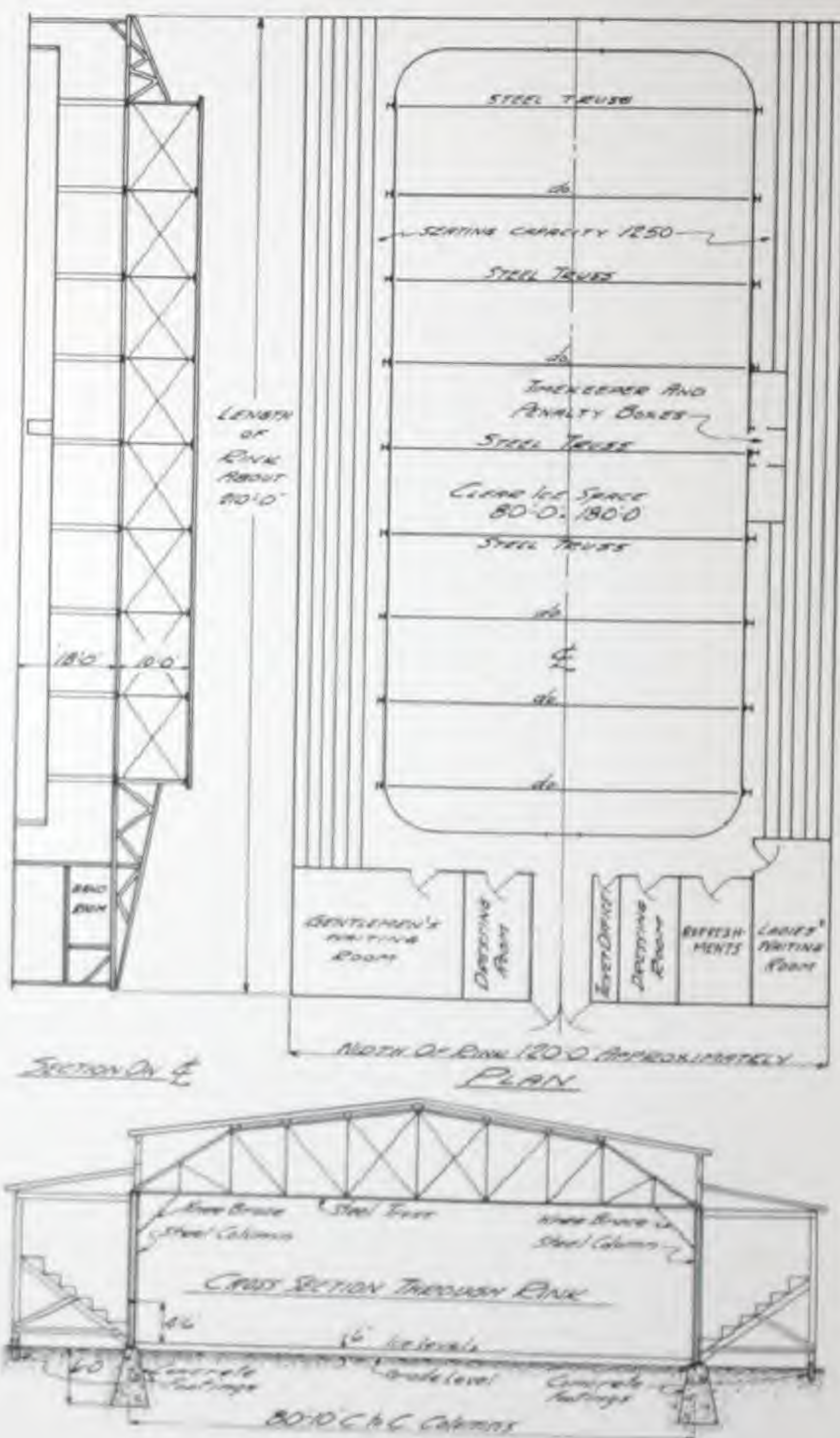
For the Canadian Pacific we fabricated and erected the viaduct over the Bow River on the Suffield-Kipp branch, the bridges on that company's line to Drumheller, Alta. and on their line through southern Saskatchewan, as well as on the main line in British Columbia. We have also built bridges on the Kettle Valley Railway at the coast.

For the Canadian National Railways, we fabricated and erected all the bridges on the Calgary-Edmonton line and many others throughout the West and as far east as Port Arthur. On page 159 is illustrated a railway bridge on the Canadian National cut-off at Dora, Ont., fabricated and erected by us.

In the construction of highway bridges our record is no less imposing. Every province of Western Canada has numerous evidences of the creditable work of our organization. The Morris bridge, recently erected by us at Morris, Man., is an excellent example of fine workmanship in handling a difficult contract. Its center span is an unusual piece of work, measuring 356 feet from center to center of bearings. Views of the span and of the steel work may be seen on pages 64 and 145.

We also construct movable opening bridges and, of these, two examples are the Osborne bridge, over the Assiniboine, shown on page 28, and the Lockport bridge, over the locks. Both are Strauss bascule spans, fabricated and erected by us.





No. 18—Typical Enclosed Skating and Hockey Rink



## RINKS

The problem of providing an outlet for the energy of the youthful members of a community during the long months of Canadian winter finds solution in the enclosed rink. Skating, hockey and curling rinks are an acknowledged necessity, in towns throughout Western Canada, from the standpoint of health as well as recreation.

On the opposite page appears plan and section of a type of enclosed rink which has proved popular and which we have supplied for various towns in Manitoba, Saskatchewan and Alberta.

The size of rink illustrated is 210 feet by 120 feet, with a clear ice space to conform to hockey regulations, 80 feet by 180 feet. The plan allows of a seating capacity for more than 1250 persons, as well as ample space for dressing and waiting rooms, refreshment booth and box office.

No provision is made in this design for end seating, but this can be arranged by putting in an extra truss at the end, and framing to suit. If so desired a further extension can be made at the sides for the accommodation of a curling rink, or the seats at one side may be replaced by curling surface.

The design shown illustrates a type of combination steel-and-wood construction. In any rink, the most difficult and expensive portion is the truss-work. The advantages of steel trusses over those of wooden construction are more than sufficient to offset the slight increase in cost.

Shrinkage, in a wooden truss, whether framed or arched, increases with the length of time the truss has been in position. This shrinkage causes distortion in the members and warping in the truss itself. These defects are concentrated to the roof covering, resulting in leakage, and necessitating continuous repairs.

With steel truss-work, there is a minimum of such difficulty and inconvenience—a sound roof is the result.

In the plan shown on the opposite page, the columns are placed inside the rink so that the truss span may be the shortest possible. In the case of larger rinks the columns may be located in the wall so that there is no obstruction to the view.

The column footings are concrete carried below frost level. Steel columns of 8 x 8-inch I-section are used for carrying the roof trusses, although in some cases 12 x 12-inch timber posts are used. The latter are rather large, and obstruct the view to some extent, but they may be placed back about the middle of the seating. This gives a rather good and economical layout, the saving on the columns helping to balance the extra cost of lengthening the trusses.

The ends of the trusses are framed up in timber so that a row of windows can be put in along the sides, obviating the objectionable necessity of roof skylights, which are so hard to keep watertight.

The roof is made up of timber purlins and 2 x 4-inch or 2 x 6-inch joist rafters, covered with shingles and prepared roofing; in some cases, corrugated iron is used. The sides are either timber framing or corrugated sheeting. The seating accommodation is framed in timber.

Road loading conditions in Western Canada are taken into consideration in designing the trusses, which have all necessary rod bracing to take care of wind loads, etc.

The design shown is only one of many we have supplied. We will be pleased to submit designs to suit any required site and conditions on request.



## TRUSSES

**Roof Trusses**—A roof truss is a frame work designed to support the roof covering over large spans, avoiding the use of interior columns. They form a structure of compression and tension members and produce vertical reactions under vertical loads; the total load of the roof, that is, the weight of the truss, purlins, roof covering, ceiling, and often also the snow and wind load, is usually considered a uniformly distributed load, equally divided between the two supports and producing equal and vertical end reactions.

The purlins usually rest on the upper chord of the truss, transmitting to the latter, the load of the roof covering, the wind and snow load, that of the jack rafter and their own, and are often so arranged as to carry the dead load directly to the truss joints or panel points to avoid transverse stresses. The distance between two consecutive joints of the top chord is the panel length, the distance between two adjacent trusses the bay length.

The transverse strength of the sheathing or of the corrugated iron used for the roof covering generally determines the spaces between the jack rafters or the purlins. These purlins or rafters are small steel shapes, such as beams, channels and angles, or wooden beams, if the roof is not of fireproof construction.

The design and selection of the covering depends on local conditions as to snow load, wind load, etc.

Forms of trusses in common use, with rigid bearing supports, are shown by No. 19 on page 70. A large number of different styles of trusses are used, the character of the building deciding the correct style of truss. The diagram shown on page 70 will serve to illustrate the trusses in most general use in building construction.

**Snow Loads**—Snow load varies according to location and slope of roof. Up to slopes of 20 degrees, the snow load should be taken around 25 pounds per square foot of horizontal roof area, reducing by one pound per degree of slope up to 45 degrees, where no snow load need be considered. Regard should also be given to the possibility of partial snow load with local concentration.

**Wind Loads**—Wind loads also vary with local conditions and with the slope of the roof. When not fixed by building by-laws, they are usually taken as acting horizontally at 40 pounds per square foot on vertical surfaces of greatly-exposed structures and 30 pounds on less-exposed structures. On inclined surfaces, only the normal components of the wind pressure need be considered. The following table gives the normal wind pressure on sloping roofs for a horizontal pressure of 30 pounds per square foot.

NORMAL WIND PRESSURE, IN POUNDS PER SQUARE FOOT

Slope, Degrees	Pressure per Square Foot, Pounds	Slope, Degrees	Pressure per Square Foot, Pounds	Slope, Degrees	Pressure per Square Foot, Pounds	Slope, Degrees	Pressure per Square Foot, Pounds
5	5.19	20	18.37	35	25.90	50	28.97
10	10.11	25	21.51	40	27.29	55	29.41
15	14.55	30	24.00	45	28.28	60	29.69

For other pressures than 30 pounds per square foot, the values given above change in proportion. For slopes over 60 degrees the values assumed for horizontal pressure are applied.

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Corrugated  
Slate  
Tile on steel  
Glass

For roofs  
pounds per  
total live and

Copper, No.  
Corrugated  
Corrugated  
Felt, 2 layers  
Felt and asph  
Glass, 1/2 in  
Lath and plas  
Lead, 1/8 in  
Mackite,  
Sheathing,  
Sheathing,  
Shingles, 6 in  
Skylight, 2 in  
Slag roof,  
Slate, 1/2 in  
Slate, 3/4 in  
Terneplate  
Terneplate  
Tiles (plain)  
Tiles (spec)  
Zinc, No.



**Combined Roof Loads**—Where the roof loads are not fixed by building laws, ordinary roofs up to 30 feet span should carry the following minimum loads per square foot of exposed surface, applied vertically to provide for dead, wind and snow loads.

**Minimum Roof Loads, in Pounds per Square Foot**

Roof Covering	Minimum Load
Gravel or Composition on boards, steep slope, 1 to 8 or less	15
Roofing on 3 inch flat tile or similar concrete	20
Corrugated sheeting on boards or purlins	25
Slate on boards or purlins	30
Tile on steel purlins	35
Glass	40

For roofs in climates where ice snow is likely to occur, reduce these loads by 10 pounds per square foot, but no roof or any part thereof should be designed for a total live and dead load less than 40 pounds per square foot.

**Approximate Weights of Roofs in Pounds**

Roofing Material	Weight
Copper, No. 22 B. W. G.	15
Corrugated galvanized iron, No. 20 B. W. G.	12
Corrugated galvanized iron, No. 24 B. W. G.	10
Felt, 2 layers	1
Felt and asphalt or similar	2
Glass, 1/2 inch thick	12
Lath and plaster ceiling	10
Lath, 1/2 inch thick	5
Machine, 1 inch thick, with plaster	15
Sheeting, hemlock, 1 inch thick	35
Sheeting, white pine, spruce, 1 inch thick	30
Sheeting, yellow pine, 1 inch thick	25
Shingles, 16x8 inches, 11 inches to weather	18
Shingles, glass 1/2 to 3/4 inch, including frame	25
Slag roof, 4 ply, with cement and sand	15
Slate, 1/2 inch thick, 8 inch double lap	40
Slate, 3/4 inch thick, 8 inch double lap	45
Terminator, B	10
Terminator, IX	12
Tile (glazed), 10 1/2 x 14 1/2 inches, 3 1/4 inches to weather	18
Tile (unglazed), 14 1/2 x 20 1/2 inches, 7 1/4 inches to weather	40
Zinc, No. 20 B. W. G.	12



**Form of Trusses.**—A great variety of trusses are used in building construction the form depending on the character of the building.

The trusses in No. 19 are so arranged that the compression members are the shorter members while the tension members are longer. The last four types are for corrugation, wood and steel, for which they are well adapted. The flat type are well adapted for tar and gravel covering and it is only necessary to give them enough slope for proper drainage.



Fig. 19. Forms of Trusses in Common Use, when supported by Equal Spacing.

Comparative estimates of steel trusses for comparing the total cost of steel trusses of the same span for various spacing indicate that for spans up to 50 feet the most economical spacing is about 12 feet for light loads or about  $\frac{1}{2}$  the span.

The spans of from 50 feet to 100 feet the spacing should be about  $\frac{1}{3}$  the span for the shorter spans and about  $\frac{1}{4}$  the span for the longer spans or from 12 feet to 20 feet. In spans over 100 feet conditions govern and determine the spacing of the trusses according to the economic conditions.

Spacing for a roof supported on rigid walls cannot be calculated definitely and the designer must use his judgment, based on past experience, as to the position, size and number required to give a stiff roof.

Steel trusses supported on steel columns allow of the approximate determination of stresses in trusses, and generally every third or fourth joint of trusses should be rigidly braced with diagonals placed on the plane of the top and bottom chords of the trusses. The compression between trusses being taken by lines of stress running continuously the length of the building.



### DETAILS FOR PUNCHING AND RIVETTING

Dimensions in Inches

### CONVENTIONAL SIGNS FOR RIVETTING

SHOP RIVETS			FIELD RIVETS		
Two full heads	Counter-sunk and Chipped		Two full heads	Counter-sunk and Chipped	
	Near Side	Far Side		Near Side	Far Side
	Both Sides			Both Sides	

SHOP RIVETS		
Counter-sunk but not chipped. Max. Height, $\frac{1}{8}$ "	Flattened to $\frac{1}{8}$ " high $\frac{1}{2}$ " and $\frac{3}{4}$ " Rivets	Flattened to $\frac{3}{4}$ " high $\frac{1}{2}$ " and $\frac{3}{4}$ " Rivets
Near Side	Far Side	Both Sides
Both Sides		

## GAUGES FOR ANGLES

Leg	8	7	6	5	4	3 $\frac{1}{2}$	3	2 $\frac{1}{2}$	2	1 $\frac{3}{4}$	1 $\frac{1}{2}$	1 $\frac{3}{8}$	1 $\frac{1}{4}$	1	$\frac{3}{4}$
g1	4 $\frac{1}{2}$	4	3 $\frac{1}{2}$	3	2 $\frac{1}{2}$	2	1 $\frac{3}{4}$	1 $\frac{3}{8}$	1 $\frac{1}{8}$	1	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{3}{4}$	$\frac{5}{8}$	$\frac{1}{2}$
g2	3	2 $\frac{1}{2}$	2 $\frac{1}{2}$	2											
g3	3	3	2 $\frac{1}{4}$	1 $\frac{3}{4}$											
Max. rivet	1 $\frac{3}{8}$	1	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{3}{4}$	$\frac{5}{8}$	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{3}{8}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$

For column details, 6" leg ( $\frac{1}{2}$  inch thick or less) against column shaft.  $g_2 = 13\frac{1}{2}"$ ,  $g_3 = 3"$

For diagonal angles, etc., gauge in middle, where riveted leg equals or exceeds 3" for  $\frac{3}{4}$ " rivets.

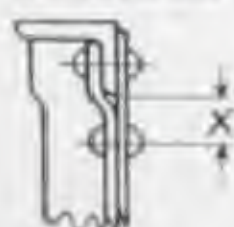
Use special gauges to adapt work to multiple punch, or to secure desirable details.

## CLEARANCE FOR WEB RIVETTING



Size Rivet	Min.	Std.
$\frac{5}{8}$	$\frac{7}{8}$	$1\frac{1}{8}$
$\frac{3}{4}$	1	$1\frac{1}{4}$
$\frac{7}{8}$	$1\frac{1}{8}$	$1\frac{3}{8}$
1	$1\frac{1}{4}$	$1\frac{1}{2}$
$1\frac{1}{8}$	$1\frac{3}{8}$	$1\frac{5}{8}$

### RIVETS IN CRIMPED ANGLES



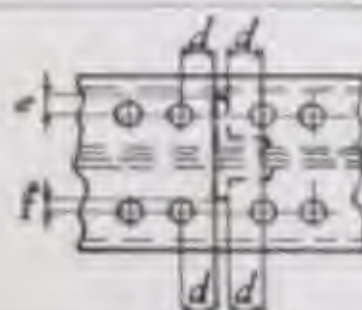
Distance X should be  $1\frac{1}{2}$  inches, plus the thickness of chord angles, but never less than 2 inches.

## STANDARD RIVET DIES



Size Rivet	Diam. of Die
$\frac{5}{8}$	2
$\frac{3}{4}$	$2\frac{1}{4}$
$\frac{7}{8}$	$2\frac{1}{2}$
1	$2\frac{3}{4}$
$1\frac{1}{8}$	3

### CLEARANCE FOR COVER PLATE RIVETTING



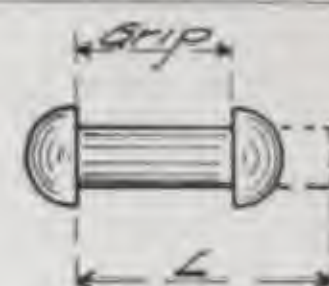
e	$1_2$	1	$11_2$	2	$21_2$	3	$31_2$	4	$1_2$	5	$51_2$	6
d	$21_2$	$25_8$	$23_4$	$23_4$	$27_8$	$27_8$	3	$31_8$	$31_8$	$31_4$	$31_4$	$31_8$
f	0	$1_2$	1	$11_2$	2	$21_2$						
d	$21_2$	$21_4$	$21_8$	2	$11_2$	0						



## RIVETS

RIVET LENGTHS AND APPROXIMATE WEIGHTS  
PER HUNDRED FOR VARIOUS GRIPS

Weights given are for rivets before driving.



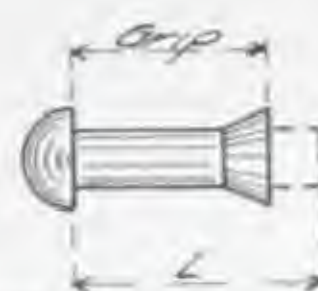
Grip, In.	3/8-Inch		1/2-Inch		5/8-Inch		3/4-Inch		7/8-Inch		1-Inch	
	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.
1/2	1 1/2	14.2	1 3/4	26.3	1 7/8	37.1	2	56.7	2 1/8	86.3		
5/8	1 5/8	14.8	1 7/8	27.4	2	38.6	2 1/8	58.8	2 1/4	88.8		
3/4	1 3/4	15.5	2	28.5	2 1/8	40.1	2 1/4	60.9	2 3/8	91.9		
7/8	1 7/8	16.2	2 1/8	29.6	2 1/4	41.8	2 3/8	63.1	2 1/2	94.6		
1	2	16.9	2 1/4	30.6	2 3/8	43.3	2 1/2	65.2	2 5/8	97.4		
1 1/8	2 1/8	17.6	2 3/8	31.7	2 1/2	44.9	2 5/8	67.3	2 3/4	100.2		
1 1/4	2 1/4	18.3	2 1/2	32.8	2 5/8	46.5	2 3/4	69.6	2 7/8	103.0		
1 3/8	2 3/8	19.0	2 5/8	33.9	2 3/4	48.0	2 7/8	71.6	3	105.0		
1 1/2	2 1/2	20.4	2 7/8	36.1	3	51.2	3 1/8	75.8	3 1/4	111.3		
1 5/8	2 3/4	21.1	3	37.2	3 1/8	52.7	3 1/4	78.0	3 3/8	114.1		
1 3/4	3	22.5	3 1/4	39.4	3 3/8	55.8	3 1/2	82.2	3 5/8	119.7		
1 7/8	3 1/8	23.2	3 3/8	40.4	3 1/2	57.4	3 5/8	84.4	3 3/4	122.4		
2	3 1/4	23.9	3 1/2	41.5	3 5/8	59.0	3 3/4	86.5	3 7/8	125.1		
2 1/8	3 3/8	24.6	3 5/8	42.6	3 3/4	60.5	3 7/8	88.6	4	128.0		
2 1/4	3 1/2	25.3	3 3/4	43.7	3 7/8	62.1	4	90.8	4 1/8	130.8		
2 3/8	3 5/8	26.0	3 7/8	44.8	4	63.7	4 1/8	92.9	4 1/4	133.6		
2 1/2	3 3/4	26.7	4	45.9	4 1/8	65.2	4 1/4	95.0	4 3/8	136.4		
2 5/8	3 7/8	27.4	4 1/8	47.0	4 1/4	66.8	4 3/8	97.1	4 1/2	139.0		
2 3/4	4	28.1	4 1/4	48.0	4 3/8	78.4	4 1/2	99.3	4 5/8	141.9		
2 7/8	4 1/8	28.7	4 3/8	49.1	4 1/2	69.9	4 5/8	101.4	4 3/4	145.0		
3	4 3/8	30.1	4 5/8	51.3	4 3/4	73.1	4 7/8	105.6	5	150.0		
3 1/8	4 1/2	30.8	4 3/4	52.4	4 7/8	74.6	5	107.8	5 1/8	153.0		
3 1/4	4 5/8	31.5	4 7/8	53.5	5	76.2	5 1/8	109.9	5 1/4	155.8		
3 3/8	4 3/4	32.2	5	54.6	5 1/8	77.8	5 1/4	112.0	5 3/8	158.6		
3 1/2	4 7/8	32.9	5 1/8	55.6	5 1/4	79.3	5 3/8	114.2	5 1/2	161.4		
3 5/8	5	33.6	5 1/4	56.7	5 3/8	80.9	5 1/2	116.3	5 5/8	164.2		
3 3/4	5 1/8	34.3	5 3/8	57.8	5 1/2	82.4	5 5/8	118.4	5 3/4	167.0		
3 7/8	5 1/4	35.0	5 1/2	58.9	5 5/8	84.0	5 3/4	120.6	5 7/8	169.7		
4	5 3/8	35.7	5 5/8	60.0	5 3/4	85.6	5 7/8	122.7	6	172.5		
4 1/8	5 5/8	36.8	5 7/8	62.2	6	88.6	6 1/8	126.9	6 1/4	178.1		
4 1/4	5 3/4	37.8	6	63.3	6 1/8	90.3	6 1/4	129.1	6 3/8	180.9		
4 3/8	6	39.2	6 1/4	65.5	6 3/8	93.4	6 1/2	133.3	6 5/8	186.5		
4 1/2	6 1/8	39.9	6 3/8	66.6	6 1/2	95.1	6 3/8	135.4	6 3/4	189.2		
4 5/8	6 1/4	40.6	6 1/2	67.6	6 5/8	96.5	6 3/4	137.6	6 7/8	192.0		
4 3/4	6 3/8	41.3	6 5/8	68.7	6 3/4	98.1	6 7/8	139.7	7	194.8		
4 7/8	6 1/2	42.0	6 3/4	69.8	6 7/8	99.7	7	141.9	7 1/8	197.6		
5	6 5/8	42.7	6 3/8	70.9	7	101.12	7 1/8	144.0	7 1/4	200.3		
5 1/8					7 1/8	102.8	7 3/4	146.1	7 3/8	203.1		
5 1/4					7 1/4	104.4	7 5/8	148.2	7 1/2	205.9		
5 3/8					7 3/8	105.9	7 1/2	150.4	7 3/8	208.7		
5 1/2					7 5/8	108.9	7 3/4	154.7	7 3/8	214.3		
5 5/8					7 3/8	111.0	7 5/8	156.8	8	217.0		
5 3/4					7 5/8	112.5	8	159.0	8 1/8	219.8		
5 7/8					8	114.0	8 1/8	161.1	8 1/4	222.6		
6					8 1/8	115.5	8 1/4	163.2	8 3/8	224.5		



## RIVETS

RIVET LENGTHS AND APPROXIMATE WEIGHTS  
PER HUNDRED FOR VARIOUS GRIPS

Weights given are for rivets before driving.



Grip, In.	$\frac{1}{2}$ -Inch		$\frac{3}{8}$ -Inch		$\frac{1}{4}$ -Inch		$\frac{7}{16}$ -Inch		1-Inch	
	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.	L, In.	Weight per 100, Lbs.
$\frac{1}{2}$	$1\frac{1}{8}$	12.2	$1\frac{1}{4}$	22.0	$1\frac{1}{4}$	29.3	$1\frac{3}{8}$	46.1	$1\frac{3}{8}$	69.6
$\frac{3}{8}$	$1\frac{1}{4}$	12.8	$1\frac{3}{8}$	23.1	$1\frac{3}{8}$	30.9	$1\frac{1}{2}$	48.2	$1\frac{1}{2}$	72.2
$\frac{3}{4}$	$1\frac{3}{8}$	13.4	$1\frac{1}{2}$	24.1	$1\frac{1}{2}$	32.4	$1\frac{5}{8}$	50.3	$1\frac{5}{8}$	74.6
$\frac{7}{8}$	$1\frac{1}{2}$	14.2	$1\frac{5}{8}$	25.2	$1\frac{5}{8}$	34.0	$1\frac{3}{4}$	52.5	$1\frac{3}{4}$	77.7
1	$1\frac{5}{8}$	14.8	$1\frac{3}{4}$	26.3	$1\frac{3}{4}$	35.5	$1\frac{7}{8}$	54.6	$1\frac{7}{8}$	80.7
$1\frac{1}{8}$	$1\frac{3}{4}$	15.5	$1\frac{7}{8}$	27.4	$1\frac{7}{8}$	37.1	2	56.7	2	83.3
$1\frac{1}{4}$	$1\frac{7}{8}$	16.2	2	28.5	2	38.6	$2\frac{1}{8}$	58.8	$2\frac{1}{8}$	86.3
$1\frac{3}{8}$	2	16.9	$2\frac{1}{8}$	29.6	$2\frac{1}{8}$	40.1	$2\frac{1}{4}$	61.0	$2\frac{1}{4}$	88.8
$1\frac{5}{8}$	$2\frac{1}{4}$	18.3	$2\frac{3}{8}$	31.7	$2\frac{1}{2}$	44.9	$2\frac{1}{2}$	65.2	$2\frac{3}{4}$	97.4
$1\frac{3}{4}$	$2\frac{1}{2}$	19.7	$2\frac{5}{8}$	33.9	$2\frac{3}{4}$	48.0	$2\frac{3}{4}$	69.5	$2\frac{7}{8}$	103.0
$1\frac{7}{8}$	$2\frac{3}{8}$	20.4	$2\frac{3}{4}$	35.0	$2\frac{7}{8}$	49.6	$2\frac{7}{8}$	71.6	3	105.0
2	$2\frac{3}{4}$	21.1	$2\frac{7}{8}$	36.1	3	51.2	3	73.7	$3\frac{1}{8}$	108.5
$2\frac{1}{8}$	$2\frac{7}{8}$	21.8	3	37.2	$3\frac{1}{8}$	52.7	$3\frac{1}{8}$	75.9	$3\frac{1}{4}$	111.3
$2\frac{1}{4}$	3	22.5	$3\frac{1}{8}$	38.3	$3\frac{1}{4}$	54.3	$3\frac{1}{4}$	78.0	$3\frac{3}{8}$	114.1
$2\frac{3}{8}$	$3\frac{1}{8}$	23.2	$3\frac{1}{4}$	39.4	$3\frac{3}{8}$	55.8	$3\frac{3}{8}$	80.1	$3\frac{1}{2}$	116.9
$2\frac{1}{2}$	$3\frac{1}{4}$	23.9	$3\frac{3}{8}$	40.4	$3\frac{1}{2}$	57.4	$3\frac{1}{2}$	82.3	$3\frac{5}{8}$	119.7
$2\frac{5}{8}$	$3\frac{3}{8}$	24.6	$3\frac{1}{2}$	41.5	$3\frac{5}{8}$	59.0	$3\frac{5}{8}$	84.4	$3\frac{3}{4}$	122.4
$2\frac{3}{4}$	$3\frac{1}{2}$	25.3	$3\frac{5}{8}$	42.6	$3\frac{3}{4}$	60.5	$3\frac{3}{4}$	86.5	$3\frac{7}{8}$	125.1
$2\frac{7}{8}$	$3\frac{5}{8}$	26.0	$3\frac{3}{4}$	43.7	$3\frac{7}{8}$	62.1	$3\frac{7}{8}$	88.6	4	128.0
3	$3\frac{7}{8}$	27.4	4	45.9	4	63.7	$4\frac{1}{8}$	92.9	$4\frac{1}{4}$	133.6
$3\frac{1}{8}$	4	28.1	$4\frac{1}{8}$	47.0	$4\frac{1}{8}$	65.2	$4\frac{1}{4}$	95.0	$4\frac{3}{8}$	136.4
$3\frac{1}{4}$	$4\frac{1}{8}$	28.7	$4\frac{1}{4}$	48.0	$4\frac{1}{4}$	66.8	$4\frac{3}{8}$	97.2	$4\frac{1}{2}$	139.0
$3\frac{3}{8}$	$4\frac{1}{4}$	29.4	$4\frac{3}{8}$	49.1	$4\frac{3}{8}$	68.4	$4\frac{1}{2}$	99.3	$4\frac{5}{8}$	141.9
$3\frac{1}{2}$	$4\frac{3}{8}$	30.1	$4\frac{1}{2}$	50.2	$4\frac{1}{2}$	69.9	$4\frac{5}{8}$	101.4	$4\frac{3}{4}$	145.0
$3\frac{5}{8}$	$4\frac{1}{2}$	30.8	$4\frac{5}{8}$	51.3	$4\frac{5}{8}$	71.5	$4\frac{3}{4}$	103.5	$4\frac{7}{8}$	147.5
$3\frac{3}{4}$	$4\frac{5}{8}$	31.5	$4\frac{3}{4}$	52.4	$4\frac{3}{4}$	73.1	$4\frac{7}{8}$	105.7	5	150.0
$3\frac{7}{8}$	$4\frac{3}{4}$	32.2	$4\frac{7}{8}$	53.5	$4\frac{7}{8}$	74.6	5	107.8	$5\frac{1}{8}$	153.0
4	$4\frac{7}{8}$	32.9	5	54.6	5	76.2	$5\frac{1}{8}$	109.9	$5\frac{1}{4}$	155.8
$4\frac{1}{8}$	$5\frac{1}{8}$	34.3	$5\frac{1}{4}$	56.7	$5\frac{1}{4}$	79.3	$5\frac{3}{8}$	114.2	$5\frac{1}{2}$	161.4
$4\frac{1}{4}$	$5\frac{1}{4}$	35.0	$5\frac{3}{8}$	57.8	$5\frac{3}{8}$	80.9	$5\frac{1}{2}$	116.3	$5\frac{5}{8}$	164.2
$4\frac{3}{8}$	$5\frac{1}{2}$	36.4	$5\frac{5}{8}$	60.0	$5\frac{5}{8}$	84.0	$5\frac{5}{8}$	118.4	$5\frac{3}{4}$	167.0
$4\frac{1}{2}$	$5\frac{3}{8}$	37.1	$5\frac{3}{4}$	61.1	$5\frac{3}{4}$	85.6	$5\frac{3}{4}$	120.6	$5\frac{7}{8}$	169.7
$4\frac{5}{8}$	$5\frac{3}{4}$	37.8	$5\frac{7}{8}$	62.2	$5\frac{7}{8}$	87.1	$5\frac{7}{8}$	122.7	6	172.5
$4\frac{3}{4}$	$5\frac{7}{8}$	38.5	6	63.3	6	88.6	6	124.8	$6\frac{1}{8}$	175.3
$4\frac{7}{8}$	6	39.2	$6\frac{1}{8}$	64.4	$6\frac{1}{8}$	90.3	$6\frac{1}{8}$	126.9	$6\frac{1}{4}$	178.1
5	$6\frac{1}{8}$	39.9	$6\frac{1}{4}$	65.5	$6\frac{1}{4}$	91.8	$6\frac{1}{4}$	129.1	$6\frac{3}{8}$	180.9
$5\frac{1}{8}$	.....	.....	.....	.....	$6\frac{3}{8}$	93.4	$6\frac{3}{8}$	131.2	$6\frac{1}{2}$	184.0
$5\frac{1}{4}$	.....	.....	.....	.....	$6\frac{1}{2}$	95.1	$6\frac{1}{2}$	133.4	$6\frac{3}{4}$	186.5
$5\frac{3}{8}$	.....	.....	.....	.....	$6\frac{3}{4}$	96.5	$6\frac{3}{4}$	135.5	$6\frac{7}{8}$	189.2
$5\frac{1}{2}$	.....	.....	.....	.....	$6\frac{7}{8}$	99.7	$6\frac{7}{8}$	139.8	7	194.8
$5\frac{3}{8}$	.....	.....	.....	.....	7	101.2	7	142.0	$7\frac{1}{8}$	197.6
$5\frac{3}{4}$	.....	.....	.....	.....	$7\frac{1}{8}$	102.8	$7\frac{1}{8}$	144.1	$7\frac{1}{4}$	200.3
$5\frac{7}{8}$	.....	.....	.....	.....	$7\frac{1}{4}$	104.4	$7\frac{1}{4}$	146.2	$7\frac{3}{8}$	203.1
6	.....	.....	.....	.....	$7\frac{3}{8}$	105.9	$7\frac{3}{8}$	148.3	$7\frac{1}{2}$	205.9



## RIVETS

## SHEARING AND BEARING VALUES

 $\frac{3}{8}$ -INCH RIVETS—Area .1104 Square Inch

Shear	Unit, Lbs. per Sq. In.	7000	8000	9000	10000	11000	12000
	Single Shear per Rivet, Lbs.	770	880	990	1100	1210	1320
	Double Shear per Rivet, Lbs.	1540	1760	1980	2200	2420	2640
Bearing	Unit, Lbs. per Sq. In.	14000	16000	18000	20000	22000	24000
	Thickness, In.						
	$\frac{1}{8}$	660	750	840	940	1030	1130
	$\frac{3}{16}$	980	1130	1270	1410	1550	1690
	$\frac{1}{4}$	1310	1500	1690	1880	2060	2250
	$\frac{5}{16}$	1640	1880	2110	2340	2580	2810
	$\frac{3}{8}$	1910	2250	2530	2810	3090	3380

 $\frac{1}{2}$ -INCH RIVETS—Area .1963 Square Inch

Shear	Unit, Lbs. per Sq. In.	7000	8000	9000	10000	11000	12000
	Single Shear per Rivet, Lbs.	1370	1570	1770	1960	2160	2360
	Double Shear per Rivet, Lbs.	2750	3140	3530	3930	4320	4710
Bearing	Unit, Lbs. per Sq. In.	14000	16000	18000	20000	22000	24000
	Thickness, In.						
	$\frac{3}{16}$	1310	1500	1690	1880	2060	2250
	$\frac{1}{4}$	1750	2000	2250	2500	2750	3000
	$\frac{5}{16}$	2190	2500	2810	3130	3440	3750
	$\frac{3}{8}$	2630	3000	3380	3750	4130	4500
	$\frac{1}{2}$	3060	3500	3940	4380	4810	5250
		3500	4000	4500	5000	5500	6000

 $\frac{5}{8}$ -INCH RIVETS—Area .3068 Square Inch

Shear	Unit, Lbs. per Sq. In.	7000	8000	9000	10000	11000	12000
	Single Shear per Rivet, Lbs.	2150	2450	2760	3070	3370	3680
	Double Shear per Rivet, Lbs.	4300	4910	5520	6140	6750	7360
Bearing	Unit, Lbs. per Sq. In.	14000	16000	18000	20000	22000	24000
	Thickness, In.						
	$\frac{3}{8}$	1640	1880	2110	2340	2580	2810
	$\frac{1}{2}$	2190	2500	2810	3130	3440	3750
	$\frac{5}{8}$	2730	3130	3520	3910	4300	4690
	$\frac{3}{4}$	3280	3750	4220	4690	5160	5630
	$\frac{7}{8}$	3830	4380	4920	5470	6020	6560
		4380	5000	5630	6250	6880	7500
		4920	5630	6330	7030	7730	8440
		5470	6250	7040	7810	8590	9380

Values in "heavy" type are greater than double shear.



## RIVETS

## SHEARING AND BEARING VALUES

## 1/2-INCH RIVETS—Area .4418 Square Inch

Fast. Lbs. per Sq. In.		7000	8000	9000	10000	11000	12000
Shear	Single Shear per Rivet, Lbs.	3089	3528	3967	4406	4845	5284
	Double Shear per Rivet, Lbs.	6178	7056	7934	8812	9690	10568
	Fast. Lbs. per Sq. In.	14000	16000	18000	20000	22000	24000
Bearing	Thickness of Plate, In.	1/4	3070	3510	3950	4390	4830
		5/16	3180	3620	4060	4500	4940
		3/8	3290	3730	4170	4610	5050
		7/16	3400	3840	4280	4720	5160
		1/2	3510	3950	4390	4830	5270
		5/8	3620	4060	4500	4940	5380
		3/4	3730	4170	4610	5050	5490
		7/8	3840	4280	4720	5160	5600
		1	3950	4390	4830	5270	5710
		1 1/8	4060	4500	4940	5380	5820

## 3/4-INCH RIVETS—Area .6013 Square Inch

Fast. Lbs. per Sq. In.		7000	8000	9000	10000	11000	12000
Shear	Single Shear per Rivet, Lbs.	4211	4812	5413	6014	6615	7216
	Double Shear per Rivet, Lbs.	8422	9624	10825	12026	13227	14428
	Fast. Lbs. per Sq. In.	14000	16000	18000	20000	22000	24000
Bearing	Thickness of Plate, In.	1/4	3640	4080	4520	4960	5400
		5/16	3750	4190	4630	5070	5510
		3/8	3860	4300	4740	5180	5620
		7/16	3970	4410	4850	5290	5730
		1/2	4080	4520	4960	5400	5840
		5/8	4190	4630	5070	5510	5950
		3/4	4300	4740	5180	5620	6060
		7/8	4410	4850	5290	5730	6170
		1	4520	4960	5400	5840	6280
		1 1/8	4630	5070	5510	5950	6390

## 1-INCH RIVETS—Area .7854 Square Inch

Fast. Lbs. per Sq. In.		7000	8000	9000	10000	11000	12000
Shear	Single Shear per Rivet, Lbs.	5895	6774	7653	8532	9411	10290
	Double Shear per Rivet, Lbs.	11790	13548	15306	17064	18822	20580
	Fast. Lbs. per Sq. In.	14000	16000	18000	20000	22000	24000
Bearing	Thickness of Plate, In.	1/4	5070	5780	6490	7200	7910
		5/16	5210	5920	6630	7340	8050
		3/8	5350	6060	6770	7480	8190
		7/16	5490	6200	6910	7620	8330
		1/2	5630	6340	7050	7760	8470
		5/8	5770	6480	7190	7900	8610
		3/4	5910	6620	7330	8040	8750
		7/8	6050	6760	7470	8180	8890
		1	6190	6900	7610	8320	9030
		1 1/8	6330	7040	7750	8460	9170

Values in "single" shear are for clean smooth rivets.

Values in "bearing" shear are generally from British tables.



## BOLTS AND SCREWS

The illustration below shows the more common types of bolts and screws in general use. It should prove useful, as discussion often arises concerning the differences between certain types.

<b>MACHINE BOLTS</b>  MADE FROM RIVET STEEL WITH HEX. NUT & HEAD MIN GRIP $\frac{3}{8}$ " BOLT LENGTH IN 1/2 INCHES MANUFACTURE PURCHASE	<b>ERECTION BOLTS</b>  MADE FROM RIVET STEEL WITH SQUARE HEAD & NUT MIN GRIP $\frac{3}{8}$ " GENERALLY ROUGH FROM U.S.A. MANUFACTURE PURCHASE	<b>TURNT BOLTS</b>  1" BOLT TURNED DOWN 1/2" HOLE 1/2" HOLE SMALL AND HEAD FOR 1/2" & 1/2" & 1/2" HEADS ALWAYS USED USUALLY 2" HEADS NUTS NOT ON SQUARE MANUFACTURE PURCHASE
<b>CARRIAGE BOLTS</b>  LENGTHS 1 1/2 TO 20" LENGTHS IN 1/2 UP TO 5" 1/2 UP TO 10, 1 UP TO 20" PURCHASE	<b>STOVE BOLTS</b>  ROUND HEAD FLAT HEAD LENGTHS 1/2 TO 6 1/2" LENGTHS IN 1/2 TO 1 1/2, IN 1/2 ABOVE 1 1/2" PURCHASE	<b>CAP SCREWS</b>  AT LEAST LENGTH HEADS SQUARE OR HEX POLISHED FINISH PURCHASE
<b>TAP BOLTS</b>  AT LEAST LENGTH MADE FROM RIVET STEEL WITH SQUARE OR HEX HEADS MANUFACTURE PURCHASE	<b>SET SCREWS</b>  POINTS VARY LENGTH HEADS SQUARE PURCHASE	<b>LAG SCREWS</b>  LENGTH LENGTHS 1 1/2 TO 12" LENGTHS IN 1/2 UP TO 8" IN 1" ABOVE 8" PURCHASE
<b>WOOD SCREWS</b>  FLAT HEAD LENGTH ROUND HEAD PURCHASE ALL SIZES	<b>DRIFT BOLTS</b>  END VARIER LENGTH BUTTON HEAD	<b>GUARD RAIL SPIKES</b>  LENGTH USUALLY 1/2" & 1/2" LONG

No. 20—Types of Bolts and Screws

Information as to sizes, lengths and finishes of the bolts and screws shown above is given in the text of the accompanying pages of this section.



## MACHINE BOLTS

The rules used for design of threads, widths of threads per inch, and sizes for heads and nuts are those commonly known as U. S. Standard, as follows:



FIG. 25. Shape of Thread.

Minor diameter of rough nut or rough head is equal to one and a half times the diameter of bolt, plus  $\frac{1}{16}$ ". Thickness of rough nut equals diameter of bolt. Thickness of rough head equals one half the shaft diameter of head.

DIMENSIONS OF HEADS AND NUTS

Size of Bolt	Round		Hex		Hex	
	Head	Nut	Head	Nut	Head	Nut
1/4"						
5/16"						
3/8"						
1/2"						
5/8"						
3/4"						
7/8"						
1"						
1 1/8"						
1 1/4"						
1 3/8"						
1 1/2"						
1 3/4"						
2"						
2 1/4"						
2 1/2"						
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16"						
16 1/4"						
16 1/2"						
16 3/4"						
17"						
17 1/4"						
17 1/2"						



### BOLTS WITH SQUARE HEADS AND NUTS WEIGHT IN POUNDS PER 100 BOLTS

Length Under Head, Inches	Diameter of Bolt, Inches								
	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	1
1	4	7	11	15	22	37	56		
$1\frac{1}{4}$	4	7	11	16	23	39	59		
$1\frac{1}{2}$	5	8	12	17	24	41	62		
$1\frac{3}{4}$	5	8	13	18	26	43	64		
2	5	9	14	19	27	45	67	101	144
$2\frac{1}{4}$	6	9	15	20	28	47	71	104	150
$2\frac{1}{2}$	6	10	15	21	30	49	74	109	155
$2\frac{3}{4}$	6	10	16	22	31	51	77	113	161
3	7	11	17	24	33	54	80	117	167
$3\frac{1}{2}$	7	12	18	25	35	58	86	126	178
4	8	13	20	28	38	62	92	134	189
$4\frac{1}{2}$	9	14	21	30	41	66	98	142	198
5	10	15	23	32	43	71	104	151	209
$5\frac{1}{2}$	10	16	25	34	46	75	111	159	220
6	11	17	26	36	49	79	117	168	232
$6\frac{1}{2}$			28	38	52	84	123	170	243
7			29	40	55	88	129	185	254
$7\frac{1}{2}$			31	42	57	92	136	193	265
8			32	45	60	97	142	202	276
9			34	49	65	105	154	218	298
10				53	71	114	167	235	320
12				61	82	131	192	269	364
14					93	148	217	303	409
Per Inch Additional	1.4	2.2	3.1	4.3	5.6	8.7	12.5	17.0	22.3

### SQUARE NUTS AND BOLT HEADS WEIGHTS IN POUNDS FOR ONE HEAD AND ONE NUT

Diameter of Bolt, Inches	$1\frac{1}{4}$	$1\frac{1}{2}$	$1\frac{3}{4}$	2	$2\frac{1}{2}$	3
Square Head and Nut	2.05	3.51	5.48	8.08	15.5	26.2
Weight of Shank per Inch	.3477	.5007	.6815	.8900	1.301	2.003



# **BOLTS WITH HEXAGONAL HEADS AND NUTS** **WEIGHT IN POUNDS PER 100 BOLTS**

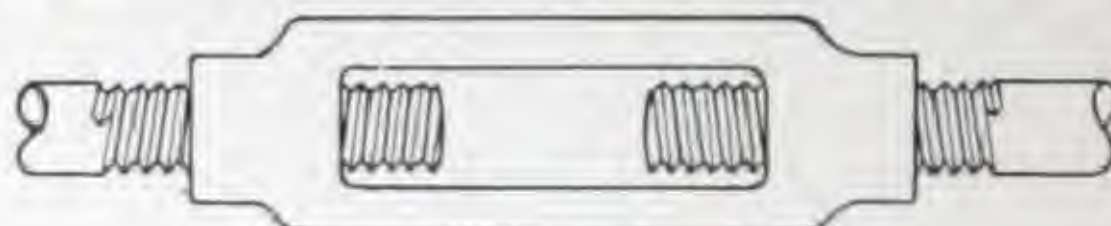
Length Under Head, Inches	Diameter of Bolt, Inches					Length Under Head, Inches	Diameter of Bolt, Inches				
	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{7}{8}$	1	1 1/4		$\frac{1}{2}$	$\frac{3}{4}$	$\frac{7}{8}$	1	1 1/4
1	19	31	32			8	56	93	137	194	264
1 1/4	20	34	34			8 1/2	60	96	143	202	274
1 1/2	22	36	37			9	64	100	149	210	283
1 3/4	23	38	39			9 1/2	66	103	153	215	286
2	24	40	41	50	102	10	68	106	157	220	292
2 1/4	26	43	44	57	107	10 1/2	71	111	164	229	304
2 1/2	27	45	46	60	113	11	74	116	171	238	316
2 3/4	29	47	48	63	118	11 1/2	77	121	178	247	328
3	30	49	50	66	124	12	80	127	187	259	342
3 1/4	31	51	52	69	130	12 1/2	82	131	193	265	348
3 1/2	33	54	55	72	136	13	85	136	200	274	361
3 3/4	34	56	57	75	142	13 1/2	88	140	206	280	368
4	35	58	59	78	148	14	91	144	213	289	381
4 1/4	37	60	61	81	154	14 1/2	93	148	219	296	389
4 1/2	38	62	63	84	160	15	96	153	225	303	397
4 3/4	39	64	65	87	166	15 1/2	99	157	231	310	405
5	41	66	67	90	172	16	102	161	237	317	413
5 1/4	42	68	69	93	178	16 1/2	105	165	243	324	422
5 1/2	44	71	72	96	184	17	107	170	250	333	435
5 3/4	45	73	74	99	190	17 1/2	110	174	256	340	443
6	46	75	76	102	196	18	113	177	262	347	452
6 1/4	48	77	78	105	202	18 1/2	116	182	269	356	465
6 1/2	49	79	80	108	208	19	119	187	275	363	474
6 3/4	51	81	82	111	214	19 1/2	121	191	281	370	483
7	52	84	85	114	220	20	124	196	287	377	492
7 1/4	53	86	87	117	226						
7 1/2	55	88	89	120	232						
7 3/4	56	90	91	123	238						
Per Inch Additional	3.6	4.2	4.3	5.0	5.6	Per Inch Additional	3.6	4.2	4.3	5.0	5.6

## **HEXAGONAL NUTS AND BOLT HEADS** **WEIGHTS IN POUNDS FOR ONE HEAD AND ONE NUT**

Diameter of Bolt, Inches	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{7}{8}$	1	1 1/4	1 1/2
Hexagon Head and Nut	1.70	2.40	3.00	4.70	7.00	10.00
Weight of Shank per Inch	.3477	.5072	.6813	.8881	1.200	1.688



## DROP-FORGED STEEL STANDARD TURNBUCKLES



No. 22—Standard Turnbuckle

These Turnbuckles are drop-forged from the bar, are free from welds and seams, thus making them absolutely reliable and giving a tensile strength of 60,000 pounds or more per square inch.

Diameter of Stub Ends, Inches	Opening between Heads, Inches	Length of Buckle With Ends, Inches	Weights	
			With Stub	Without Stub
			Lb. Oz.	Lb. Oz.
$1\frac{1}{8}$	6	22	1 8	0 12
$1\frac{1}{4}$	6	22	2 8	1 2
$1\frac{3}{8}$	6	23	3 8	1 6
$1\frac{1}{2}$	6	24	4 8	2 0
$1\frac{5}{8}$	6	25	6 8	2 14
$1\frac{3}{4}$	6	25	8 8	3 8
$1\frac{7}{8}$	6	26	10 12	5 0
$1\frac{1}{2}$	6	27	13 0	6 0
$1\frac{5}{8}$	6	27	16 0	7 0
$1\frac{3}{4}$	6	28	19 0	8 12
$1\frac{7}{8}$	6	28	21 8	10 0
2	6	29	26 8	12 8
$2\frac{1}{4}$	6	29	30 8	14 0
	6	30	45 0	19 0

Larger sizes can be supplied but are not carried in stock. Turnbuckles with longer length between heads can also be furnished.

## SQUARE WROUGHT WASHERS

Size Square, Inches	Thickness, Inches	Size of Hole, Inches	Size of Bolt, Inches	Average Number per 100 Pounds
$1\frac{1}{2}$	$1\frac{1}{8}$	$1\frac{1}{8}$	$1\frac{1}{8}$	1,300
$1\frac{3}{4}$	$1\frac{1}{8}$	$1\frac{1}{2}$	$1\frac{1}{8}$	1,100
2	$1\frac{1}{8}$	$1\frac{3}{4}$	$1\frac{1}{2}$	500
$2\frac{1}{4}$	$1\frac{1}{8}$	$1\frac{3}{4}$	$1\frac{3}{4}$	390
$2\frac{1}{2}$	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	315
$2\frac{3}{4}$	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	426
$3\frac{1}{4}$	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	409
$3\frac{1}{2}$	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	250
3	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	166
$3\frac{1}{2}$	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	165
4	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	87
$4\frac{1}{2}$	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	65
5	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	48
6	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	40
6	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	28
6	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	24
6	$1\frac{1}{8}$	$2\frac{1}{8}$	2	21

These can be supplied either black hot galvanized or electric galvanized.



## SQUARE PLATE WASHERS

Heavy plate washers are furnished in large numbers for all classes of structural work. As we always carry a large stock of plates of all sizes and thicknesses, these washers can be turned out very promptly. When ordering always state width, length and thickness of plate, also size of bolt hole.

## CUT, PRESSED OR PLATE WASHERS

We can supply from stock standard cut, pressed or plate washers in the sizes tabulated below for cut round washers.

SPECIFICATIONS FOR CUT ROUND WASHERS

Outside Diameter In.	Size of Hole In.	Thickness Wire Gauge No.	Size of Bolt In.	Average Number in 100 lbs.
$\frac{3}{8}$	$\frac{1}{4}$	18	$\frac{3}{8}$	30,400
$\frac{3}{4}$	$\frac{3}{8}$	16	$\frac{3}{4}$	15,000
$\frac{7}{8}$	$\frac{1}{2}$	16	$\frac{7}{8}$	11,250
1	$\frac{5}{8}$	14	$\frac{1}{2}$	6,800
$1\frac{1}{4}$	$\frac{3}{4}$	13	$\frac{3}{4}$	4,300
$1\frac{3}{4}$	$\frac{7}{8}$	12	$\frac{7}{8}$	2,900
$1\frac{1}{2}$	$\frac{1}{2}$	12	$\frac{1}{2}$	2,250
$1\frac{3}{4}$	$\frac{3}{4}$	10	$\frac{3}{4}$	1,300
$1\frac{1}{4}$	$\frac{1}{2}$	10	1	1,580
2	$\frac{1}{2}$	10	$\frac{1}{2}$	1,010
2	$\frac{3}{4}$	10	$\frac{3}{4}$	1,110
$2\frac{1}{4}$	$\frac{1}{2}$	9	$\frac{1}{2}$	860
$2\frac{1}{2}$	$1\frac{1}{2}$	9	1	625
$2\frac{3}{4}$	$1\frac{1}{4}$	9	$1\frac{1}{4}$	670
$2\frac{1}{2}$	$1\frac{3}{4}$	9	$1\frac{3}{4}$	520
$2\frac{3}{4}$	$1\frac{1}{2}$	9	$1\frac{1}{2}$	570
3	$1\frac{1}{4}$	8	$1\frac{1}{4}$	400
$3\frac{1}{4}$	$1\frac{1}{2}$	8	$1\frac{1}{2}$	300
$3\frac{1}{2}$	$1\frac{3}{4}$	8	$1\frac{3}{4}$	260
$3\frac{3}{4}$	$1\frac{1}{2}$	8	$1\frac{1}{2}$	240
4	$1\frac{3}{8}$	8	$1\frac{3}{8}$	215
$4\frac{1}{4}$	$2\frac{1}{8}$	8	$2\frac{1}{8}$	180
$4\frac{1}{2}$	$2\frac{1}{4}$	8	$2\frac{1}{4}$	175







## STRUCTURAL TIMBER

In building construction, timber is used for the ordinary class of a building of a well-defined nature. It has to be treated to resist the fire risk in a structure and you will go to the expense of treated construction, well construction is used.

Well construction means in framing the timber post and beam is being used instead of so as to expose the bare surface of timber and protected by fire. The columns are supported against moisture with steel post and steel beam, being directly supporting a solid horizontal beam.

Details of steel beams, post beam and rafter, etc., which are considered in our well timber construction, are given on pages 48 to 50.

The strength of structural timber depends upon the kind of wood, the age of the tree, the time of the year in which it was killed, the method of drying, the diameter of the specimen and thickness of its moisture content, the proportion of moisture to wood and the proportion of knots to clear wood.

The tables give the average strength as determined for the building class and size. Therefore, for post and beam timber used for ordinary building work, treated with the commercial grade of creosote, such as can be purchased in the open market, and are the most common used in Western building construction.

The safe loads include the weight of the beams and are computed on the premise that the beams are treated against general deflection. These values are for continuous and continuous spans and continuous in deflection.

The maximum safe loads are limited by the allowable bending stress and horizontal shear of beams have been calculated from the beams.

Maximum safe load =  $\frac{1}{2}$  ft. area of section of safe load stress in compression.

These loads referred also by horizontal load in the tables should not be applied to wood below of the beam in horizontal direction of the grain of the wood.

The theoretical deflection in the center of the span for uniformly distributed and permanently applied loads is obtained from the coefficient of deflection by finding the length of the beam in inches, from the corresponding coefficient, the result obtained only approximates the actual deflection as the modulus of elasticity varies with the moisture content of the wood.

The deflection of beams subjected to other than uniform loading should not exceed 1 inch in the span the table gives the maximum stress for the load, for uniformly distributed and permanently applied loads.

The loads determined by the stress of the wood can be used for the beams for the tables and for the use of the coefficient of deflection.



## TIMBER COLUMNS

The safe load tables of wooden columns which follow, based upon the working unit stresses adopted by the American Railway Engineering Association, give the allowable direct compressive loads for square and round columns.

The safe loads of rectangular columns may be found from the safe loads of square columns by direct proportion of areas, using the safe load unit stress of the square column whose side is equal to the least side of the rectangular section.

The following table gives the safe load in pounds per square inch of sectional area for ratios of

$$\frac{l}{d} = \frac{\text{effective length of column, in inches}}{\text{least side or diameter, in inches}}$$

ranging between limits of 15 and 30.

UNIT WORKING STRESSES IN POUNDS PER SQUARE INCH

$\frac{l}{d}$	Longleaf Pine	Douglas Fir	Spruce	Tamarack	Red Cedar,	Norway Pine
	$1300 \times (1 - l/d60)$	$1200 \times (1 - l/d60)$	$1100 \times (1 - l/d60)$	$1000 \times (1 - l/d60)$	$900 \times (1 - l/d60)$	$800 \times (1 - l/d60)$
15	975	900	825	750	675	600
16	953	880	807	733	660	587
17	931	860	788	717	645	573
18	910	840	770	700	630	560
19	888	820	752	683	615	547
20	867	800	733	667	600	533
21	845	780	715	650	585	520
22	823	760	697	633	570	507
23	802	740	678	617	555	493
24	780	720	660	600	540	480
25	758	700	642	583	525	467
26	737	680	623	567	510	553
27	715	660	605	550	495	440
28	693	640	587	533	480	427
29	672	620	568	517	465	413
30	650	600	550	500	450	400

LONGLEAF PINE  
WHITE OAK  
1300 (1 - l/d60)

DOUGLAS FIR  
WESTERN HEMLOCK  
1200 (1 - l/d60)

SHORTLEAF PINE  
SPRUCE  
1100 (1 - l/d60)

WHITE PINE  
TAMARACK  
1000 (1 - l/d60)



**SQUARE TIMBER COLUMNS**  
SAFE LOADS IN THOUSANDS OF POUNDS

	Lgth. Feet	Side of Square, Inches								
		4	6	8	10	12	14	16	18	20
LONGLEAF PINE WHITE OAK 1300 (1-1/2 in.)	5	15.6								
	6	14.6								
	7	13.5	35.1							
	8	12.5	34.3							
	9	11.4	32.8	62.4						
	10	10.4	31.2	62.4						
	11		29.6	60.3						
	12		28.1	58.2	97.5					
	14		25.0	54.1	93.6	140.4				
	16			49.0	88.4	137.3	191.1			
	18			45.8	83.2	131.0	189.3	249.6		
	20			41.6	78.0	124.8	182.0	249.6	315.9	390.0
DOUGLAS FIR WESTERN HEMLOCK 1200 (1-1/2 in.)	5	14.4								
	6	13.4								
	7	12.5	32.4							
	8	11.5	31.7							
	9	10.6	30.2	57.6						
	10	9.6	28.8	57.6						
	11		27.4	55.7						
	12		25.9	53.8	90.0					
	14		23.0	49.9	86.4	129.6				
	16			46.1	81.6	126.7	176.4			
	18			42.2	76.8	121.0	174.7	230.4		
	20			38.4	72.0	115.2	168.0	230.4	291.6	360.0
SHORTLEAF PINE SPRUCE 1100 (1-1/2 in.)	5	13.2								
	6	12.2								
	7	11.4	29.7							
	8	10.6	29.0							
	9	9.7	27.7	52.8						
	10	8.8	26.4	52.8						
	11		25.1	51.0						
	12		23.8	49.3	82.5					
	14		21.1	45.8	79.2	118.8				
	16			42.2	74.8	116.2	161.7			
	18			38.7	70.4	110.9	160.2	211.2		
	20			35.2	66.0	105.6	154.0	211.2	267.3	330.0
WHITE PINE TAMARACK 1000 (1-1/2 in.)	5	12.0								
	6	11.0								
	7	10.4	27.0							
	8	9.6	26.4							
	9	8.8	25.2	48.0						
	10	8.0	24.0	48.0						
	11		22.8	46.4						
	12		21.6	44.8	75.0					
	14		19.2	41.6	72.0	108.0				
	16			38.4	68.0	105.6	147.0			
	18			35.2	64.0	100.8	145.6	192.0		
	20			32.0	60.0	96.0	140.0	192.0	243.0	300.0

(loads in "heavy" type above horizontal lines are the maximum allowable safe loads)



# **RECTANGULAR TIMBER BEAMS** **ONE INCH THICK**

## **MAXIMUM SAFE LOADS AND LIMITING SPANS**

Species of Timber		Depth of Beam, Inches											
		2	4	6	8	10	12	14	16	18	20	22	24
Max. Safe Loads Lbs.	Douglas Fir	293	587	880	1173	1467	1760	2053	2347	2640	2933	3227	3520
	Spruce	187	373	560	747	933	1120	1307	1493	1680	1867	2053	2240
Min. Spans, Feet	Douglas Fir	1.8	3.6	5.5	7.3	9.1	10.9	12.8	14.6	16.4	18.2	20.0	21.9
	Spruce	2.4	4.9	7.1	9.5	11.9	14.3	16.7	19.0	21.4	23.8	26.2	28.6

## **MAXIMUM SPANS IN FEET**

For Deflections = 1/360 Span

Species of Timber		Depth of Beam, Inches											
		2	4	6	8	10	12	14	16	18	20	22	24
Douglas Fir		1.4	2.8	4.2	5.6	7.0	8.4	9.8	11.2	12.6	14.0	15.4	16.7
Spruce		1.5	2.9	4.4	5.8	7.3	8.7	10.1	11.6	13.1	14.6	16.0	17.5

## **COEFFICIENT OF DEFLECTION FOR PERMANENT LOADS**

Span, Feet	Douglas Fir	Spruce	Span, Feet	Douglas Fir	Spruce	Span, Feet	Douglas Fir	Spruce
1	0.05	0.05	15	10.74	10.31	29	40.14	38.52
2	0.19	0.18	16	12.22	11.73	30	42.96	41.22
3	0.43	0.41	17	13.79	13.24	31	45.87	44.01
4	0.76	0.73	18	15.47	14.84	32	48.88	46.90
5	1.19	1.15	19	17.23	16.53	33	51.98	49.88
6	1.72	1.65	20	19.09	18.32	34	55.18	52.95
7	2.34	2.24	21	21.05	20.20	35	58.47	56.11
8	3.06	2.93	22	23.10	22.17	36	61.86	59.36
9	3.87	3.71	23	25.25	24.23	37	65.34	62.70
10	4.77	4.58	24	27.49	26.38	38	68.92	66.14
11	5.78	5.54	25	29.83	28.63	39	72.60	69.66
12	6.87	6.60	26	32.27	30.96	40	76.37	73.28
13	8.07	7.74	27	34.80	33.39			
14	9.36	8.98	28	37.42	35.91			



# RECTANGULAR TIMBER BEAMS—DOUGLAS FIR ONE INCH THICK

## ALLOWABLE UNIFORM LOAD IN POUNDS

Maximum Bending Stress, 1200 Pounds per Square Inch

Span in Feet	Depth of Beam in Inches											
	2	4	6	8	10	12	14	16	18	20	22	24
2	<b>293</b>											
3	267											
4	178	<b>587</b>										
5	131	533										
6	107	427										
7			<b>880</b>									
8	89	356	800									
9	76	305	686	<b>1173</b>								
10	67	267	600	1067								
11		237	533	948	<b>1467</b>							
12		213	480	853	1333							
13						<b>1760</b>						
14		194	436	776	1212	1745						
15		178	400	711	1111	1600	<b>2053</b>					
16			360	656	1026	1477	2010					
17			343	610	952	1371	1867	<b>2347</b>				
18			320	569	889	1280	1742	2276				
19									<b>2640</b>			
20			300	533	833	1200	1633	2133	2541			
21				502	784	1129	1537	2008	2541			
22				474	741	1067	1452	1896	2400	<b>2933</b>		
23				446	702	1011	1375	1796	2274	2807	<b>3227</b>	
24				427	667	960	1307	1707	2160	2667	3227	
25												<b>3520</b>
26					635	914	1244	1625	2057	2540	3073	
27					606	873	1188	1552	1964	2424	2933	3491
28					580	835	1136	1484	1878	2319	2806	3389
29					556	800	1089	1422	1800	2222	2689	3280
30						768	1045	1365	1728	2133	2581	3072
31												
32						738	1005	1313	1662	2051	2482	2954
33						711	968	1264	1600	1975	2390	2844
34						686	933	1219	1543	1905	2305	2743
35							901	1177	1490	1839	2225	2648
36							871	1138	1440	1778	2153	2560
37												
38							843	1101	1394	1720	2082	2477
39							817	1067	1350	1667	2017	2400
40								1034	1309	1616	1956	2327
								1004	1271	1560	1898	2250
								975	1234	1524	1844	2194
								948	1200	1481	1791	2133
									1168	1441	1744	2070
									1137	1404	1698	2021
									1108	1368	1655	1969
									1080	1333	1613	1920

Loads in "heavy" type indicate the limit for maximum to stress in the horizontal direction of the grain.



# RECTANGULAR TIMBER BEAMS—SPRUCE ONE INCH THICK

ALLOWABLE UNIFORM LOAD IN POUNDS  
Maximum Bending Stress, 1000 Pounds per Square Inch

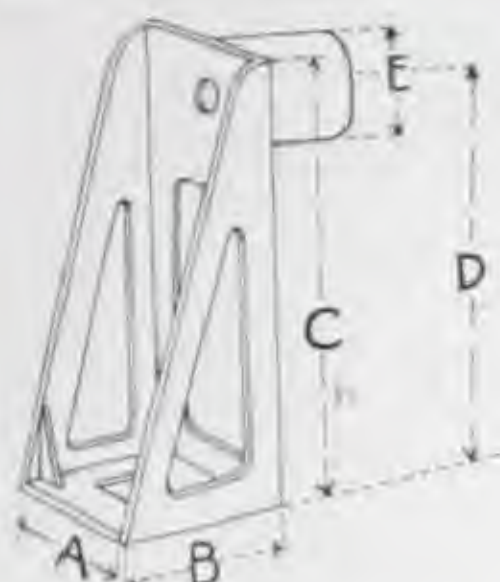
Span in Feet	Depth of Beam in Inches											
	2	4	6	8	10	12	14	16	18	20	22	24
2	187											
3	148											
4	111	373										
5	89	356										
6	74	296										
7	63	254	560									
8	56	222	500									
9		198	444	747								
10		178	400	711								
11		162	364	646	933							
12		148	333	593	926							
13			308	547	855							
14			286	508	794	1120						
15			267	474	741	1067						
16			250	444	694	1000	1307					
17				418	654	941	1281					
18				395	617	889	1210					
19				374	585	842	1146	1493				
20				356	556	800	1089	1422				
21					520	762	1037	1354	1680			
22					505	727	990	1293	1636			
23					483	696	947	1237	1593	1867		
24					463	667	907	1185	1500	1832		
25						640	871	1138	1440	1778		
26						615	838	1094	1385	1709	2053	
27						593	807	1053	1333	1646	1992	
28						571	778	1016	1290	1587	1921	2240
29							751	981	1241	1533	1854	2197
30							726	948	1200	1481	1793	2133
31							703	918	1161	1434	1735	2065
32							681	889	1125	1389	1681	2000
33								862	1061	1347	1630	1930
34								837	1030	1307	1582	1862
35								813	1000	1270	1537	1820
36								790	966	1235	1494	1778
37									973	1201	1453	1730
38									947	1169	1415	1684
39									923	1140	1379	1641
40									900	1111	1344	1600

Beams of "heavy" type indicate the limit for uniformity of stress in the horizontal direction of the grain.

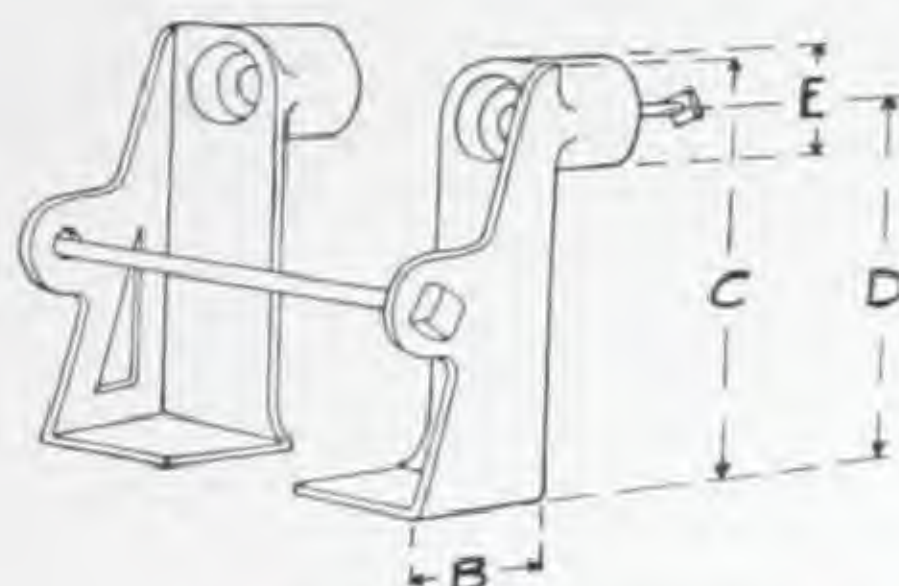


## JOIST HANGERS

The old method of framing by mortise and tenon is obsolete. The use of joist hangers reduces joist-shrinkage to a minimum. Building construction experts find that all headers six feet long or over should be carried on joist hangers, while all framing in warehouses and first-class buildings should be done by means of means of joist hangers.



No. 26—Duplex Joist Hanger



No. 27—Duplex Joist Hangers, in Pairs

## SPECIFICATIONS FOR DUPLEX JOIST HANGERS

No.	Dimensions, Inches					Length Lug, In.	Carries Joist, Sizes, In.		Ship. Wt., Lbs.
	A	B	C	D	E				
10	2	3	5 $\frac{3}{4}$	5	1 $\frac{1}{2}$	1 $\frac{3}{4}$	2 x 6 to 2 x 10		2 $\frac{1}{4}$
14	2	3	8	7	1 $\frac{3}{4}$	2	2 x 12 to 2 x 16		3 $\frac{1}{8}$
15	3	3	5 $\frac{3}{4}$	5	1 $\frac{5}{8}$	2 $\frac{1}{4}$	3 x 6 to 3 x 10		2 $\frac{3}{4}$
18	2 $\frac{1}{2}$	3	8	7	1 $\frac{3}{4}$	2 $\frac{1}{2}$	2 $\frac{1}{2}$ x 6 to 2 $\frac{1}{2}$ x 16		3 $\frac{1}{2}$
20	4	3	5 $\frac{3}{4}$	5	1 $\frac{3}{4}$	2	4 x 6 to 4 x 10		3
21	3	3	8	7	1 $\frac{7}{8}$	2 $\frac{1}{2}$	3 x 12 to 3 x 14		3
21X	3	3	10	9	1 $\frac{7}{8}$	2 $\frac{1}{2}$	3 x 16 to 3 x 20		4 $\frac{3}{4}$
28	4	3 $\frac{1}{2}$	8 $\frac{1}{4}$	7	1 $\frac{3}{8}$	2 $\frac{3}{4}$	4 x 12 to 4 x 14		4 $\frac{1}{2}$
28X	4	3 $\frac{1}{2}$	10	9	2 $\frac{3}{8}$	2 $\frac{7}{8}$	4 x 16 to 4 x 20		7 $\frac{1}{2}$
53	5	3 $\frac{1}{2}$	8 $\frac{1}{4}$	7	2 $\frac{3}{8}$	3	5 x 8 to 5 x 16		5 $\frac{1}{2}$
16	6	3 $\frac{1}{2}$	6	5	2	2 $\frac{3}{4}$	6 x 6 to 6 x 9		4
60	6	3 $\frac{1}{2}$	8 $\frac{1}{4}$	7	2 $\frac{3}{8}$	3	6 x 10 to 6 x 12		6 $\frac{1}{8}$
60X	6	4	9 $\frac{1}{2}$	8	2 $\frac{3}{8}$	3	6 x 14 to 6 x 16		8 $\frac{3}{4}$
80	8	4	8 $\frac{1}{4}$	7	2 $\frac{3}{8}$	3 $\frac{1}{4}$	8 x 8 to 8 x 12		10 $\frac{1}{2}$
90	8	4	9 $\frac{1}{2}$	8	2 $\frac{3}{8}$	3	8 x 16 to 8 x 18		14
35R		3 $\frac{3}{4}$	8 $\frac{1}{4}$	7	2 $\frac{3}{8}$	3 $\frac{1}{4}$	8 x 8 to 8 x 14		9 $\frac{1}{2}$
35L							10 x 10 to 10 x 14		pr.
75R		4 $\frac{1}{4}$	11 $\frac{1}{2}$	10	2 $\frac{7}{8}$	3 $\frac{1}{2}$	10 x 16 to 10 x 18		19 $\frac{1}{2}$
75L									pr.

Nos. 35 R and L and 75 R and L are used in pairs as shown in illustration No. 27 above. Weights of these are per pair, without bolts.



## WALL HANGERS

In a warehouse intended to be constructed on slow burning principle the floor beams and girders should be anchored to and supported by the walls in such a way that in case the beams are burnt through the ends may fall without injuring the wall, and where large timbers are used provision should be made against the possibility of dry rot. When the wall hanger is used to hold a tie in the wall and the saving of six inches in the length of the timbers is effected which in some cases would be a consideration.

The Duplex hanger, an ideal hanger for general construction use, is shown by No. 28, on the right. In heavier work, an extra durable type of this style hanger, shown below is used. Tables showing the size of joist carried by each size of wall hanger, and shipping weights of hangers, are given herewith.



No. 28—Duplex Wall Hanger

No.	Carries Joist, Size, In.	Shipping Weight, Lbs.	No.	Carries Joist, Size, In.	Shipping Weight, Lbs.
100	2 x 6 to 2 x 12	2 1/4	280	4 x 12 to 4 x 18	6 1/4
180	2 x 14 to 2 x 18	3 1/4	500	5 x 8 to 5 x 10	10
190	3 x 6 to 3 x 12	4	600	6 x 8 to 6 x 10	11 1/4
210	3 x 14 to 3 x 18	5 1/4	800	8 x 8 to 8 x 14	13 1/4
280	4 x 9 to 4 x 10	2 1/2	1000	10 x 10 to 10 x 12	18

For heavy mill construction work, the extra heavy steel wall hanger shown by No. 29 herewith is highly adaptable. It is provided with a plate that has eight



No. 29—Extra Heavy Duplex Wall Hanger

inches of bearing on the wall and the bearing of the timbers on the hangers is also eight inches.

Wall hangers made from extruded shapes should not be used for heavy beams.

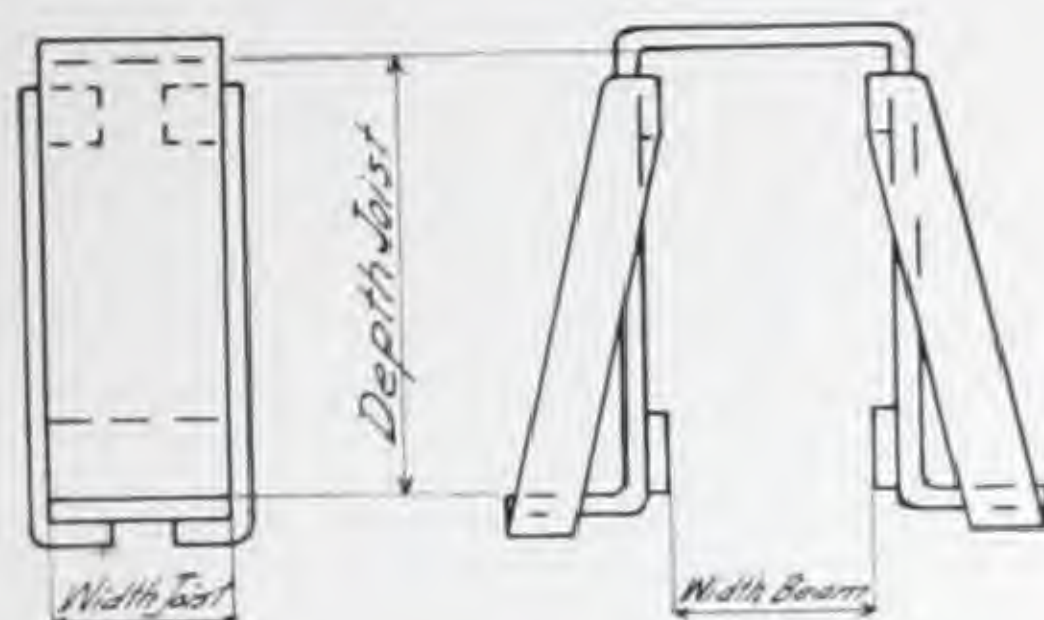
We carry all sizes of the extra heavy wall hanger in stock, the tables below show the size of joist carried by each size of wall hanger.

No.	Carries Joist, Size, In.	Shipping Weight, Lbs.	No.	Carries Joist, Size, In.	Shipping Weight, Lbs.
800	8 x 14 to 8 x 18	24	1400	14 x 14 to 14 x 18	55
1000	10 x 14 to 10 x 18	35	1600	16 x 16 to 16 x 20	58
1200	12 x 14 to 12 x 18	52			



## WELDED HANGERS

The welded style of hanger combines strength and durability with economy in cost.

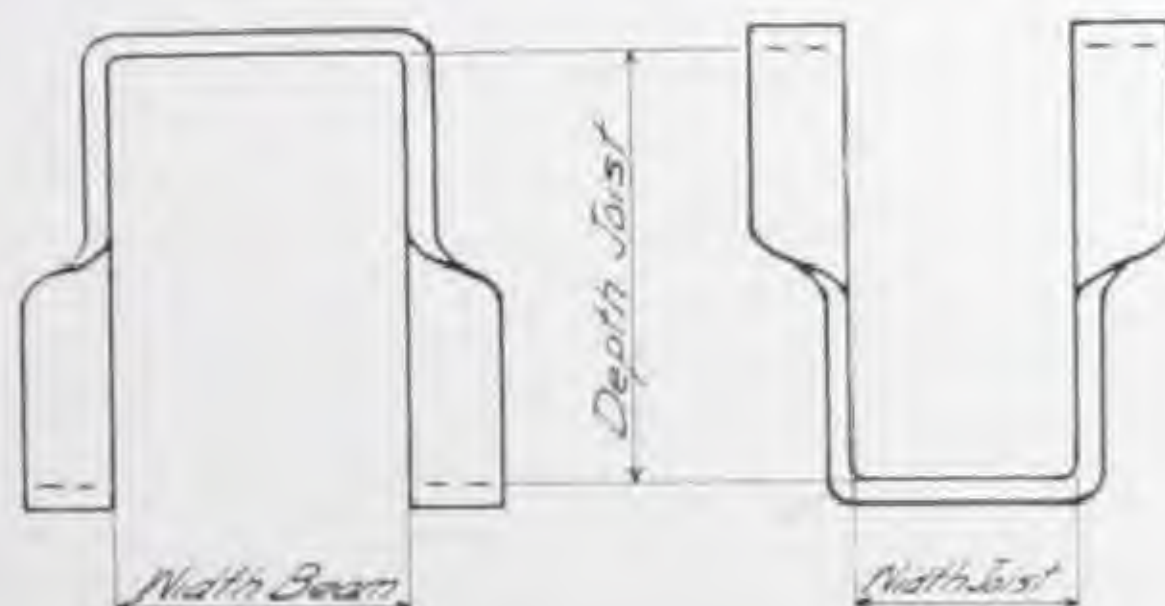


No. 30—Standard Welded Hanger

Welded hangers are made in all sizes, to suit dimensions of timber and thicknesses of material necessary for required loads.

## STIRRUPS

Stirrups can be made up very quickly in our forge shop and orders for any number of any size can be executed promptly; we carry a large range of bar iron, flats and rounds from which these stirrups are made. Sometimes holes for lag screws or wire spikes for spiking stirrups to the timbers are wanted. Unless otherwise specified in the order we will always ship stirrups without holes.



No. 31—Double Stirrup

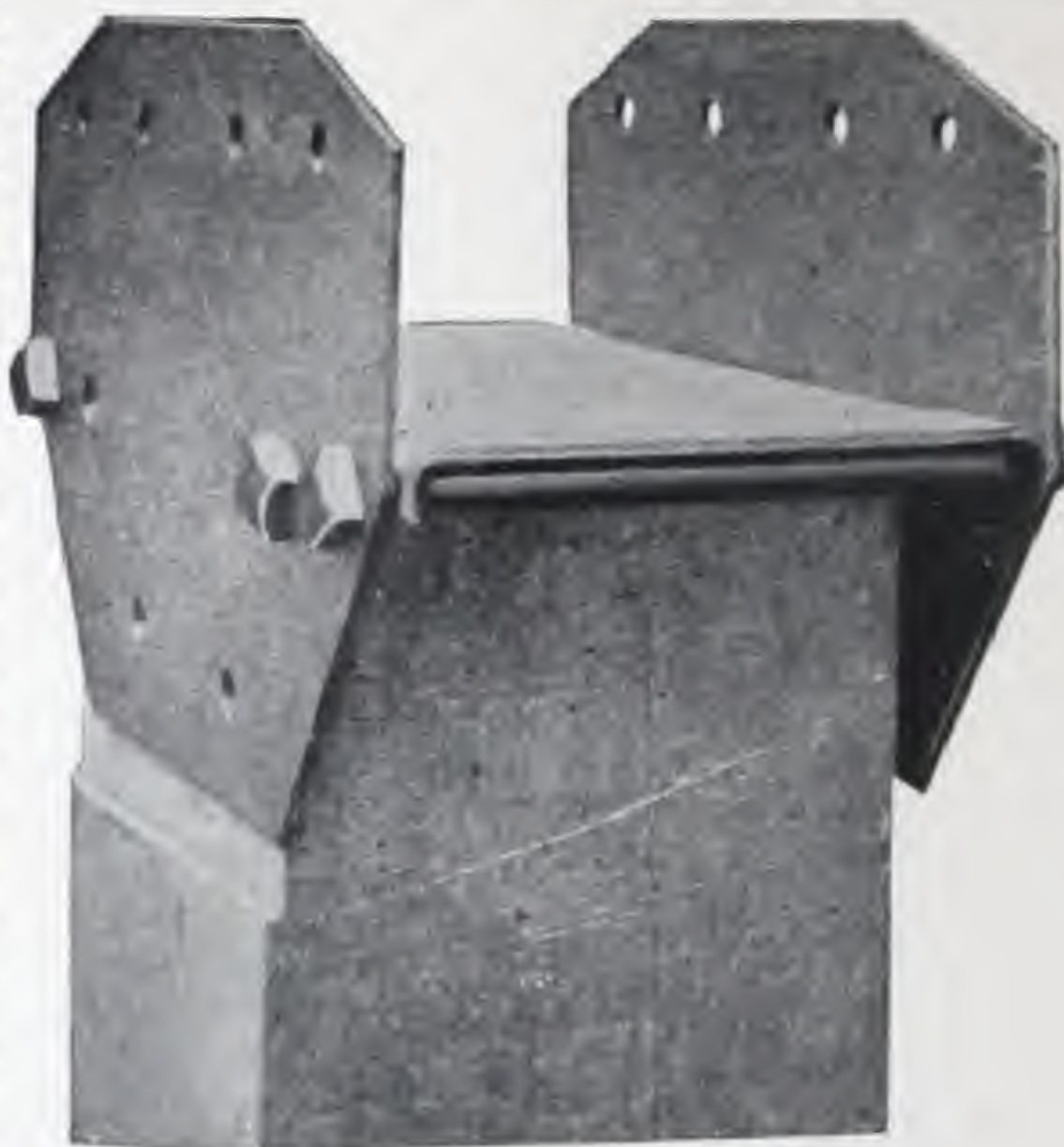
Double stirrups are used when two beams or joists are to be framed to or carried by one girder or beam; single stirrups are required when one joist or beam is to be framed to or carried by a girder or beam. When ordering stirrups always state the width and depth of the carrying girder as well as the joists or beams to be carried; also state whether single or double stirrups are wanted. If size of iron is not given we will furnish the proper size for the timbers specified. Stirrups are usually made of flat bar iron as shown but may also be made of round iron, which would be somewhat less expensive but not so desirable.



## POST CAPS

At the present time, there are a number of different types of post caps in general use, the best-known and most popular being the Duplex, illustrated herewith; we sell other styles, however, as requested. Ordinary sizes can be shipped from stock promptly.

The cap of the Duplex is made in three or more pieces of mild steel. For post caps up to 12-inch,  $\frac{1}{2}$ -inch steel is used, and for heavier construction  $\frac{3}{8}$  or  $\frac{1}{2}$ -inch plates and bearing brackets are provided. The weight of the girder is carried on the shoulder formed on the post. The heavy bolts underneath the bearing brackets relieve the outer edge of the bracket and transmit the load directly to the post. The outer bolt is directly underneath the bearing bracket, while the inner bolt is close up against the post. The post cap is fastened to the post by lag screws forming a most rigid construction and virtually making a continuous post. The cap may be used for a continuous post by cutting the bearing brackets in the centre and notching the post to form a shoulder for the bearing bracket. These caps on account of their simple construction are readily made up to any desired detail and we illustrate a few of the stock sizes.



No. 32—Two-Way Post Cap

No. 32 represents the standard two-way cap while No. 33 shows a two-way post cap with bent-in side plates to accommodate a 10-inch girder with a 10 x 10



With Bent-in Side Plates

With Offset Side Plates

No. 33—Types of Two-Way Post Caps

inch post above and a 12 x 12-inch post below, as well as a two-way cap with offset side plates to carry a 14-inch girder, with a 10 x 10-inch post below.

In addition to two-way post caps, three-, four- and one-way caps are used; the latter two styles are illustrated on the following page.



No. 34 represents a four-way post cap to carry four 10-inch girders on a 10 x 10-inch post. A different style of four-way cap is seen in illustration No. 35,

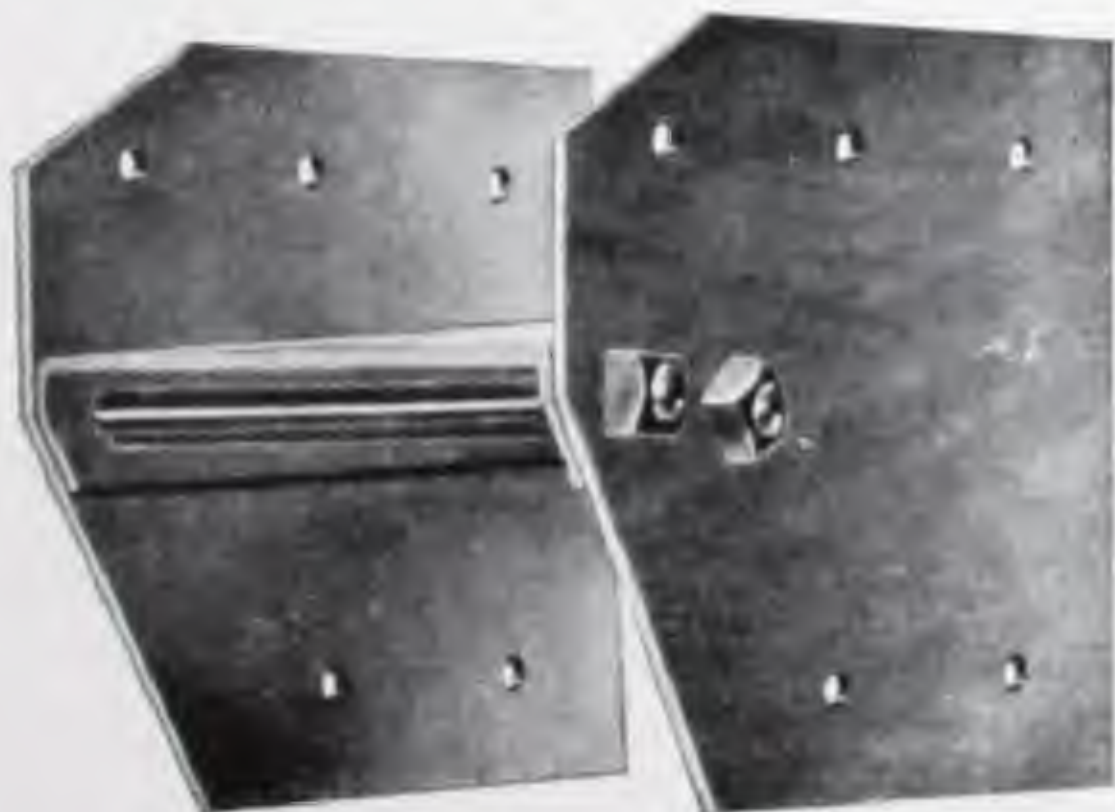


No. 34—Four-Way Post Cap



No. 35—Four-Way Post Cap, Offset

indicating a cap to carry two 14-inch girders and two 10-inch girders on a 10 x 10-inch post.



No. 36—One-Way Post Cap

The one-way cap is shown by No. 36 above, illustrated to carry one 12-inch girder on a 12-inch post.



## SHIPPING WEIGHTS OF TWO-WAY DUPLEX POST CAPS

Size Post, In.	Size Girder, In.	Off-set, In.	Ship. Wt., Lbs.	Size Post, In.	Size Girder, In.	Off-set, In.	Ship. Wt., Lbs.	Size Post, In.	Size Girder, In.	Off-set, In.	Ship. Wt., Lbs.
6 x 6	6	0	30	10 x 10	12	1	57	14 x 14	18	2	140
6 x 6	8	1	31	10 x 10	14	2	69	16 x 16	16	0	155
6 x 6	10	2	34	12 x 12	12	0	72	16 x 16	18	1	160
8 x 8	8	0	35	12 x 12	14	1	76	16 x 16	20	2	168
8 x 8	10	1	36	12 x 12	16	2	84	18 x 18	18	0	190
8 x 8	12	2	40	14 x 14	14	0	124	20 x 20	20	0	220
10 x 10	10	0	52	14 x 14	16	1	132				

For three-way caps, add 25%. For four-way caps, add 50%. Bent-in caps should be estimated same as offset. Weights include bolts.

## MISCELLANEOUS POST CAPS

Very serviceable and low priced post caps can be made up of standard channel, I-beam and angle sections as illustrated. The different parts are rivetted together as shown. Hundreds of them are sold for building construction in all parts of Western Canada. The angles form the post cap and the channel or I-beam carries the girder. Post caps of this description can be made of any size up to the limit of



No. 27—Steel Post Cap—Channel and Angles Rivetted



No. 28—Steel Post Cap—I-Beam and Angles Rivetted

size of standard rolled sections of I-beams and channels. The angles are spiked to the post and the channel or I-beam is spiked to the girders. The girders should be securely fastened together lengthwise with iron straps or dogs. As we always carry a large stock of all sizes of I-beams, channels and angles, steel post caps of this kind can be made up very readily of any required size and shipped promptly. They are sold either at so much per 100 lbs. or at a stated price for any number required. Size of post and of girders should be given when writing for prices.



## POST BASES

Both steel and cast iron bases are used for various grades. The most commonly used styles are illustrated but other types of bases can be made up if desired.



Fig. 38 Steel Post Base

The illustration shows above a steel post base made up of a plate of angles all riveted together and properly finished off. These bases can be made up for steel and cast iron and will be shipped promptly. Please see specifications.



Fig. 39 Cast Iron Post Base

We have on hand a large quantity of cast iron bases which can be made for steel and cast iron bases. You will observe above and right that various models, various in grade. Any style can be made up to suit your needs, and shipped promptly. Take stock of your other columns, and specify whether round or square. Please see specifications.



## JOIST ANCHORS AND BEAM TIES

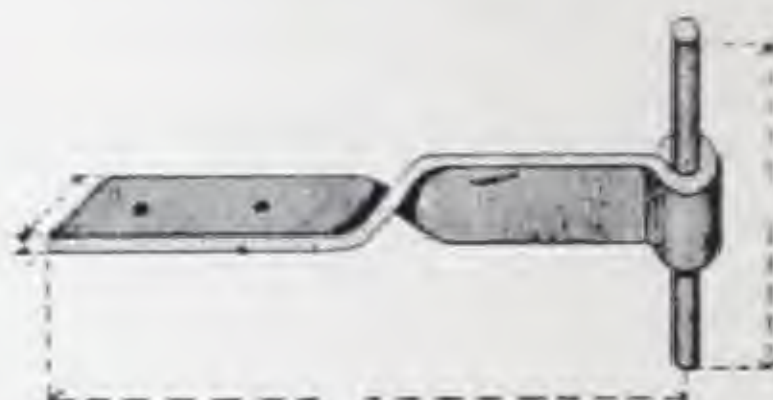
Several styles of joist anchors and dogs, beam anchors and ties are illustrated herewith. We can supply any style desired in these lines.



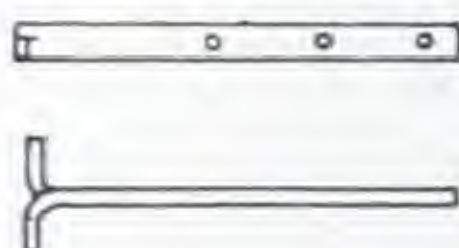
No. 41—Wrought Iron Joist Anchor with Round Face Plate.



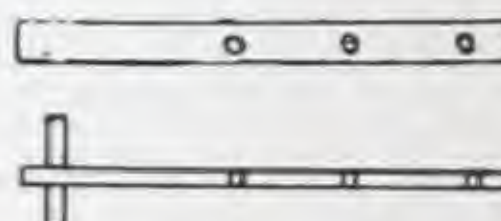
No. 42—Wrought Iron Joist Anchor with Pin.



No. 43—Wrought Iron Joist Anchor with Pin.



No. 44—Wrought Iron Joist Anchor with Split End.



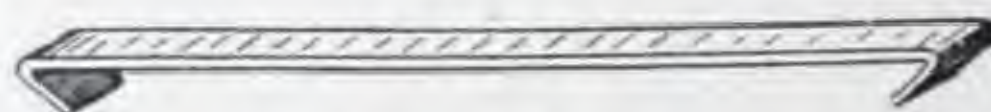
No. 45—Wrought Iron Joist Anchor with Pin.

No. 41 shows a joist anchor for use on either side or top of joist. Nos. 42 and 43 are used fastened to side, and Nos. 44 and 45 fastened to top of joist.



No. 46—Wrought Iron Dog.

The wrought iron dog shown above is used for connecting joists or beams.



No. 47—Wrought Iron Tie



No. 48—Wrought Iron Pin Anchor

The tie and anchor illustrated above are for use with I-beams.

When ordering give dimensions, and number and size of holes wanted. Estimates for quantity orders will gladly be submitted.



## BRIDGE BOLTS

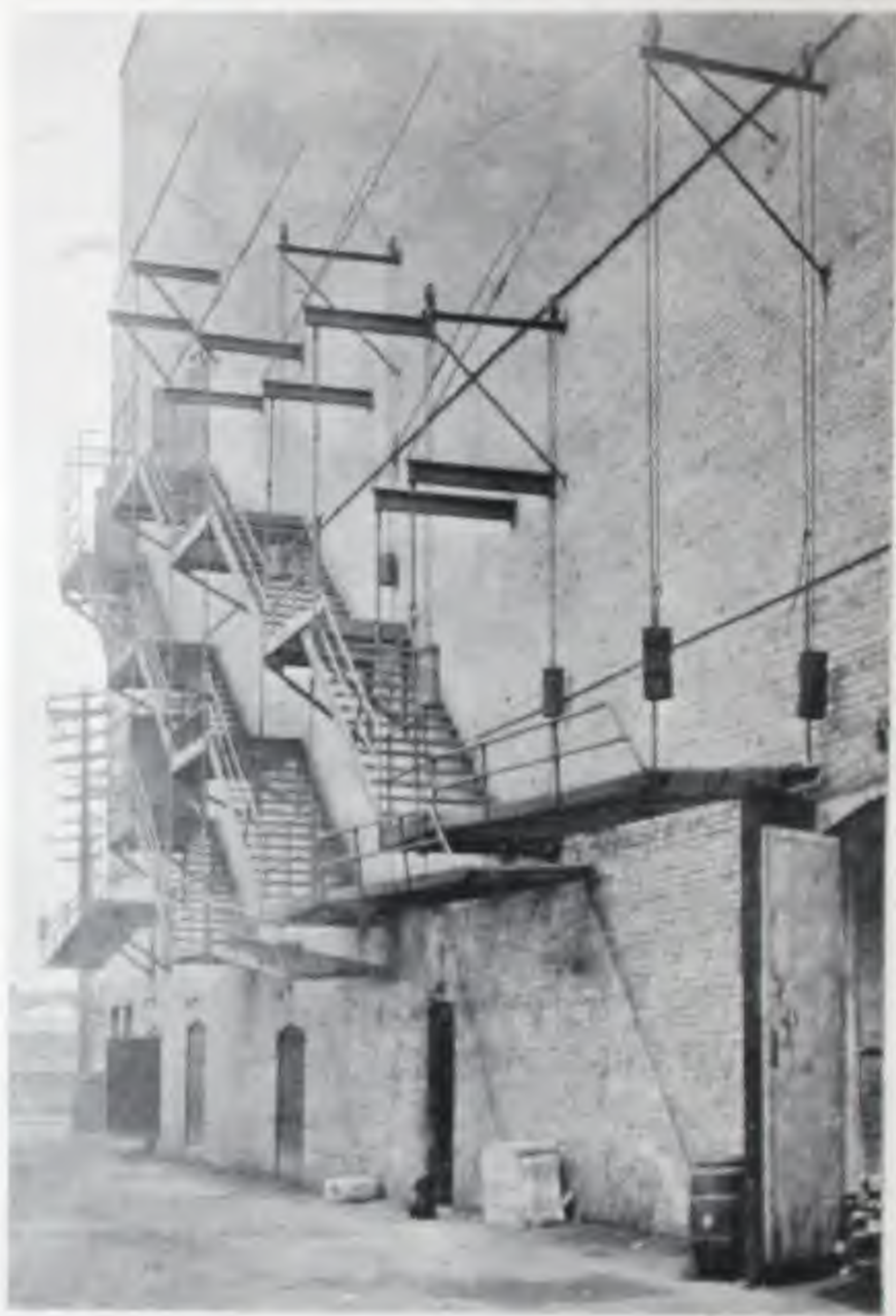


No. 4

- |   |   |   |
|---|---|---|
| A—Lag screw.                                      | H—Hexagonal bolt, wedge point, with nut head.   | W—Washer, flat or round, with head nut.         |
| B <sub>1</sub> —Bridge bolt, square head and nut. | I—Washer.                                       | X—Hexagonal washer, with cross bridge washer.   |
| C—Round head, wedge point, drill spike.           | J—Round, sharp point, drill spike without head. | Y—Square, with cross, angle or lateral washer.  |
| D—Round head, wedge point, drill spike.           | K—Round, sharp point, drill spike without head. | Z—Square, with cross, angle or lateral washer.  |
| E—Square, sharp point, drill spike, without head. | L—Round, sharp point, drill spike without head. | AA—Square, with cross, angle or lateral washer. |
| F—Square, sharp point, drill spike, without head. | M—Round, sharp point, drill spike without head. | BB—Square, with cross, angle or lateral washer. |
| G—Round, sharp point, drill spike, without head.  | N—Round, sharp point, drill spike without head. | CC—Round, with cross, angle or lateral washer.  |
| H—Hexagonal bolt, wedge point, with nut head.     | O—Cross section, bridge washer with nut.        |   |
| I—Washer.   |   |   |
| J—Round, sharp point, drill spike without head.   |   |   |
| K—Round, sharp point, drill spike without head.   |   |   |
| L—Round, sharp point, drill spike without head.   |   |   |
| M—Round, sharp point, drill spike without head.   |   |   |
| N—Round, sharp point, drill spike without head.   |   |   |
| O—Cross section, bridge washer with nut.          |   |   |
| P—Cross section, bridge washer with nut.          |   |   |
| Q—Cross section, bridge washer with nut.          |   |   |

Notes.—In ordering from above list, care must be taken to specify length, diameter, style of head and nut, thickness of washer, size of hole, degree of angle, and whether washer is used or not.





No. 50—View of Shop at West of Third St. Showing Lateral Bracing System with Counterweights.

**Notes.**—When the company other than those illustrated in this section are required, sketches and measurements showing how they are to be made up must be forwarded to us before we can quote prices or manufacture the company.



## FIRE ESCAPES

A modern fire escape consists of one or more balconies or landings, securely fastened to the wall of a building opposite some convenient exit, either door or window, with a stairway so placed that the occupants of the building can reach the ground in safety from any balcony in case of fire. The fire escape, including stairs and ladder, should be constructed of steel, wrought iron or a combination of both. Fire escapes may be plain or as ornamental as required. In every case the balconies or landings, with their supporting brackets, should be strong enough to carry safely as many people as can be crowded on to them. It is customary to provide a ladder extending from the topmost balcony to the roof. At the lowest balcony a drop stairway is usually provided, which may be kept off the ground when not in use. Stairs with counterweights are shown by No. 50. The counterweight is enclosed in a pipe to prevent possibility of accident.

Our Standard Fire Escape, designed to conform to by-laws of the city of Winnipeg, is the most serviceable and least expensive on the market to-day. Several hundred have been sold during the past few years. The balconies consist of steel angle frame work with flat steel strap floor, carried on strongly-made steel brackets. Either ladder or stairs may be provided, as required. The ladders are well made, and if properly attached to wall will safely carry as many people as can get on them at one time. The stairs have steel channel or bar strings, with bar treads, no risers.

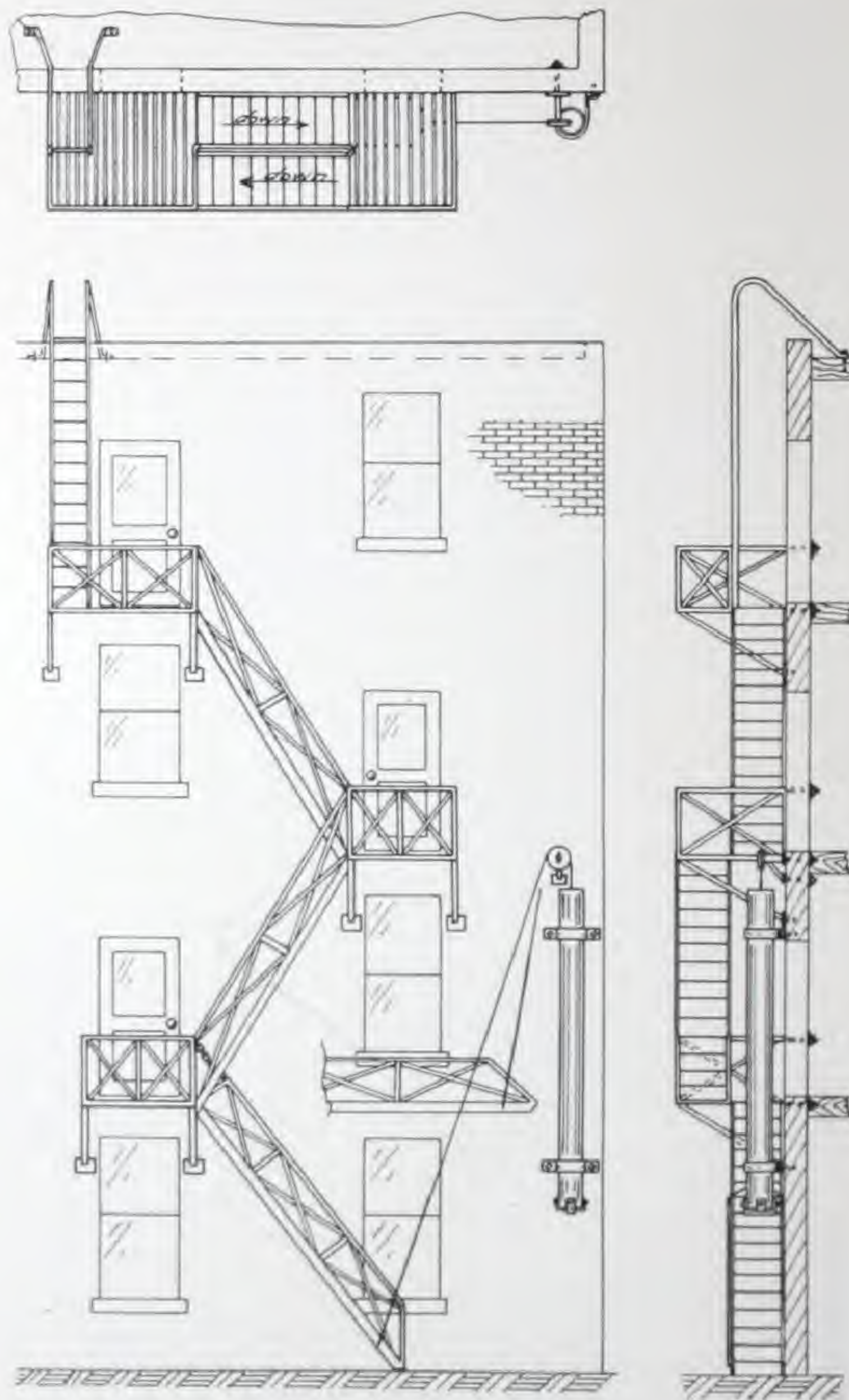
Balconies and stairs may have either angle railings or pipe railings. Angle railings are the least expensive and being made of steel will, if properly painted, last as long as any other kind. When fire escapes are ordered we will always furnish steel angle railings to both stairs and balconies unless otherwise instructed.

These fire escapes are shown by Nos. 50 and 51. We sell these standard fire escapes L.O.B. Winnipeg, made up with all fittings ready for erection.

When ordering or asking for prices on fire escapes it is necessary for us to have the following information:

- A—Length and width of balcony.
- B—Whether angle or pipe railing is required.
- C—Location of stair or ladder opening in floor or balcony; whether at right, left, or in centre.
- D—Number of lineal feet of ladder.
- E—Whether opening in floor for stand pipe is to be provided or not.
- F—Whether ladder or stairs are required.
- G—Whether ladder is to be attached to wall or to outside of frame work of balcony.
- H—Thickness of wall at each landing, so that we may know what length to make the bracket bolts.
- I—Width and height of parapet on roof, if any.
- J—Projection and depth of cornice, if any.
- K—If stairs are wanted, always give the "rise" and the "run". By "rise" we mean the vertical height from ground level to floor of lowest balcony or vertical height from the floor of each balcony to the floor of the one above. The "run" means the length of base of a triangle of which the stairs form the diagonal or longest side. Considering any flight or section of stairs, the stairs themselves would be one side, diagonal, of a triangle; the "rise" would be the vertical side and the "run" the base. These measurements should be given as correctly as possible to avoid mistakes.





No. 51—Standard Fire Escape, with Stairs

Specifications for this fire escape may be found on page 102.

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## CHUTE FIRE ESCAPES



No. 52—Chute Fire Escape

Chute fire escapes are used very extensively for country schools, their advantages over the ordinary stair type for children being obvious.

The illustration at the left, No. 52, illustrates a chute fire escape actually installed on a Manitoba school.

The top balcony is of the usual fire escape type, while the chute is constructed of twenty-gauge galvanized iron, rolled over a one-inch gas pipe and supported at intervals with flat bar brackets.

The inside of the chute and the rods are made perfectly smooth, and all corners are rounded.

The slope of the chute is usually 8 inches in 12 inches and at the bottom is a horizontal section about six feet long, two feet above the ground, being supported on four pipe standards. This straight section decreases the speed of the children sliding down and allows of adults standing at side to help the children clear of the escape as they come down.

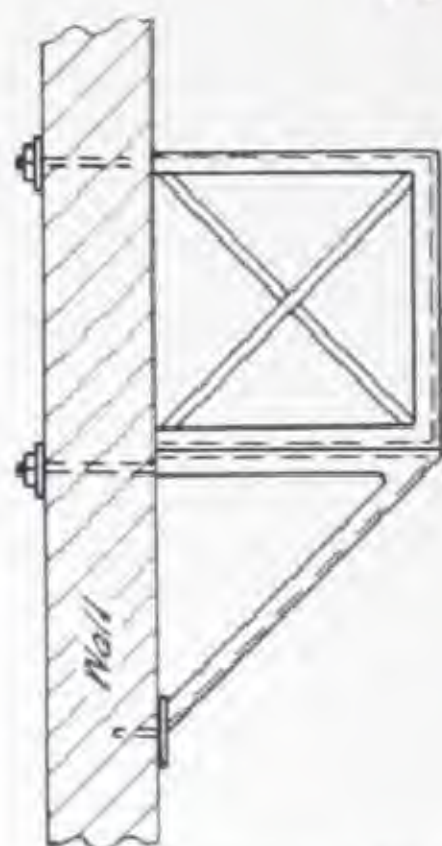
Sometimes the bottom section of the escape is made with a hinged section and counterweight as shown on the right in illustration No. 53.



No. 53—Chute Escape with Counterweight



# FIRE ESCAPE SPECIFICATIONS



No. 54—Showing End View of Balcony

## STANDARD STYLE

### Balcony

Steel angle frame-work; flat steel strap floor, rivetted.

### Brackets

Steel angles and bolts through wall.

### Ladders

Side bars,  $1\frac{1}{2}$  x  $\frac{5}{8}$ -inch steel; rungs,  $\frac{3}{8}$ -inch square bars.



No. 55—Detail of Standard Tread

## Treads

Made of  $1\frac{1}{4}$  x  $\frac{1}{4}$ -inch bars. The advantage of these treads is that no snow or ice will lodge in them; thus they are non-slip. This is the only type of tread now approved by by-laws for outside fire escapes.

## CHUTE STYLE

### Chute

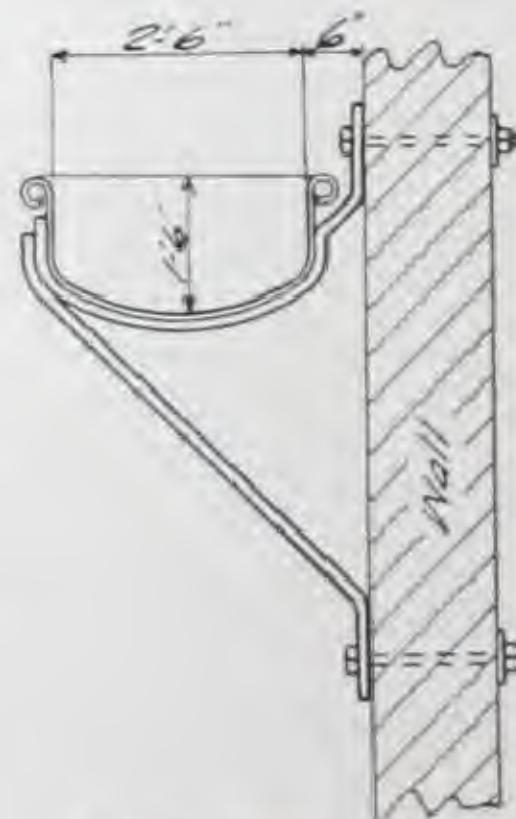
Galvanized iron construction, 20-gauge.

### Brackets

Flat bars, 3 x  $\frac{5}{8}$ -inch;  $\frac{3}{4}$ -inch bolts through walls.

### Chute Beading

1-inch gas pipe with galvanized iron rolled over and soldered.



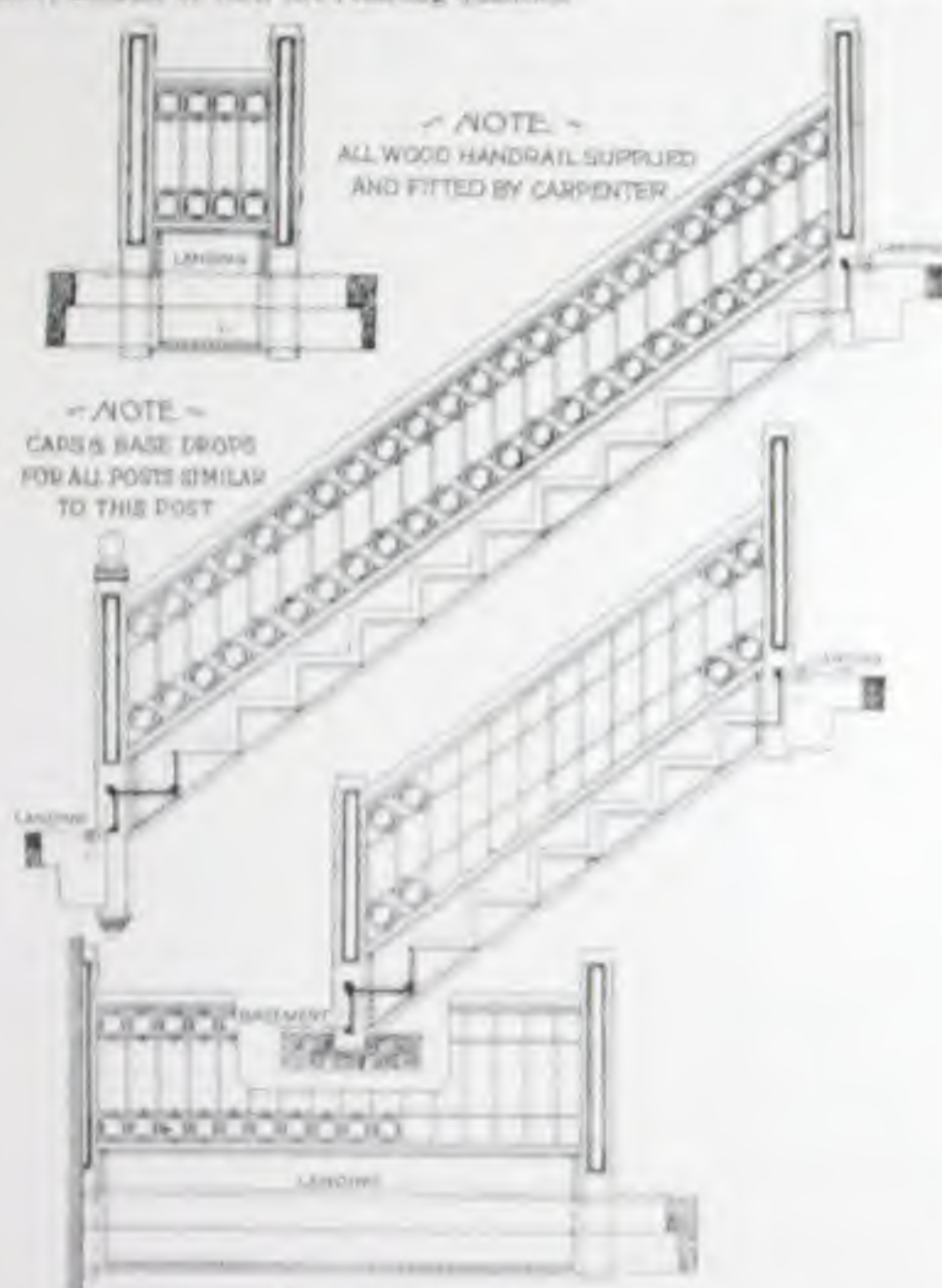
No. 56—Section of Chute Fire Escape

All fire escapes are assembled and properly fitted in our shops before shipment, and mistakes are not often made through any fault of ours. Workmanship is first-class.



## STEEL AND IRON STAIRS

In municipal buildings, hotels, apartment houses, theatres, churches, office buildings, etc., interior stairways should be made of steel or iron or a combination of both, because of their fire resisting qualities.



No. 57 - Ornamental Iron Stairway

The design above illustrates our standard type of ornamental iron stairway. Posts or newels are cast iron, patterned. Stringers, both wall and well, are cast iron or steel with exposed surfaces patterned; risers, well castings and nosing are of cast iron or steel, with exposed surfaces patterned; balustrade is wrought iron. As the treads are usually made of slate, stone or marble, metal treads are not furnished unless ordered.

Dimensions of standard stairways are as follows:

Width of stairs, 4 feet.  
Width of tread, 10 inches.  
Height of nosing, 7 inches.

Height of balustrade, 27 inches.  
Width of stringer, 12 inches.  
Width of well casing, 12 inches.  
(varies with thickness of floor)



## SPIRAL STAIRS

Where space is limited and it is necessary to have means of communication between two or more floors, spiral stairs, made of pipe and cast iron, are often used.



No. 58.—Exterior Spiral Stairway.

The illustration on the left depicts one type of stairs we make.

The width of the stairs can be made anywhere from 36 inches to 72 inches, while the spiral may be right or left hand.

Landings can be provided anywhere, but, in this type of stairs, are usually limited in size to two treads, or in very exceptional cases, to three.

The center, or carrying post is made of standard wrought iron pipe, fitted with floor plate at bottom and ball cap at top.

Treads, in most cases, are corrugated cast iron, but can be made lead-filled cast iron, the cost in the latter case being much higher. Information concerning and description of lead-filled treads may be found on page 106.

The following information should be given when ordering:

- A—Total height of stairs
- B—Distance from finished floor to finished floor, each storey.
- C—Whether post is to extend to ceiling; or, if not, how far above top landing.
- D—Width or diameter of stairs.
- E—Size of well or floor openings.
- F—Whether spiral is right or left hand.

We have many other designs of spiral stairways besides that shown on the left; these designs will gladly be supplied to our customers without charge. We have patterns in stock which will enable us to make up these stairs within a few days after receiving order.

Shipping weights range from 44 to 120 lbs. per foot for spiral stairs from three to six feet in diameter.



## IRON CRESTINGS

Iron crestings are used as decorative material for deck ends, walls and copings. Besides the designs of crestings shown on this page, many other styles can be made up at reasonable cost. Further details for any design are obtainable at small additional expense.



No. 88—Weight per Lineal Foot, 5.5 lbs.



No. 89—Weight per Lineal Foot, 5 lbs.



No. 90—Weight per Lineal Foot, 9 lbs.

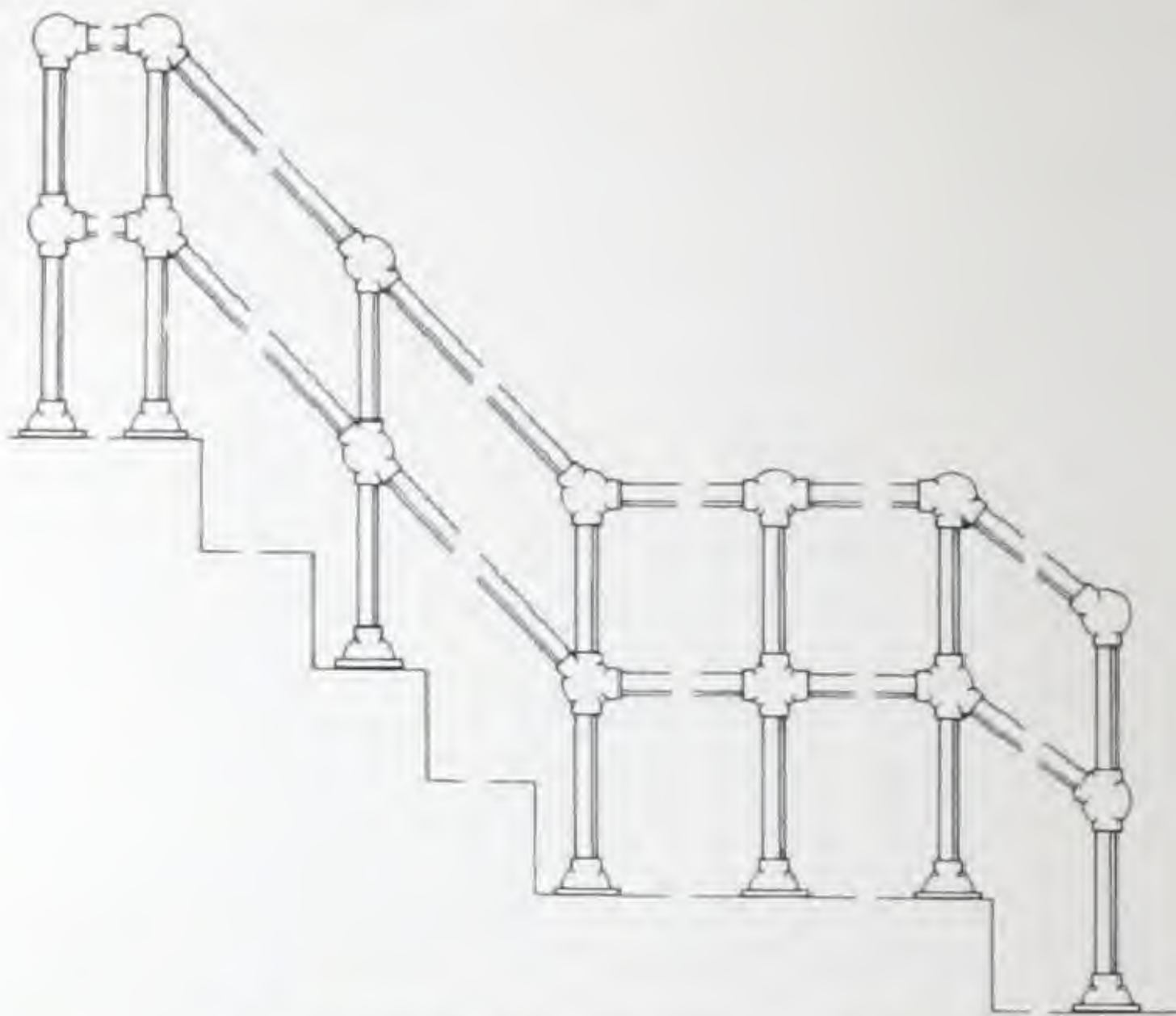


No. 91—Weight per Lineal Foot, 10 lbs.



## PIPE RAILINGS

We make up pipe railings of all sizes for concrete stairs, area railings, etc. These are fitted up complete before shipping.

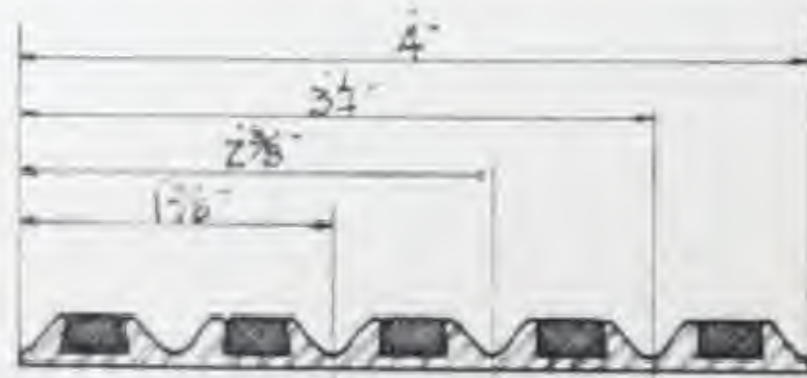


No. 63—Pipe Railing Equipped with Ball Fittings.

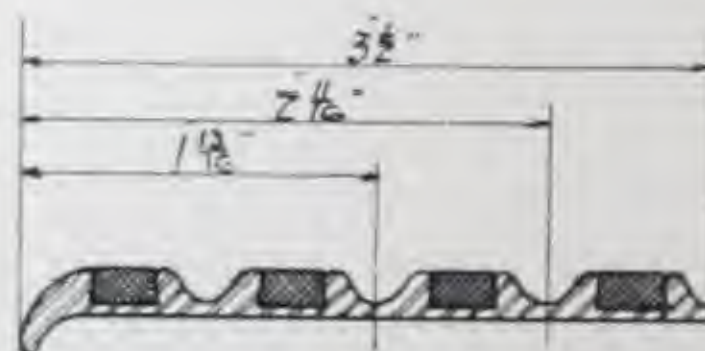
We use ball fittings in making up railings; the different angles of fittings are illustrated above. Our large variety of patterns enables us to furnish railings fully fitted-up, that will cover all requirements and specifications.

## SAFETY TREADS

Lead-filled safety treads for use on concrete steps can be supplied to customer's measurements. These treads are highly durable and afford secure footing in every



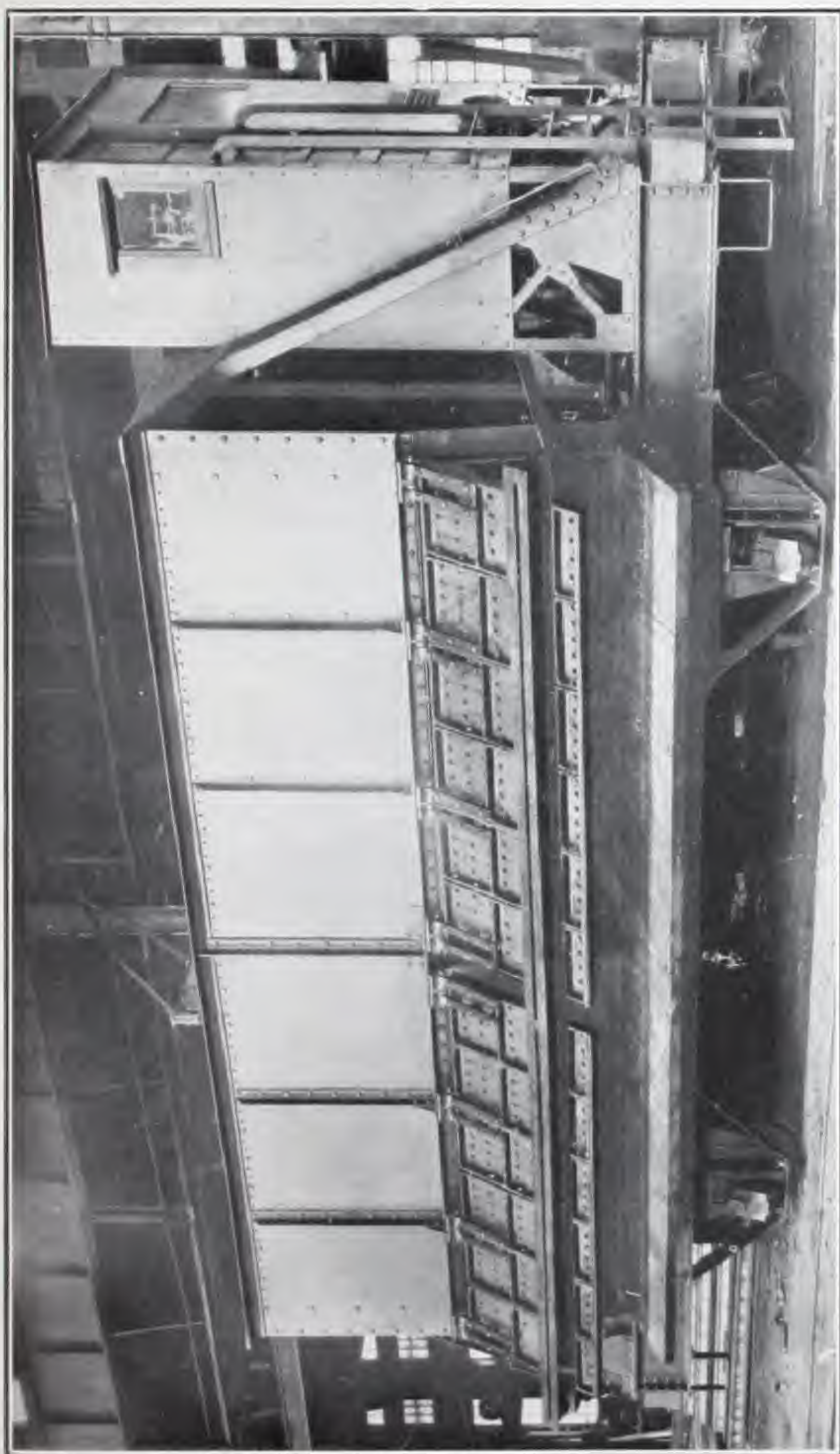
No. 64—Safety Tread



No. 65—Safety Tread with Nosing.

weather. They may be had in depths as indicated in the accompanying diagram, plain or with nosing.



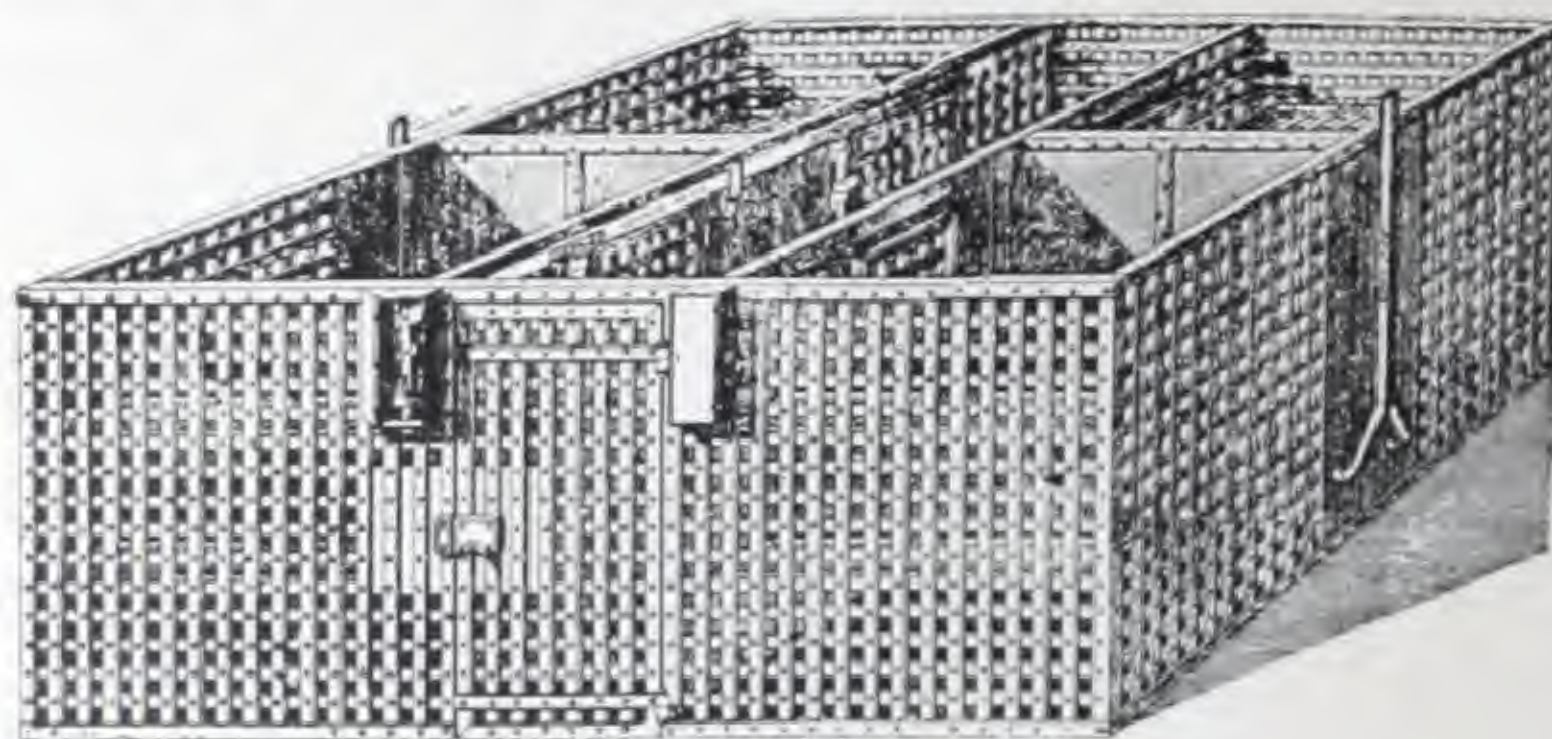


No. 56—Coke Quenching Car built by us for and to the design of the Atlas Car Co., Cleveland, Ohio, for the Winnipeg Electric Company.



## JAIL EQUIPMENT

We will be pleased to enter into correspondence with towns, villages or municipal offices interested in jail and cell fittings.

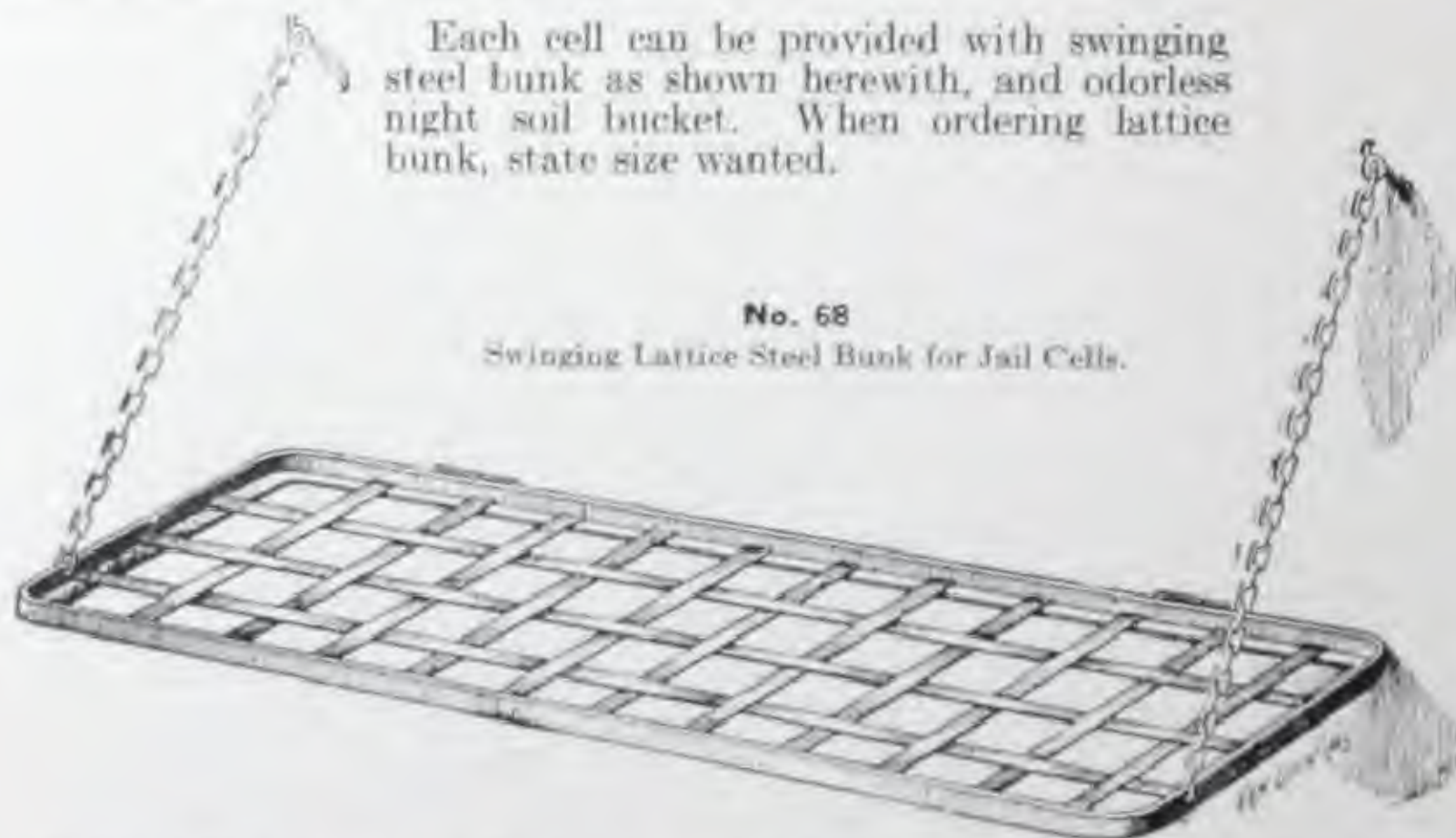


No. 67—Steel Lattice Jail Cells

Above is shown a block of four steel lattice cells with corridor. These cells are usually made of  $1\frac{1}{2}$  x  $\frac{1}{4}$  inch or  $1\frac{1}{2}$  x  $\frac{3}{8}$  inch steel bars, with spaces about  $4\frac{1}{2}$  inches square, securely riveted with heavy rivets at all intersections. The frames are formed of  $1\frac{3}{4}$  x  $1\frac{3}{4}$  x  $\frac{3}{8}$  inch steel angles. Roof can be lattice work same as front, and sides of solid steel plate. Can be made with steel plate floor if desired or to attach to cement or wood floor. Partitions between cells are usually of steel plate lattice work facing corridor. Doors are fitted with improved locks, which afford ample security. All parts are fitted together complete at works before shipment and marked so that any ordinary mechanic can set up the cells without trouble.

We can furnish single cells or blocks of two, four, six or eight cells, with or without corridor. The lattice jail cell is the best medium priced cell made and has given satisfaction wherever installed.

Each cell can be provided with swinging steel bunk as shown herewith, and odorless night soil bucket. When ordering lattice bunk, state size wanted.



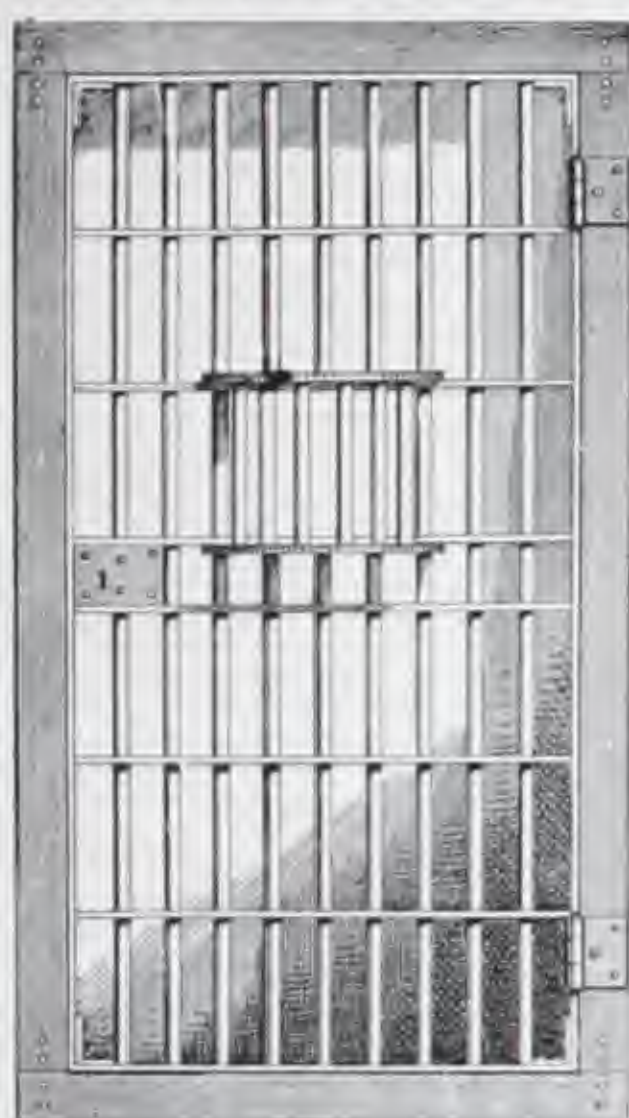
No. 68

Swinging Lattice Steel Bunk for Jail Cells.

On the following pages, illustrations and descriptions of types of jail doors and window-guards will be found. These doors can be constructed as part of the equipment for the jail cells shown above.



The illustrations on this page show jail doors of steel bar, lattice steel and steel plate construction—the styles of doors generally used for entrance to cell-room or jail building. They can be constructed heavier or lighter as occasion demands.



No. 69



No. 70



No. 71



No. 72



No. 73

No. 69, above, illustrates a steel bar jail door with round steel vertical bars, 1-inch diameter; horizontal bars  $2 \times \frac{3}{8}$ -inch; frame,  $2 \times \frac{1}{4}$ -inch; steel; outside frame heavy steel angle; forged hinges; heavy lock. This style of door can be made to fit any size of opening.

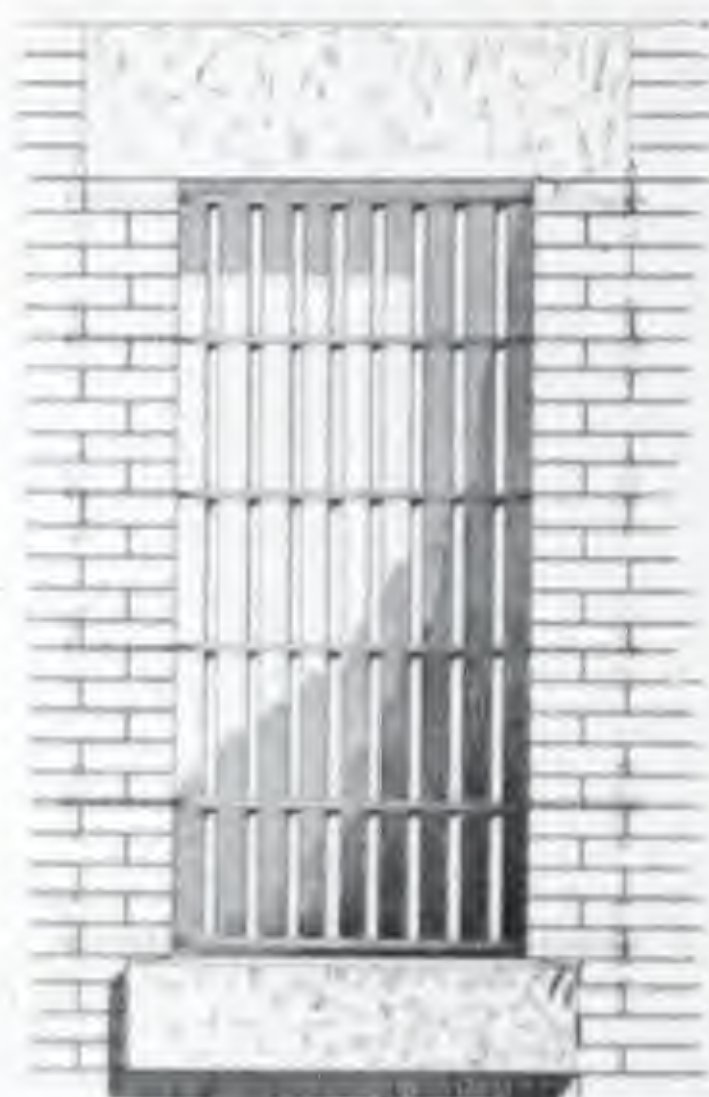
The heavy lattice steel door, No. 70, has steel bars  $1\frac{1}{2} \times \frac{3}{8}$ -inch; open space about  $4\frac{1}{2}$  inches square;  $2 \times 2 \times \frac{1}{4}$ -inch angle steel frames into which lattice is



rivetted; forged hinges, steel armor plate around lock as shown; separate angle frame all around, usually wider and heavier than frame to lattice work of door.

Nos. 71, 72 and 73 are types of heavy steel plate jail doors made to fit any size of opening. Usually made of  $\frac{3}{8}$ -inch or  $\frac{1}{2}$ -inch steel plate securely riveted to 2 x 2 x  $\frac{1}{4}$ -inch steel angle frame, extra heavy, forged hinges, separate steel angle frame all around, usually wider and heavier than frame of door.

Steel plate doors can be fitted with observation grating as shown at No. 73, so jailer can see what is going on without opening doors.



No. 74



No. 75

We can supply window guards, in the styles illustrated above, to fit openings of any size. The guard shown in No. 74 is featured by round steel vertical bars set in heavy horizontal steel bars built securely into the wall, while No. 75 has square steel vertical bars set in heavy horizontal bars securely anchored in the wall. When ordering, give width and height of each clear opening.

Prices on any style of jail or cell fittings will gladly be quoted upon application.

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## STEEL DOORS AND FIRE SHUTTERS

Steel doors and fire shutters can be made up to any size and in any style. All work is securely rivetted and well finished.

No. 76 represents a sturdy and serviceable type of steel door.

When ordering or asking for prices, give all dimensions and thickness of plates also state if locking bars are wanted.

No. 76 (At Left)—Steel Door

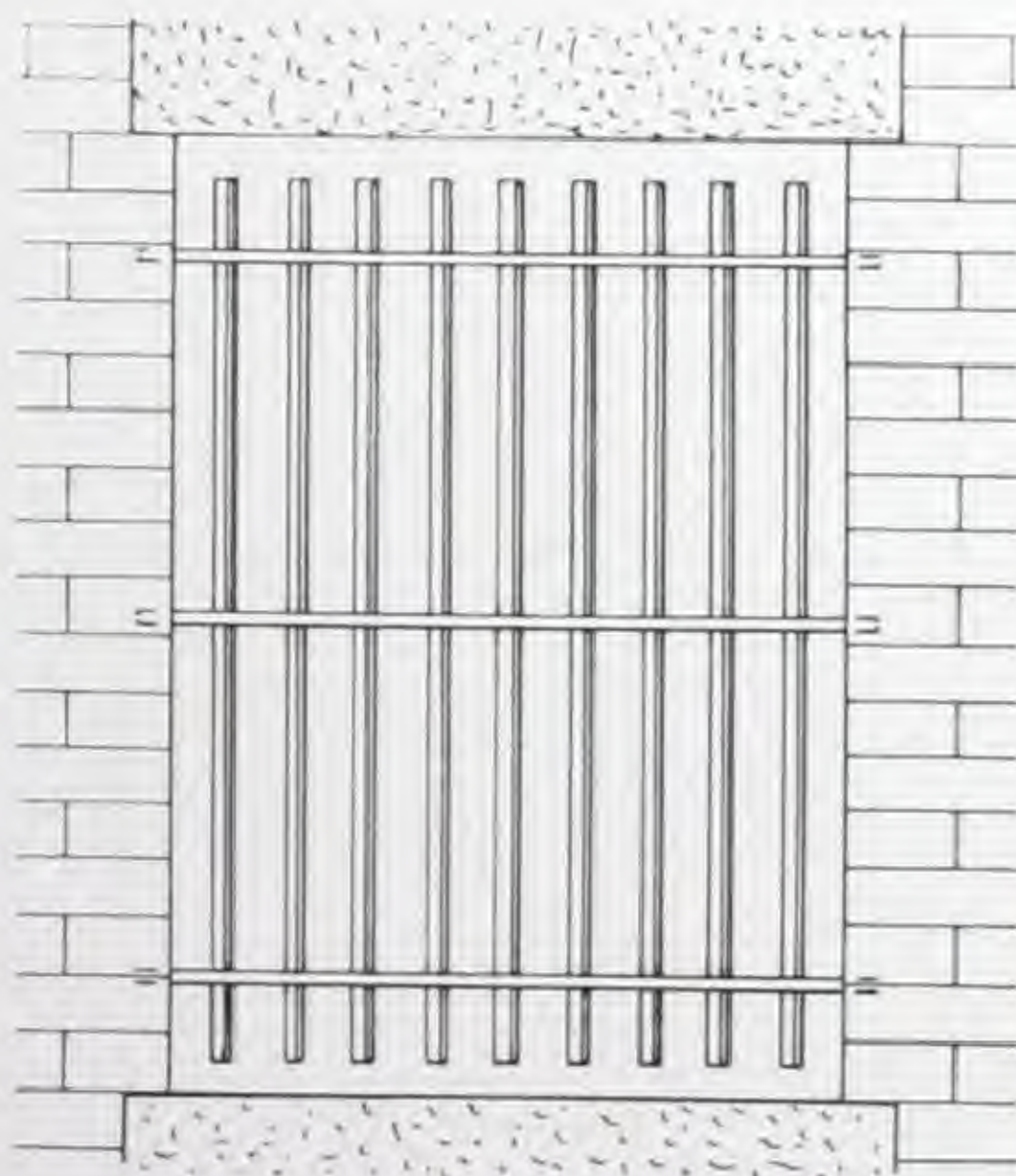
## WINDOW GUARDS

Steel window guards can be supplied to suit individual requirements.

In the illustration herewith, No. 77, a guard is shown constructed of 1-inch vertical round bars with  $2 \times \frac{1}{4}$ -inch horizontal bars.

Give width and height of opening when ordering.

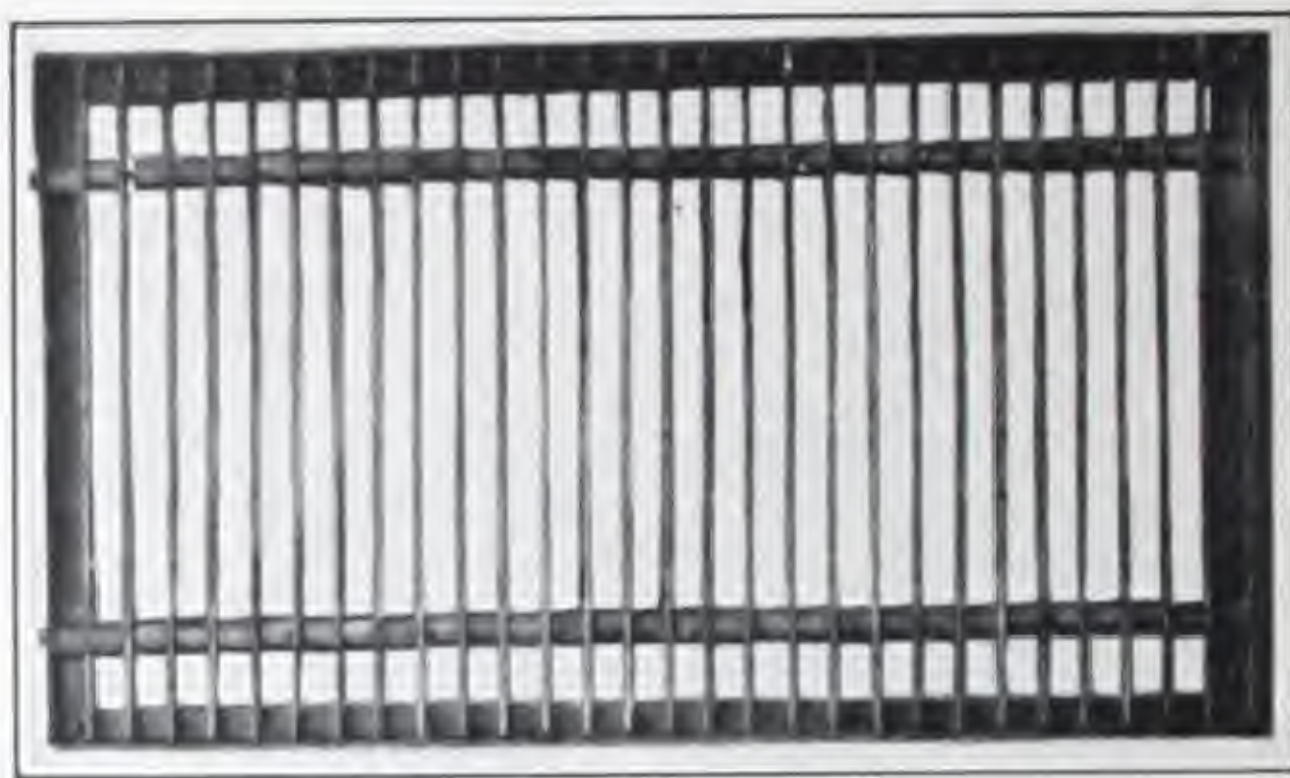
No. 77 (At Right)—  
Steel Window Guard





### AREA GRATINGS

We are able to supply any size of any style of area grating on short notice as a large assortment of flats, rounds and angles are carried in stock for this work.



No. 78—Standard Area Grating.

Our standard side-walk area grating illustrated above, is made up of steel angle frame  $1\frac{1}{2} \times 1\frac{1}{2} \times \frac{1}{16}$ -inch, riveted at corners;  $1\frac{1}{4} \times \frac{1}{4}$ -inch flat bars on edge, spaced at  $1\frac{1}{2}$ -inch centers with cast iron separators on  $\frac{3}{4}$ -inch round iron rods or bolts. Two of these rods are furnished when grating is three feet or less in width, and when over three feet wide, three or more bolts are used. Weight per square foot, out-to-out measurements, 14 lbs.

When ordering standard area grating, give length and width overall, allowing 2-inch bearing on all sides; specify whether or not angle frame is desired.



No. 79—Area Grating

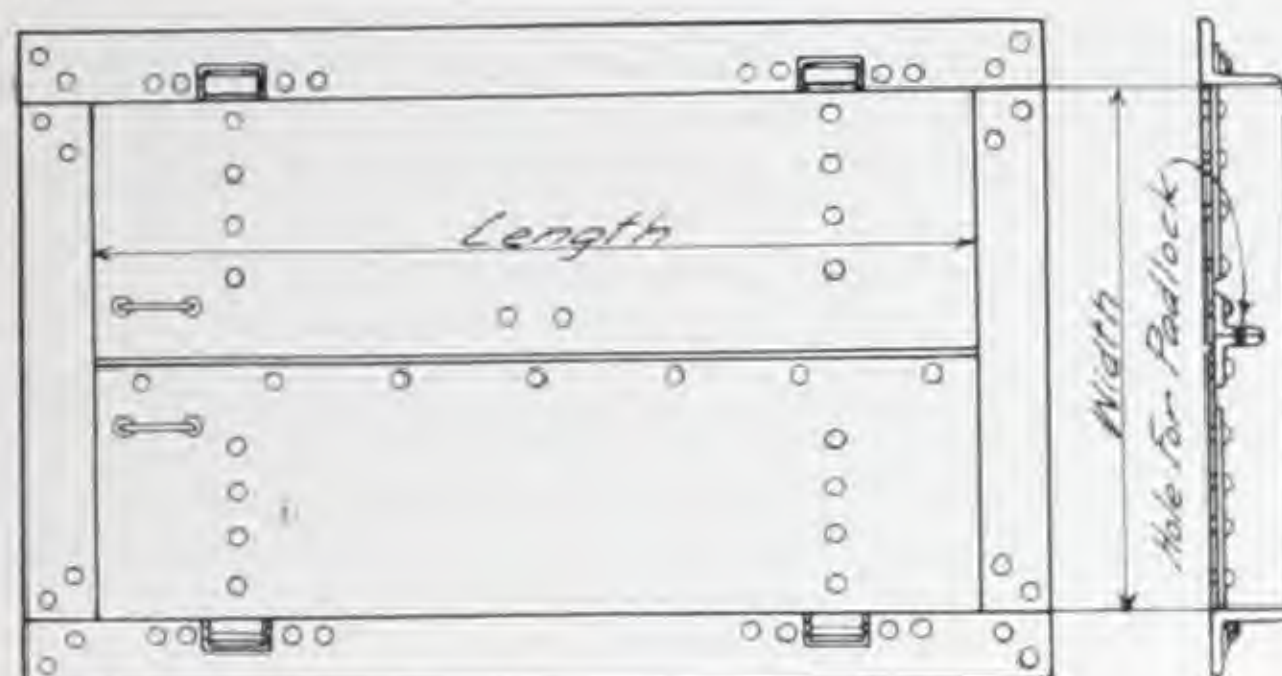
Another type of grating is illustrated by No. 79. It is made up of wrought iron slats, fastened to frame at ends; stiffening rod in center.

In writing for prices and discounts, state sizes required and style desired.



## SIDEWALK DOORS

Our standard sidewalk door is strongly made and will carry any load likely to be placed on it. It is made of solid steel plates in angle frames, with locking attachment.

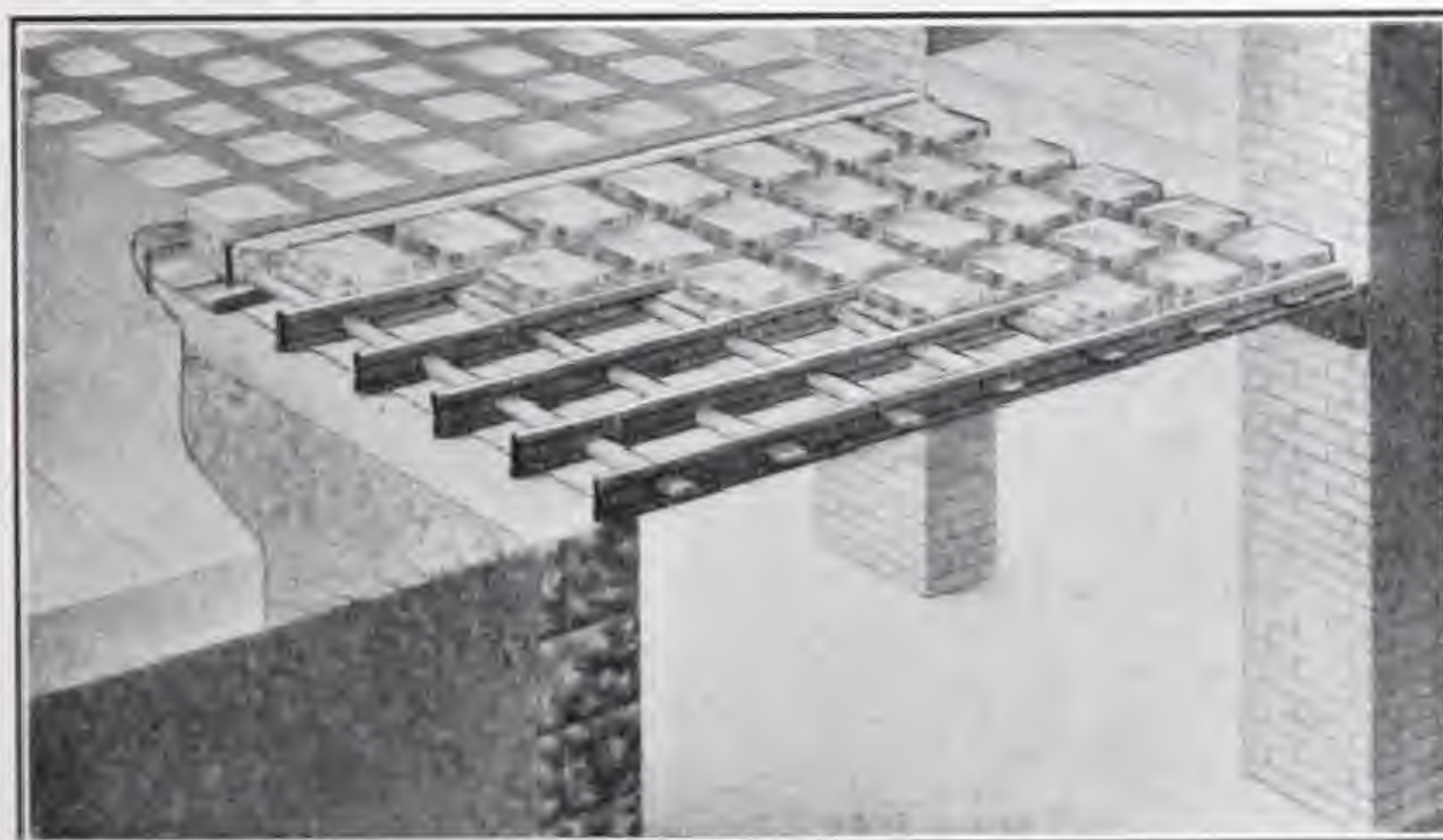


No. 80—Standard Sidewalk Door

Sizes out to out of openings should be specified in orders or requests for estimate; also whether doors are to be in one or two pieces or leaves.

## SIDEWALK LIGHTS

Space under a building and adjacent side walk may be made useful by means of sidewalk lights, as shown in the illustration below.



No. 81—Showing the Use of Sidewalk Lights

The lights are carried on wrought steel framework and imbedded in cement, watertight. A bearing of about two inches on the building side and of about the same area on the wall side should be provided; bearing should be  $2\frac{1}{4}$  inches below finish level.



## STANDARD WATER STORAGE TANKS

Our standard water storage tanks are tested to 100 pounds hydrostatic pressure and are guaranteed for a working pressure not exceeding 65 pounds per square inch.



No. 82—Standard Water Storage Tank.

Heads are dished to a radius equal to the diameter of the shell; 20-in. to 36-in. diameter tanks are welded throughout; 42-in. diameter tanks have longitudinal and girth seams rivetted, and heads welded.

Tanks can be furnished with manhole or handhole if required. Coils for hot water tanks, see page 116.

Six standard openings as shown above, are included. For larger or smaller openings or for openings located differently than shown, prices will be quoted on request.

## MANUFACTURERS' STANDARD LIST

Size		Thickness of Material			Regular Open- ings, Inches	Approximate Capacity		Approx. Weight Lbs.	List Price Black
Dia. in Inches	Length in Feet	Shell	Convex Head	Concave Head		Imp. Gals.	U.S. Gals.		
20	4	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	55	66	250	\$ 94.00
20	5	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	70	85	295	104.00
24	4	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	80	100	310	109.00
24	5	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	100	120	360	123.00
24	6	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	120	140	410	134.00
30	4	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	125	150	395	143.00
30	5	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	155	180	455	158.00
30	6	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	185	220	515	173.00
30	7	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	215	250	585	196.00
30	8	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	245	295	645	211.00
36	6	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	265	315	685	206.00
36	7	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	310	365	760	241.00
36	8	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	350	420	835	256.00
36	10	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	440	525	980	293.00
42	6	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	360	430	835	276.00
42	7	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	420	500	940	310.00
42	8	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	480	575	1025	333.00
42	10	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	600	720	1250	375.00
42	12	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	720	865	1430	415.00
42	14	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{1}{4}$	2	840	1000	1620	468.00

Larger sizes than those listed above, quoted upon application. We have a well equipped galvanizing department. Prices for galvanized tanks quoted upon application.



## EXTRA HEAVY WATER STORAGE TANKS

Our extra heavy water storage tanks are tested to 150 pounds hydrostatic pressure, and are guaranteed for a working pressure not exceeding 100 pounds per square inch.



No. 82—Extra Heavy Water Storage Tank

Heads are dished to a radius equal to the diameter of the shell; 24-in. diameter tanks are welded throughout; 30-in. and 36-in. diameter tanks have longitudinal and girth seams rivetted, and heads welded; 42 in. and 48 in. diameter tanks are rivetted throughout. Tanks can be furnished with manhole or handhole if required. Coils for hot water tanks, see page 116.

Six standard openings as shown above, are included. For larger or smaller openings or for openings located differently than shown, prices will be furnished on request.

## MANUFACTURERS' STANDARD SPECIFICATIONS

Size		Thickness of Material			Regular Openings, Inches	Approximate Capacity		Approx. Weight Lbs.	List Price, Black
Dia. in Inches	Length in Feet	Shell	Convex Head	Concave Head		Imp. Gals.	U.S. Gals.		
24	5	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	100	120	360	\$137.00
24	6	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{4}$	1 $\frac{1}{2}$	120	140	410	155.00
30	5	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{3}{8}$	2	155	180	480	182.00
30	6	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{3}{8}$	2	185	220	545	198.00
30	7	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{3}{8}$	2	215	250	615	224.00
30	8	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{3}{8}$	2	245	295	680	242.00
36	6	$\frac{3}{4}$	$\frac{3}{8}$	$\frac{3}{8}$	2	265	315	890	264.00
36	7	$\frac{3}{4}$	$\frac{3}{8}$	$\frac{3}{8}$	2	310	365	990	300.00
36	8	$\frac{3}{4}$	$\frac{3}{8}$	$\frac{3}{8}$	2	350	420	1090	328.00
36	10	$\frac{3}{4}$	$\frac{3}{8}$	$\frac{3}{8}$	2	440	525	1200	385.00
42	6	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{2}$	2	360	430	1160	345.00
42	7	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{2}$	2	420	500	1280	390.00
42	8	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{2}$	2	480	575	1430	420.00
42	10	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{2}$	2	600	720	1540	480.00
42	12	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{2}$	2	720	865	1940	540.00
42	14	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{2}$	2	840	1000	2180	514.00
48	8	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	2	625	750	1760	510.00
48	10	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	2	785	940	2030	580.00
48	12	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	2	940	1130	2340	650.00
48	14	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	2	1125	1300	2610	715.00
48	16	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	2	1250	1500	2880	800.00
48	18	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	2	1415	1700	3150	870.00

Larger sizes than those listed above, quoted upon application. We have a well equipped galvanizing department. Prices for galvanized tanks quoted upon application.



## STEAM COILS

The illustration below shows the arrangement of horizontal steam coils in standard or extra heavy water storage tanks.



No. 84—Steam Coil Arrangement

## LIST PRICES OF HORIZONTAL STEAM COILS, BUILT IN TANKS.

Size of Tank	Size of Coil	Price of Plain Coil	Price of Galvanized Coil
20" x 4'	4 Pipes 1 inch	\$29.00	\$35.00
20" x 5'	4 " 1 1/4 "	30.50	38.50
24" x 4'	4 " 1 1/4 "	35.50	42.00
24" x 5'	4 " 1 1/4 "	37.00	45.00
24" x 6'	4 " 1 1/4 "	38.50	48.00
30" x 4'	4 " 1 1/4 "	35.50	42.00
30" x 5'	4 " 1 1/4 "	37.00	45.00
30" x 6'	4 " 1 1/4 "	38.50	48.00
30" x 7'	4 " 1 1/4 "	40.00	51.00
30" x 8'	4 " 1 1/4 "	41.50	54.00
36" x 6'	4 " 1 1/2 "	51.00	62.00
36" x 7'	4 " 1 1/2 "	54.00	66.00
36" x 8'	4 " 1 1/2 "	57.50	70.00
36" x 10'	4 " 1 1/2 "	64.00	78.00
42" x 6'	4 " 1 1/2 "	51.00	62.00
42" x 7'	4 " 1 1/2 "	54.50	66.00
42" x 8'	4 " 1 1/2 "	57.50	70.00
42" x 10'	4 " 1 1/2 "	64.00	78.00
42" x 12'	4 " 1 1/2 "	70.50	85.00
42" x 14'	4 " 1 1/2 "	77.00	93.00

Prices on brass, copper and spiral coils for tanks quoted on application.

## Our Tank Catalogue

which treats in a more detailed manner, of this branch of our activities, will be gladly supplied on request. A post-card directed to our Winnipeg office will bring one of these books to you immediately.



## HYDRO PNEUMATIC PRESSURE TANKS

Our hydro pneumatic pressure tanks are tested to 125 pounds hydrostatic pressure, and are guaranteed for a working pressure not exceeding 75 pounds per square inch.



No. 85—Hydro Pneumatic Pressure Tank

Heads are dished to a radius equal to the diameter of the shell; 24-in., 30-in. and 36-in. diameter tanks are welded throughout; 42 in. and 48 in. diameter tanks are rivetted throughout. All tanks are furnished with 3 standard openings in shell for 1½-in. pipe, 2½-in. openings in shell and 2½-in. openings in concave head for water glass fittings, so that tank can be used either vertically or horizontally. Tanks can be furnished with manhole or handhole if required.

For larger or smaller openings, or for openings located differently than shown, prices will be furnished on request.

MANUFACTURERS' STANDARD LIST  
HORIZONTAL OR VERTICAL

Size		Thickness of Material			Approximate Capacity		Approx. Weight Lbs.	List Price, Black
Dia. in Inches	Length in Feet	Shell	Convex Head	Concave Head	Imp. Gals.	U. S. Gals.		
24	5	⅝	⅝	⅝	100	120	395	\$120.00
24	6	⅝	⅝	⅝	120	140	390	135.00
24	10	⅝	⅝	⅝	200	235	600	204.00
30	6	⅝	⅝	⅝	185	220	545	172.00
30	8	⅝	⅝	⅝	245	295	675	212.00
30	10	⅝	⅝	⅝	305	365	800	244.00
36	6	⅝	⅝	⅝	265	315	675	205.00
36	8	⅝	⅝	⅝	350	420	840	255.00
36	10	⅝	⅝	⅝	440	525	985	295.00
36	12	⅝	⅝	⅝	530	630	1130	330.00
36	14	⅝	⅝	⅝	615	735	1310	380.00
42	8	⅝	⅝	⅝	480	575	1340	365.00
42	10	⅝	⅝	⅝	600	720	1580	425.00
42	12	⅝	⅝	⅝	720	865	1820	480.00
42	14	⅝	⅝	⅝	840	1000	2110	545.00
48	10	⅝	⅝	⅝	785	940	1875	490.00
48	14	⅝	⅝	⅝	1095	1300	2470	620.00
48	16	⅝	⅝	⅝	1250	1500	2735	690.00
48	20	⅝	⅝	⅝	1565	1880	3280	835.00
48	24	⅝	⅝	⅝	1880	2260	3830	965.00

Sizes other than those listed above quoted upon application.



## COMPRESSED AIR TANKS



These compressed air tanks are adapted to public or private garage use.

All compressed air tanks manufactured by us, comply with the Canadian Interprovincial Regulations for the construction and installation of tanks and receptacles for compressed air and other gases.

Designs have been approved and registered by the Provinces of British Columbia, Alberta, Saskatchewan, Manitoba and Ontario.

Tanks 18-in. to 24-in. in diameter are fitted with two  $2\frac{1}{2} \times 3\frac{1}{2}$ -inch handholes in the shell. Tanks 24-in. to 36-in. in diameter have two 4 x 6-inch handholes. Tanks over 36-in. diameter are provided with a manhole 11 x 15 inches.

NOTE—In order to facilitate the delivery of tanks over 24-in. diameter, buyer should furnish a sketch showing position and sizes of inlet and outlet. If these sizes are not known, buyer should state for what purpose the tank is to be used, and the size of compressor.

No. 86 (At Left)—Compressed Air Tank

Size		Thickness of Material		Cubic Feet Capacity	Approximate Capacity		Approx. Weight Lbs.	List Price
Dia. in Inches	Length in Feet	Shell	Heads		Imp. Gals.	U.S. Gals.		
12	3	$\frac{3}{16}$	$\frac{3}{16}$	21½	15	18	105	\$ 37.00
14	4	$\frac{3}{16}$	$\frac{3}{16}$	4½	30	36	154	41.00
14	5	$\frac{3}{16}$	$\frac{3}{16}$	5	35	42	185	46.00
16	5	$\frac{1}{4}$	$\frac{1}{4}$	7	45	54	286	58.00
18	5	$\frac{1}{4}$	$\frac{1}{4}$	9¼	55	66	334	69.00
20	5	$\frac{1}{4}$	$\frac{3}{16}$	11	70	84	395	75.09
20	6	$\frac{1}{4}$	$\frac{3}{16}$	13½	85	102	450	85.00
24	5	$\frac{1}{4}$	$\frac{3}{16}$	16	100	120	490	87.00
24	6	$\frac{1}{4}$	$\frac{3}{16}$	19	120	144	560	100.00
30	5	$\frac{1}{4}$	$\frac{3}{16}$	24	150	180	800	137.00
30	6	$\frac{1}{4}$	$\frac{3}{16}$	29	180	216	905	156.00
30	8	$\frac{1}{4}$	$\frac{3}{16}$	39	245	294	1115	194.00
36	6	$\frac{3}{8}$	$\frac{1}{2}$	42	265	318	1320	181.00
36	8	$\frac{3}{8}$	$\frac{1}{2}$	56	350	420	1620	231.00
42	8	Special		77	480	576	.....	Prices on Application
42	10			96	600	720	.....	
42	12			116	720	864	.....	
48	10			125	785	942	.....	
48	12			150	935	1122	.....	
48	14			176	1095	1314	.....	
60	12			235	1470	1764	.....	
60	14			275	1700	2040	.....	
60	16			315	1950	2340	.....	



### TRUCK TANKS

Steel tanks for gasoline and oil delivery trucks, supplied in capacities up to one thousand Imperial gallons, in as many compartments as desired.

Tanks have baffle plates to prevent surging. Can room at back and also racks



No. 87—Types of Truck Tanks

at side if specified. Tanks for Ford trucks can be supplied with two compartments and can room, with capacity 250 Imperial gallons. These tanks can be made either rivetted or welded, and are tested and guaranteed gasoline tight.



## WAGON OR TRUCK TANKS

The tank shown in illustration No. 88 is designed for use on an ordinary truck or wagon, where deliveries by means of tank are made only intermittently. When it is desired to use the truck or wagon for other purposes the tank can be easily removed.



No. 88—Portable Wagon or Truck Tank.

This tank is mounted on two wood bolsters with two pairs of small wheels and axles. The wheels have eccentric centres, and to remove tanks from truck or wagon, the eccentrics are turned by means of hand levers into a position which raises the tank on to the wheels so that it can easily be rolled into warehouse.

By reversing the operation, the tank sits rigidly on the floor of the warehouse.

## TRUCK BODIES

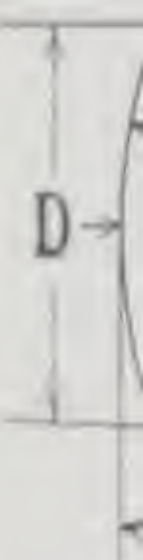


No. 89—Typical Steel Truck Body.

We furnish steel bodies for trucks in sizes and capacities as desired. The illustration above shows a typical truck body constructed to customer's design. Prices furnished upon request.

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Size

Quantity

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90"  
100"  
120"  
140"  
160"  
180"  
200"

78"  
84"  
90"  
96"

1-1/2" Long

One mil  
shells re  
separate



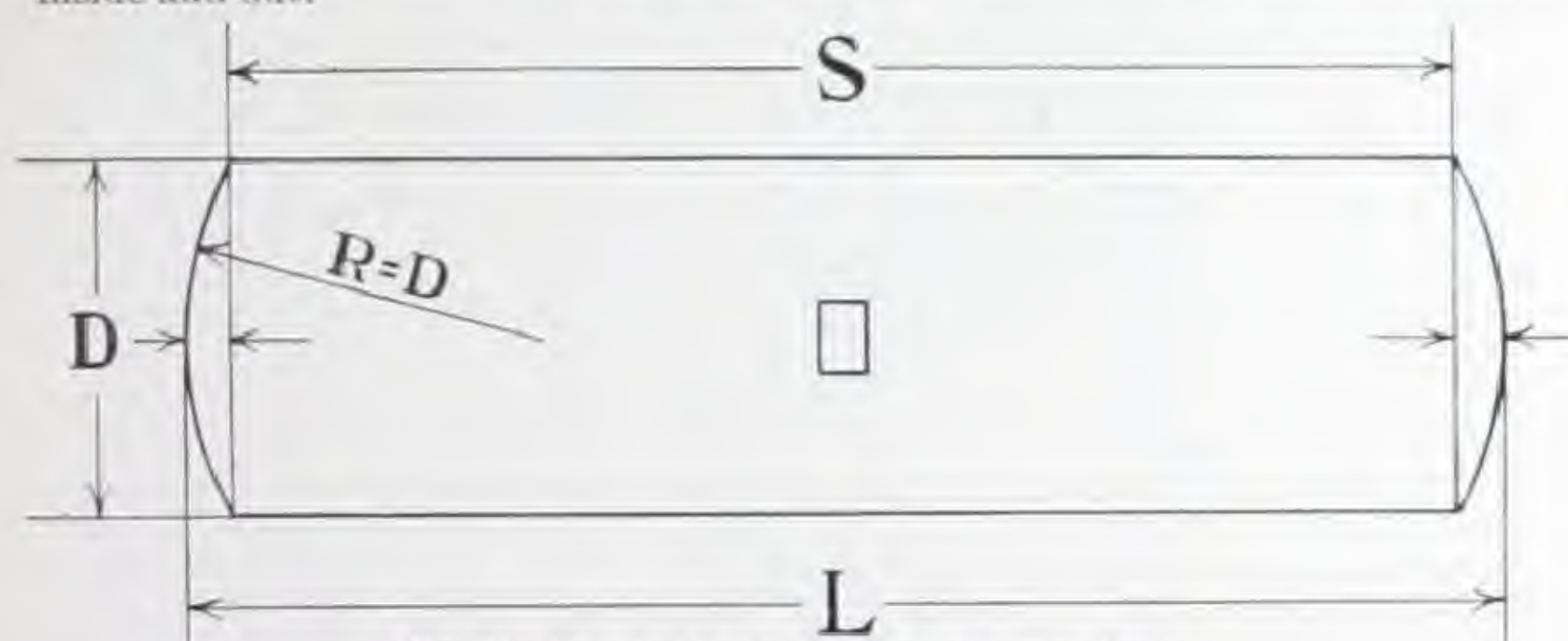
## SPRINKLER SYSTEM STORAGE TANKS

Our tanks for sprinkler system storage are built to Western Canada Fire Underwriters specifications, and are inspected during construction by the Western Canada Fire Underwriters.



No. 90—Sprinkler System Storage Tank

The table below gives specifications for standard pressure tanks for sprinkler systems. All capacities for Underwriters' specifications are U.S. gallons. All diameters are inside shell. Flange quality stamped steel is the material used. Girth seams single rivetted; longitudinal seams triple-rivetted with butt-straps inside and out.



No. 91—Detail of Sprinkler System Storage Tank

### SPECIFICATIONS FOR STANDARD SPRINKLER SYSTEM PRESSURE TANKS

Diameter D	Dish of Heads	S	L	No. of Sheets	S	L	No. of Sheets
4500 Gallons				6000 Gallons			
60"	8"	30'	31' 4"	4			
66"	8 3/4"	24' 7"	26' 1 1/2"	3			
72"	9 1/2"	20' 7"	22' 2"	3	27' 8"	29' 3"	4
78"	10 1/2"	17' 4"	19' 1 1/2"	3	23' 4"	25' 1 1/2"	3
84"	11"	14' 9"	16' 7"	2	19' 11"	21' 9"	3
90"	12"	12' 8"	14' 8"	2	17' 2"	19' 2"	3
96"	13"	10' 11"	13' 1"	2	14' 10"	17' 0"	2
7500 Gallons				9000 Gallons			
78"	10 1/2"	29' 4 1/2"	31' 1"	4	35' 5"	37' 1"	5
84"	11"	25' 1 1/2"	26' 11 1/2"	4	30' 4"	32' 2"	4
90"	12"	21' 8 1/2"	23' 8 1/2"	3	26' 3"	28' 3"	4
96"	13"	18' 10"	21' 10"	3	22' 10"	25' 0"	3

L = Length Overall    S = Length of Shell    Radius of Dish of Head = Diameter of Tank

One saddle is required under each sheet of shell, consisting of cast iron formed saddles resting on compound steel beam, varying in size according to spans. Separate price will be given on these on information as to spans required.



## STEEL TANKS AND TOWERS

We can furnish water supply tanks and towers of any height or capacity for municipalities, railways or corporations; also steel towers for supporting wooden tanks, though we do not manufacture wooden tanks.



No. 92—A steel tank and tower designed and erected by the Manitoba Bridge and Iron Works, Limited.

We will design tanks and towers and give estimates of cost without charge to prospective buyers. When writing send all particulars covering height of tower and capacity of tank.

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required.



## MUNICIPAL WATER TOWERS AND STAND-PIPES

We undertake to design, construct and erect complete elevated tanks or stand-pipes for municipal, domestic or railway water supply service.



No. 92—Elevated Water Tank at Tysonville, Minn.; Capacity 115,000 Gallons, with Suggested Drinking Water Tank.

Specifications submitted on receipt of statement of storage capacity and head required. Drawings and estimates of cost will be furnished to prospective buyers.





No. 94—Vertical Storage Tank with Rivetted Seams

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being the re  
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customers  
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body plates,

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## STEEL STORAGE TANKS

Our steel storage tanks embody the latest developments in this class of work, being the result of twenty-five years experience in the steel and iron industry. As the largest producers of tanks in Western Canada, we are prepared to fill our customers' requirements, whether for standard or special designs. Our service is prompt and efficient.

We produce steel storage tanks, either horizontal or vertical, and with seams either welded or rivetted. All welding is done electrically, and all rivets in tanks are power-driven.



No. 95—Horizontal Storage Tanks with Electrically Welded Seams

The illustration on the opposite page shows a vertical storage tank with rivetted seams.

Above are shown horizontal storage tanks with electrically welded seams. This type of tank can be furnished with division plates to make two or more compartments.

All our storage tanks are made with one-piece bottoms or ends, and with large body plates, thus reducing the number of joints to a minimum.

We can supply steel storage tanks in all sizes and to suit the customer's individual requirements.



## STEEL SMOKE-STACKS

We make steel smoke-stacks to order in any diameter and height. Most stacks are guyed, but we can supply designs and estimates on self-supporting steel stacks.

When writing for designs and estimates, send sketch showing all dimensions, and state thickness of plate required.

We also design, fabricate and erect boiler breechings.

No. 56—Two-hundred-foot steel stack, diameter seven feet, erected by Manitoba Bridge and Iron Works, Limited.

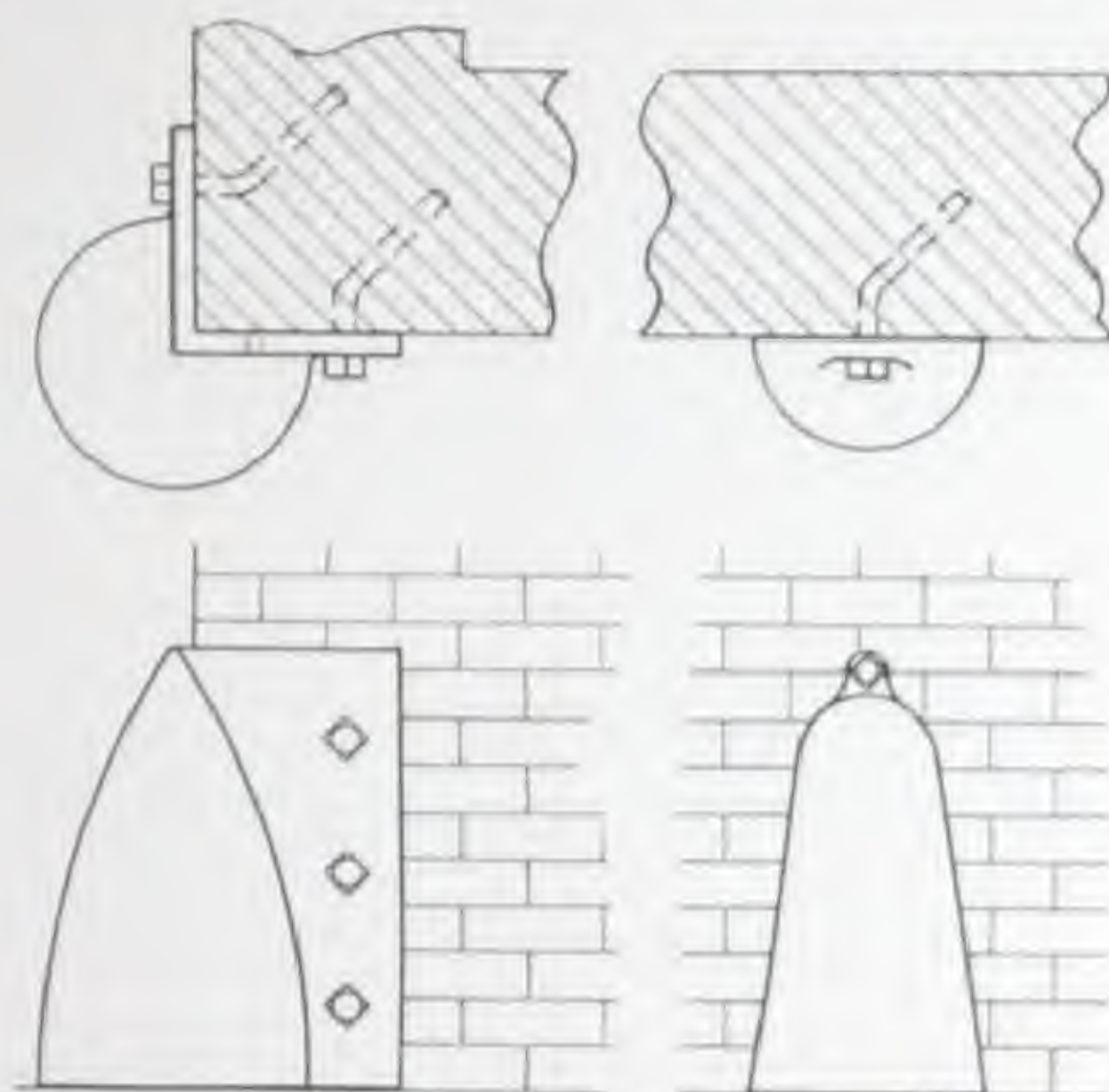




## WHEEL GUARDS

Wheel guards are used to protect corners and flat surfaces of walls at entrances to driveways and to warehouses and other buildings where trucks are driven in.

These guards are heavily constructed and securely anchored in the wall which they are designed to protect. Their cost is soon saved in damage prevented.



No. 97—Wheel Guards, for Corner and for Side of Wall

We have in stock patterns for all sizes and weights of wheel guards, and consequently are able to supply guards to suit any requirement on short notice.

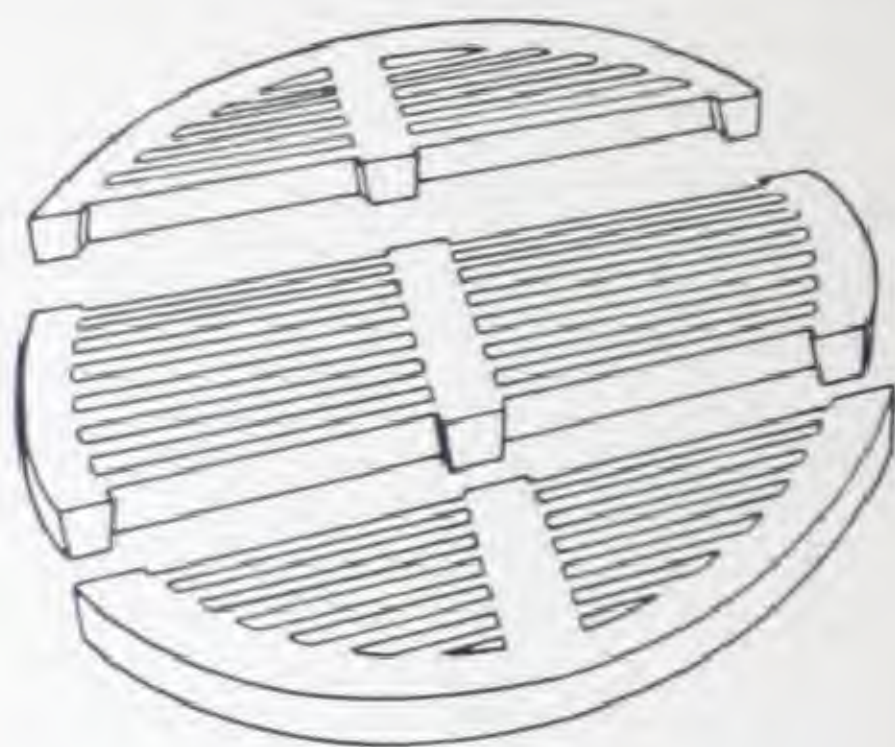
We can also supply steel angle jamb guards with anchor, and either cast iron or plate steps, curbs and thresholds for door openings in warehouses, etc.

Any size or style, whether of steel or cast iron, can be furnished. In writing for prices, give all necessary information.



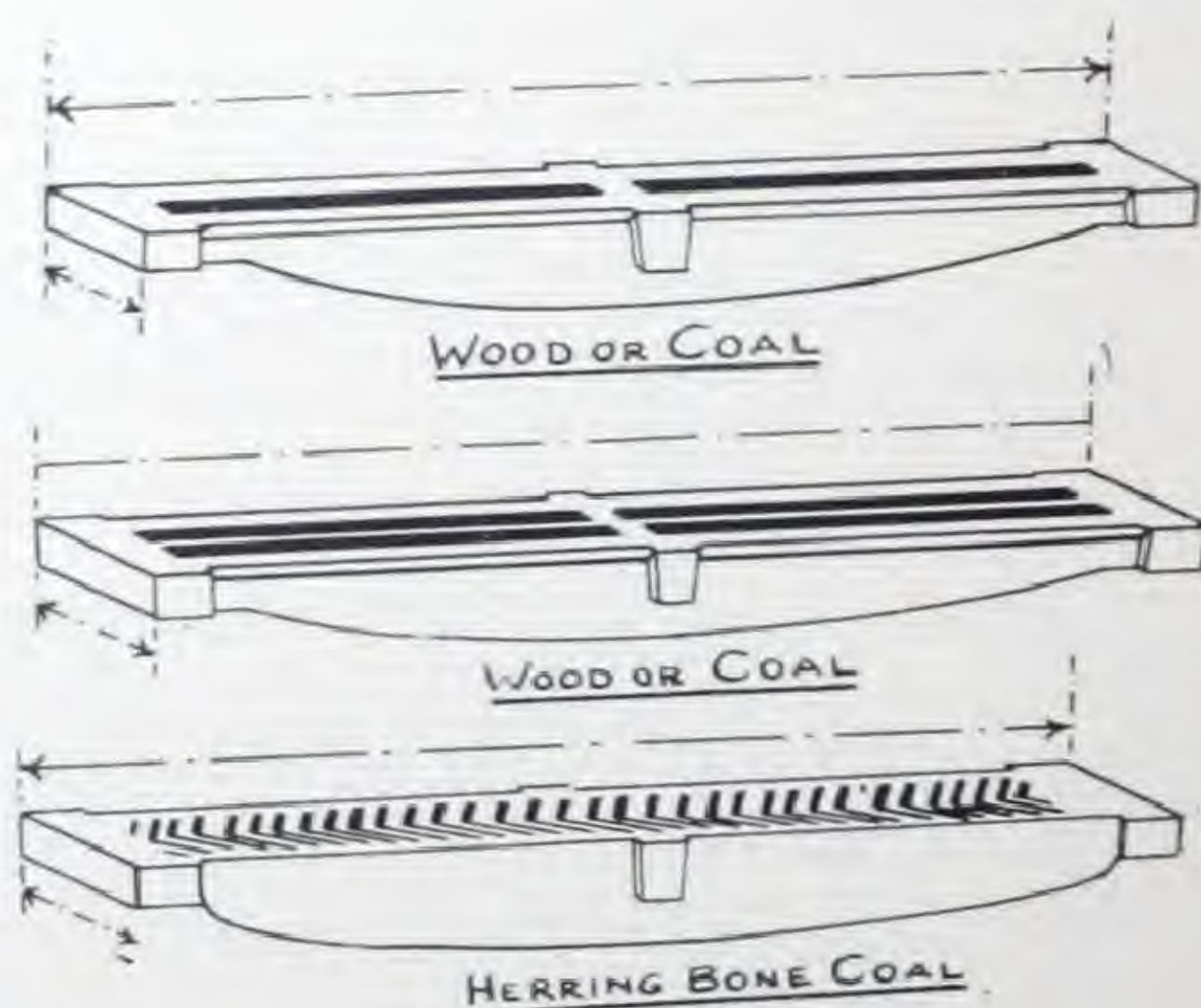
## FURNACE GRATES

Many styles of furnace grates are now in use. Several varieties are illustrated on this and the following page. The number of patterns for furnace grates which we have on hand enables us to offer a considerable selection of castings.



No. 98—Circular Grate

The illustration above depicts a circular style grate in three sections. This grate can be furnished in sizes to suit the customer's requirements.

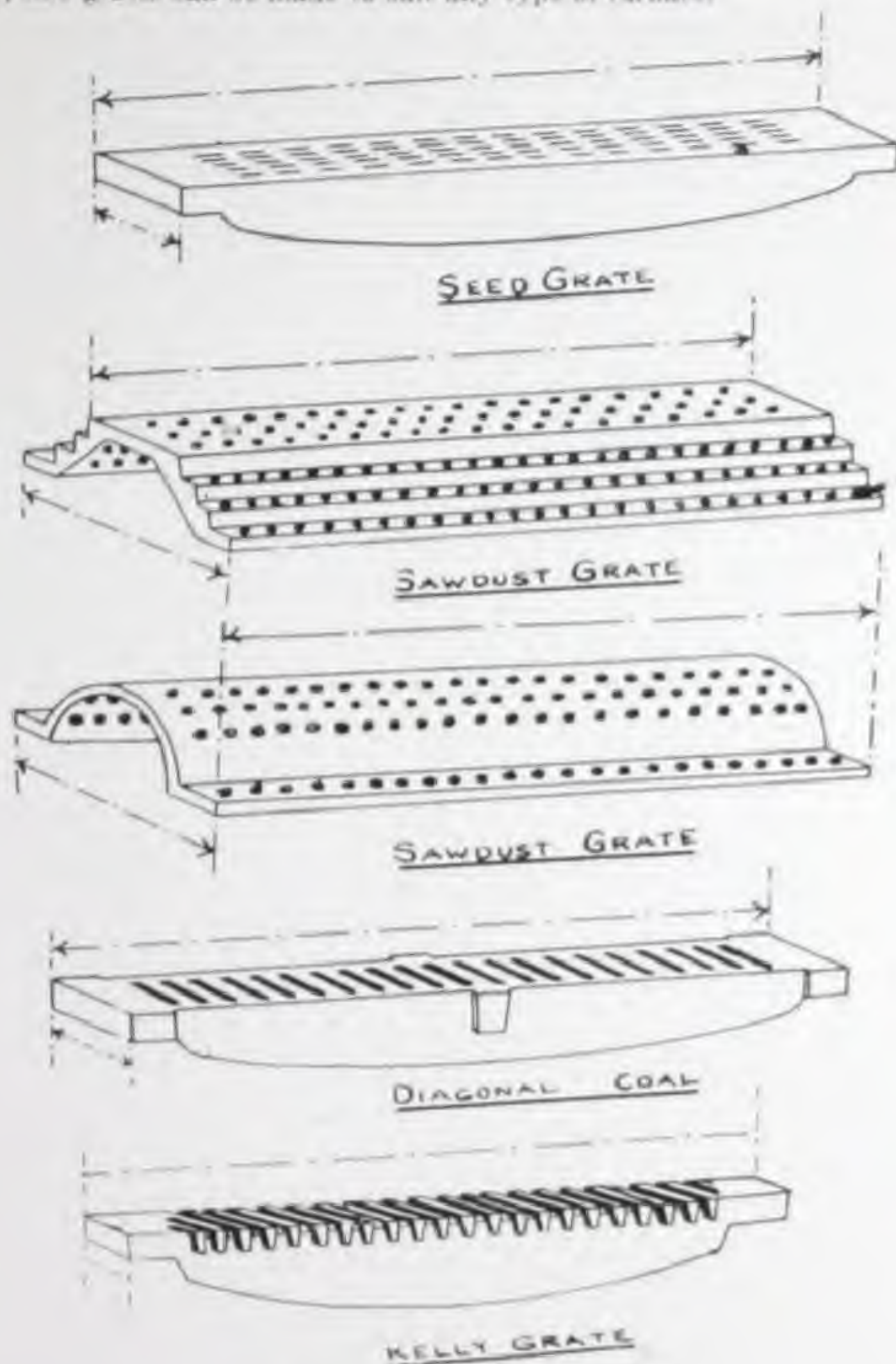


No. 99—Types of Furnace Grates

In addition to the circular grate, many styles of rectangular sectional grates are used.



A number of additional varieties of furnace grates are shown in the designs below, and grates can be made to suit any type of furnace.

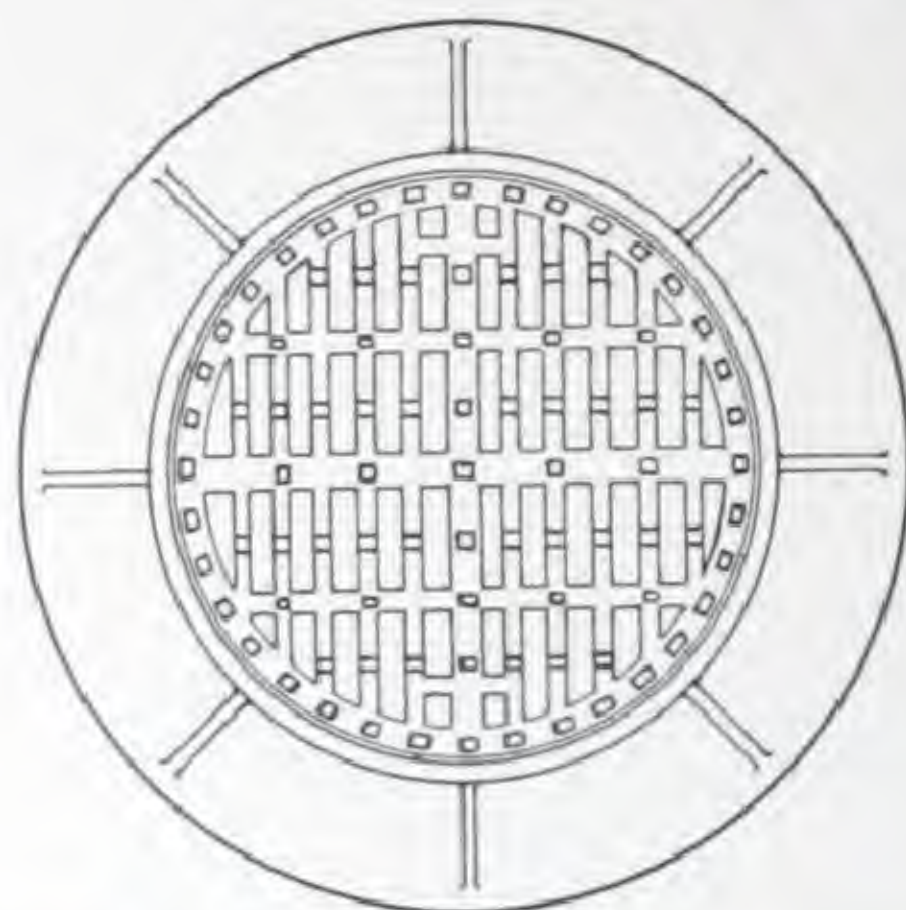


No. 100—Types of Furnace Grates

Write for prices, stating dimensions and style wanted. Estimates will be made on request.



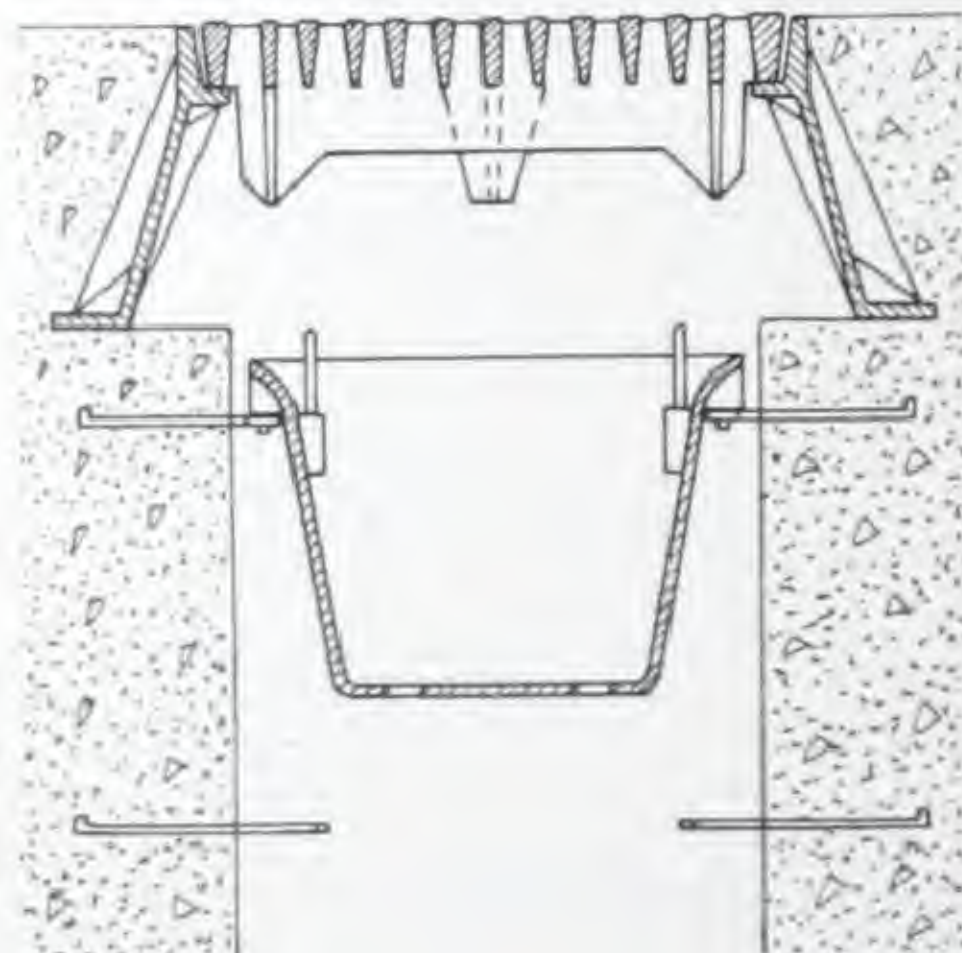
## SEWER CASTINGS

MUNICIPAL STANDARD  
MANHOLE FRAME  
AND COVER

The municipal standard manhole frame as illustrated at the left is especially adapted for city and town use.

This type of manhole frame can be supplied with solid cover as well as with grate cover shown in No. 101.

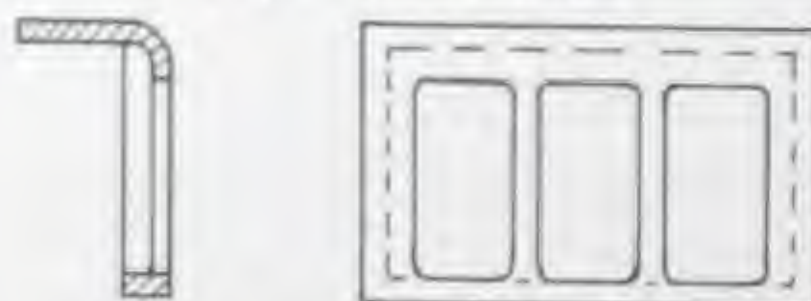
Our range of patterns enables us to offer numerous other types of manhole frames, while we can supply standards to suit the customer's individual requirements. Further information will be furnished on request.

MANHOLE MUD  
BASKETS

The mud basket shown fitted into the manhole in No. 101 can be supplied complete with brackets.

No. 101 (At Left)—Municipal Standard Sewer Manhole Frame Fitted with Grate Cover and Mud Basket.

## CURB GRATINGS



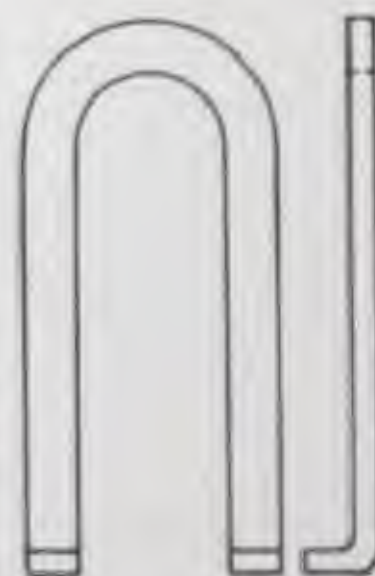
No. 102—Standard Cast Iron Curb Grating

The standard cast iron curb grating, illustrated above in No. 102, can be furnished to suit any depth of curb.

Estimates and further information furnished on request.

MANHOLE OR  
CATCH-BASIN  
STEPS

The wrought iron steps illustrated at the right are for use in manholes or catch-basins. They are shown in No. 101 above, as used in a manhole. Prices furnished on request.

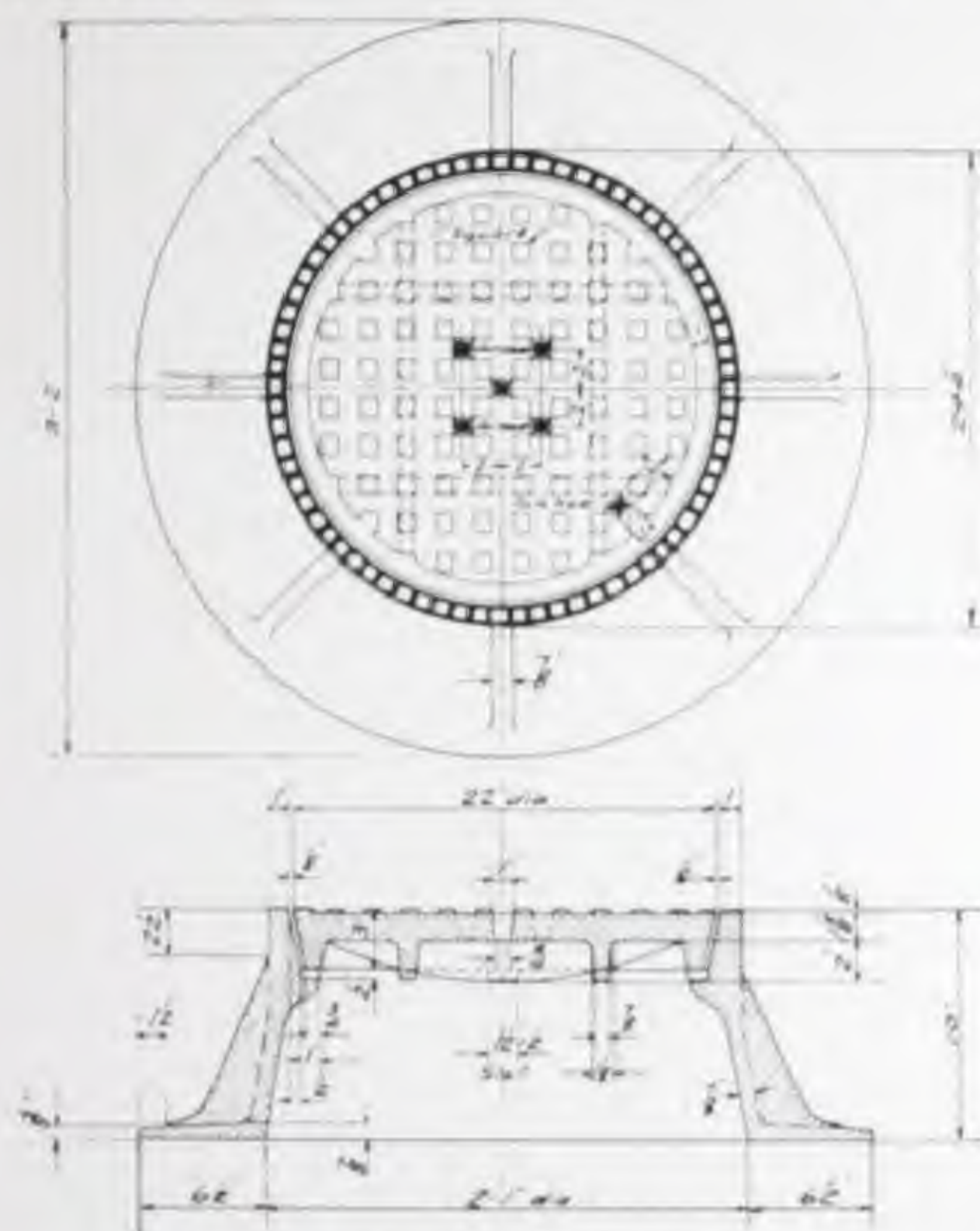


No. 103—Wrought Iron Manhole or Catch-Basin Steps.



## MANHOLE COVERS AND FRAMES

Our patterns for manhole covers and frames include those used by most of the cities of Western Canada, by the Manitoba Telephone System, Winnipeg Hydro Electric System, etc.

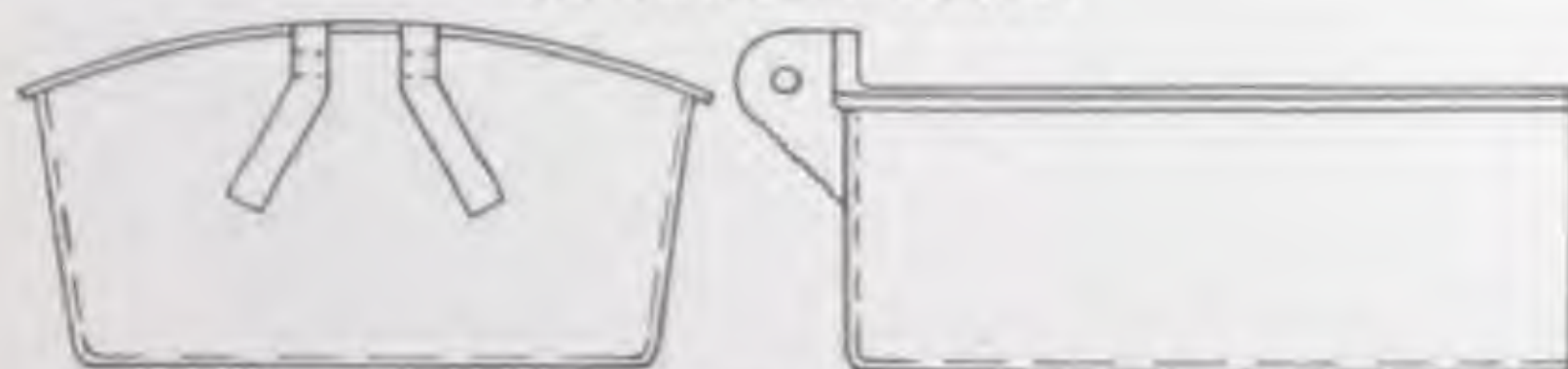


No. 104—Cast Iron Manhole Cover and Frame

Special air-tight covers with machined groove and oil seal can be supplied on order.

We make all kinds and sizes of manhole covers and frames. Estimates gladly given upon receipt of specifications.

## CATCH-BASIN HOODS



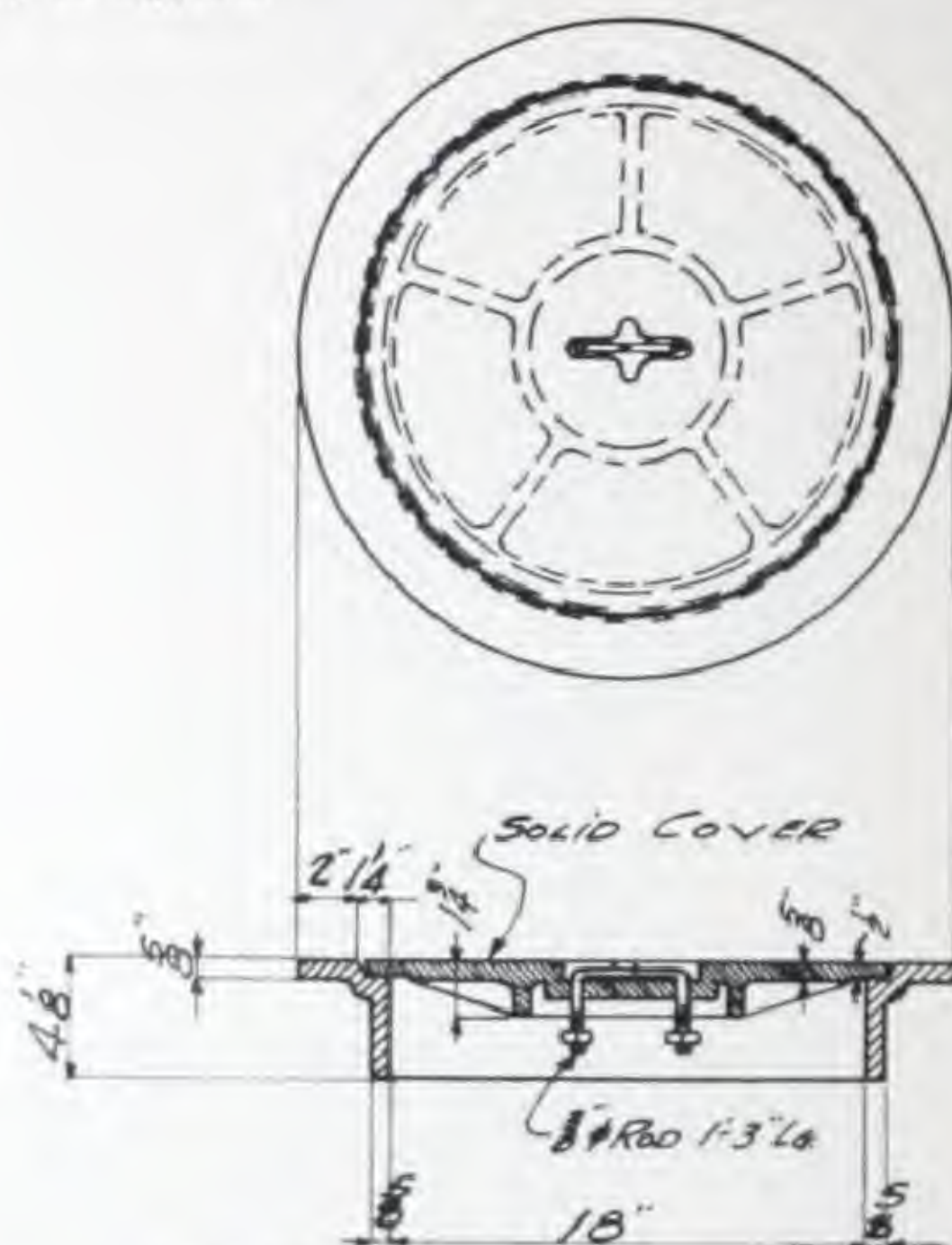
No. 105—End and Side Views of Standard Catch-Basin Hood

The standard catch-basin hood, shown in No. 105 above, is supplied complete with hinge and pin. Estimate will be furnished if requested.



## CATCH-BASIN COVERS AND FRAMES

Covers and frames for catch-basins from 10-inch to 36-inch diameter and in heavy or light pattern, either solid or perforated, according to purpose intended, can readily be supplied.



No. 106—Cast Iron Catch-Basin Cover and Frame

Where heavy trucking may take place over a catch-basin, steel plate covers may be supplied to fit cast iron frames; these covers are lighter and stronger than the cast iron variety, and will not crack under load.

**Coal-Hole Rings and Covers**—The larger sizes of catch-basin covers, with the addition of an inside locking device, are used as coal-hole covers.

## CLEAN-OUT DOORS

Cast-iron clean-out doors for general use can be supplied by us in the styles



No. 107—Circular Head Clean-out Door



No. 108—Rectangular Head Clean-out Door, Hinged

illustrated herewith, hinged or unhinged, with circular or rectangular head. Any size is obtainable. When writing for prices, state size of opening.

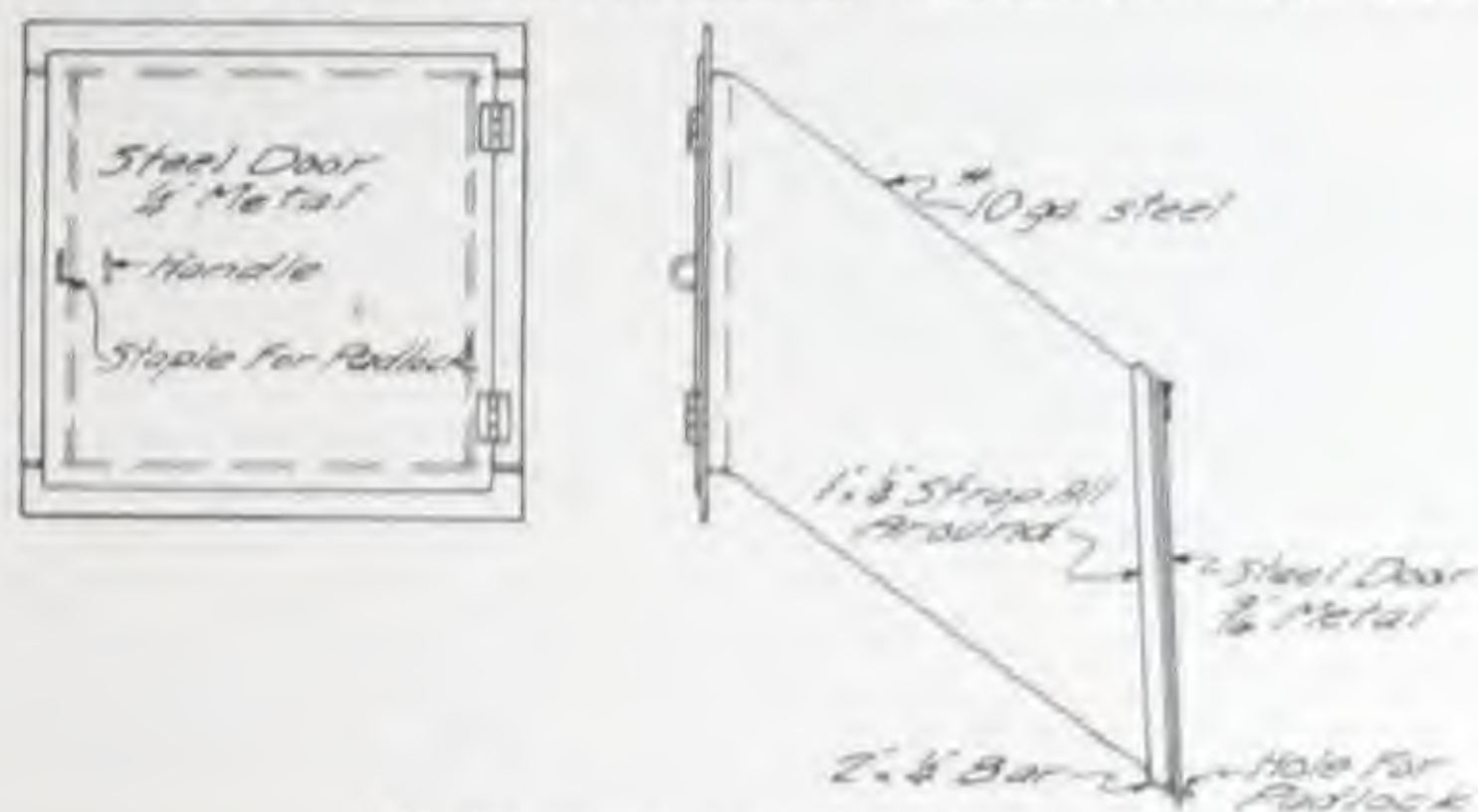


## FUEL CHUTES

The selection of fuel chutes offered to our customers includes square and round, flush and projecting types; the chutes may also be for wall or sidewalk use.

## SQUARE FLUSH TYPE

**Our Standard All Steel Design**—This pattern of fuel chute is featured by steel doors with locking devices at both inside and outside terminations of the chute. Highly durable and economical. Standard sizes shown below.



No. 109—Standard Square Fuel Chute

No.	Opening, In.	Depth Chute, In.	Weight, Lbs.
1	24 x 24	13	
2	24 x 24	17	
3	24 x 24	21	
4	24 x 24	27	
5	24 x 24	18	



**Majestic Design**—The "Majestic" is a well-known pattern of the square flush type of chute. It is well-made, giving great convenience with a maximum of service, even under heavy use. It can be supplied with cast iron or glass door. The latter style is shown by No. 110. The standard sizes for this chute are tabulated below.

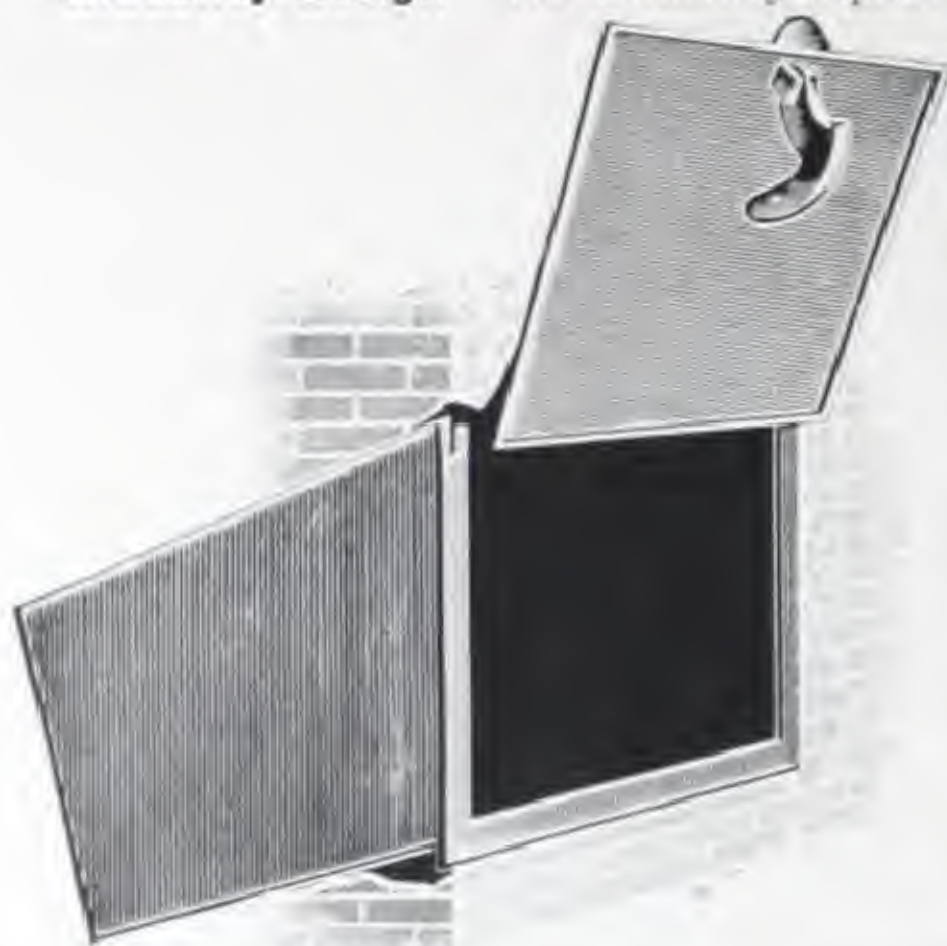
No. 110 (At Left)—Majestic Chute

No.	Opening, In.	Depth Chute, In.	Weight, Lbs.
10A—Glass Door	19 x 22	12	
10B—Iron Door	19 x 22	12	

Both our Standard and Majestic Designs are also made in Special Sizes.



**Gibboney Design**—The Gibboney Square Self-Locking Chute as seen in No. 111 is deservedly popular. It has a flanged door which fits over the rim of frame making it both wind and water proof.



The cast frame and door, combined with a sturdy steel body make the Gibboney a strong, reliable chute which will stand while the building lasts.

Ideal for receiving coal, wood or vegetables, and suitable for any style of building.

The door closes flush with the building and can be opened only from the inside.

No. 111 (At Left)—Gibboney Square Fuel Chute

#### MADE IN THE FOLLOWING SIZES:

No.	Opening, In.	Depth Chute, In.	Weight, Lbs.
4	18 x 18	24	70
5	18 x 24	30	105

Also made in sizes to suit individual requirements.

#### ROUND PROJECTING TYPE

**Gibboney Design**—The Round Gibboney Chute has practically the same features as the square type. It is self-locking and can be opened only from the inside. The frame and door are cast, while the body is of heavy steel.

The door is made with a flange which fits over rim of frame, making it wind and water proof.

The chute is neat in appearance and can be used in residences, business blocks, churches and other public buildings.



No. 112 (At Right)—Gibboney Round Fuel Chute

#### MADE IN THE FOLLOWING SIZES:

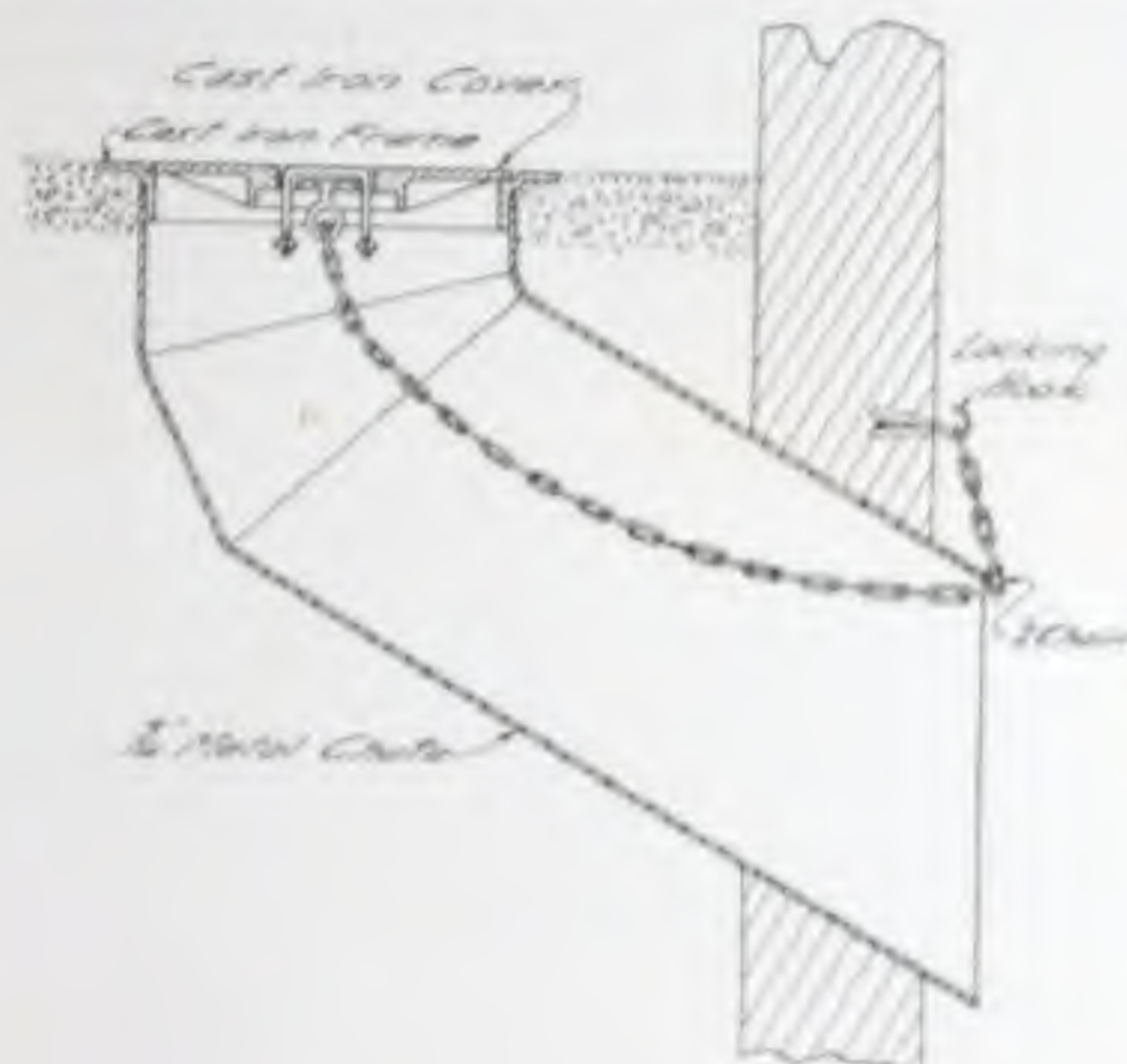
No.	Opening, In.	Depth Chute, In.	Weight, Lbs.
1	18 (diam.)	24	85
2	18 (diam.)	30	90
3	24 (diam.)	30	155

Also made in sizes to suit individual requirements.



## ROUND SIDEWALK TYPE

**Our Standard Design**—This pattern of chute which passes through both sidewalk and wall is a popular style in cases where its use is suitable.



No. 113—Standard Sidewalk Chute

The heavy round cast cover fits into a frame built into the sidewalk. The chute passes down and through the adjoining wall into the interior of the building. The cover is fastened on the inside by a simple but effective locking device as shown in No. 113 above.

This chute is made in sizes to suit the specifications of the individual customer. Estimates gladly furnished.

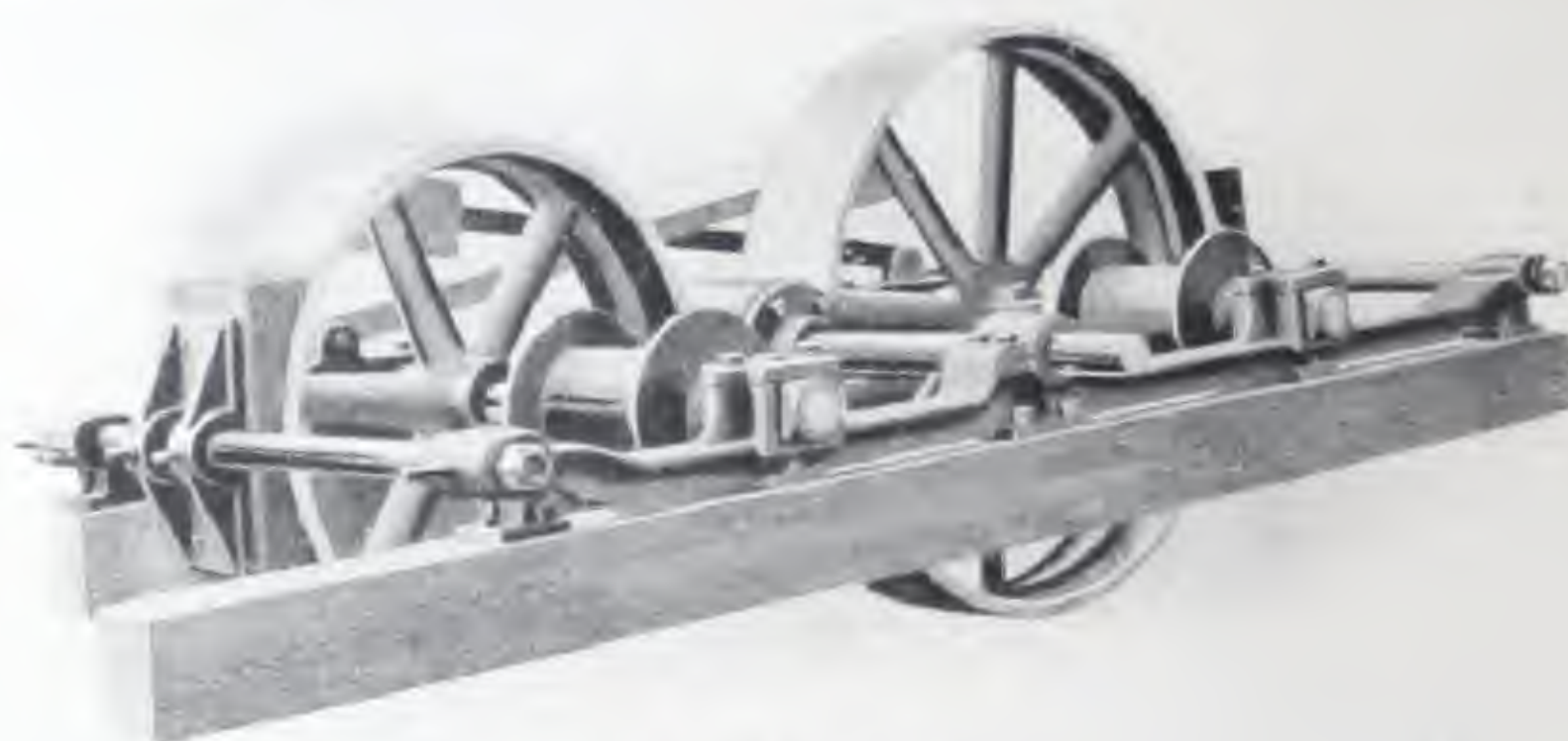


## PACKING HOUSE EQUIPMENT

We manufacture a varied range of equipment for use in abattoirs, cold storage plants, etc. In the design and construction of our products of this nature, every attention is given to assuring economical production in the packing industry. The following pages show some of the lines in which we specialize, but by no means indicate the limit of our ability; we can supply any requirement of this nature.

### BEEF HOISTS

We can supply both single and double beef hoists to suit the requirements of any meat packer. The hoist shown on this page is a double hoist, equipped with heavy-rimmed friction wheels, accurately machined and balanced. The paper friction is constructed with a cast iron sleeve and held firmly by bolts through the paper and flanges.



No. 114—Beef Hoist

The frames are of a heavy flanged ribbed construction and are made from high-grade cast iron, same as is used for machine castings. They are machined on the bottom of the frame and the bearings are babbitted with high grade babbit in perfect alignment with the lower surface so that in erecting these frames on overhead timber or steel beams it is not necessary to use liners under frames to line them with other shafts.

The weight levers are forged from high-grade steel. The sliding boxes on the friction wheel shaft are designed so that there will always be a square contact on the paper friction by the friction wheels.

The brakes are adjustable so that the brake block can be set squarely and in perfect alignment on the face of the friction wheel. The tie rods are made of heavy steel. The line shaft carrying paper friction is not furnished unless specified in order.

In ordering, state whether single or double hoist is desired.

No.  
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## TRACK HANGERS



No. 115



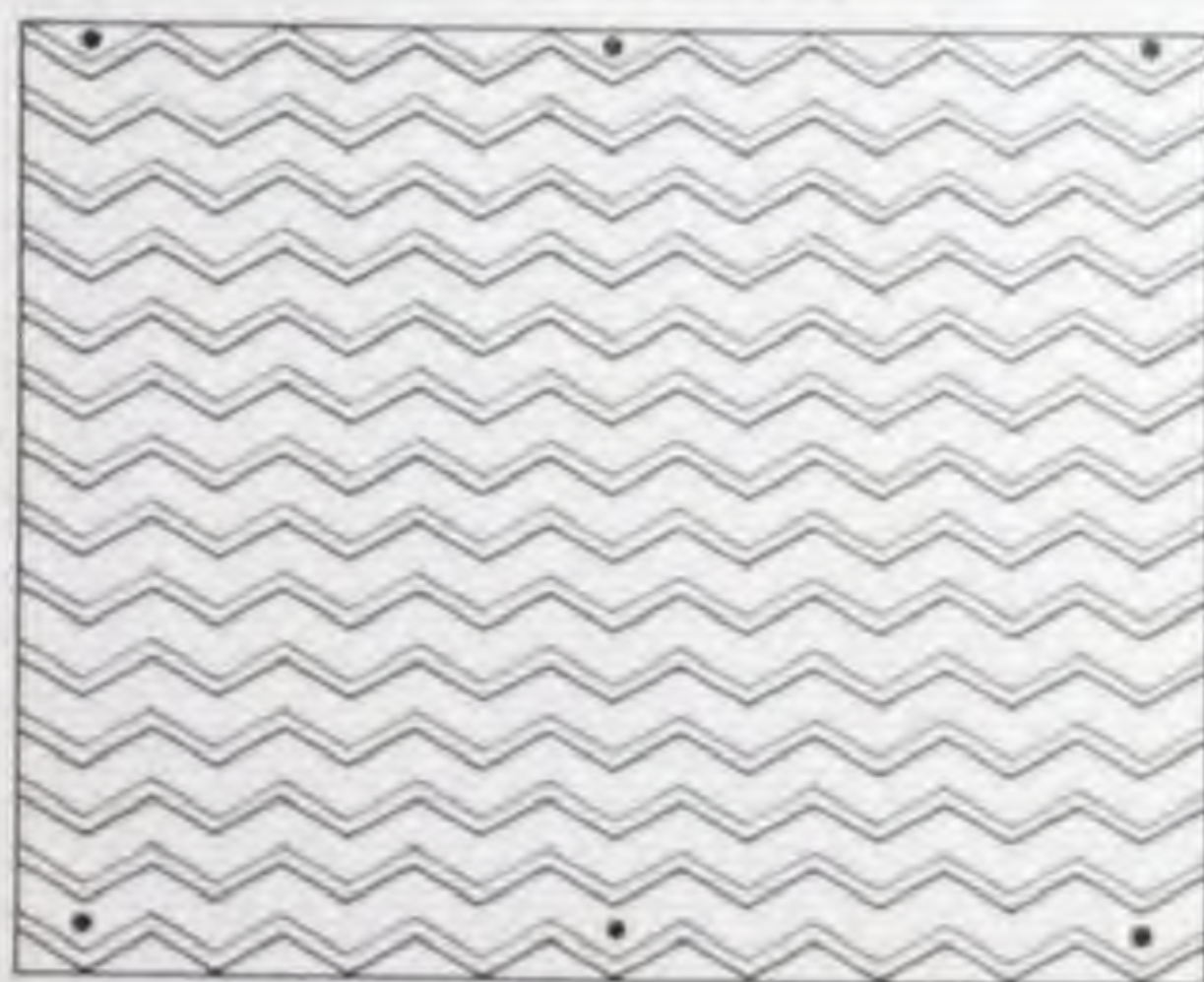
No. 116



No. 117

The illustration above shows three standard types of hangers to support overhead tracking. They are the strongest hangers for their weight obtainable, and in them are incorporated all the latest improvements. No. 115 is a cast iron track hanger; No. 116 is a soft steel track hanger; No. 117 is a cast iron hooking rail hanger. In ordering, specify length of drop, width of track, and style desired. We also roll all different types of steel track.

## PRITCH PLATES



No. 113

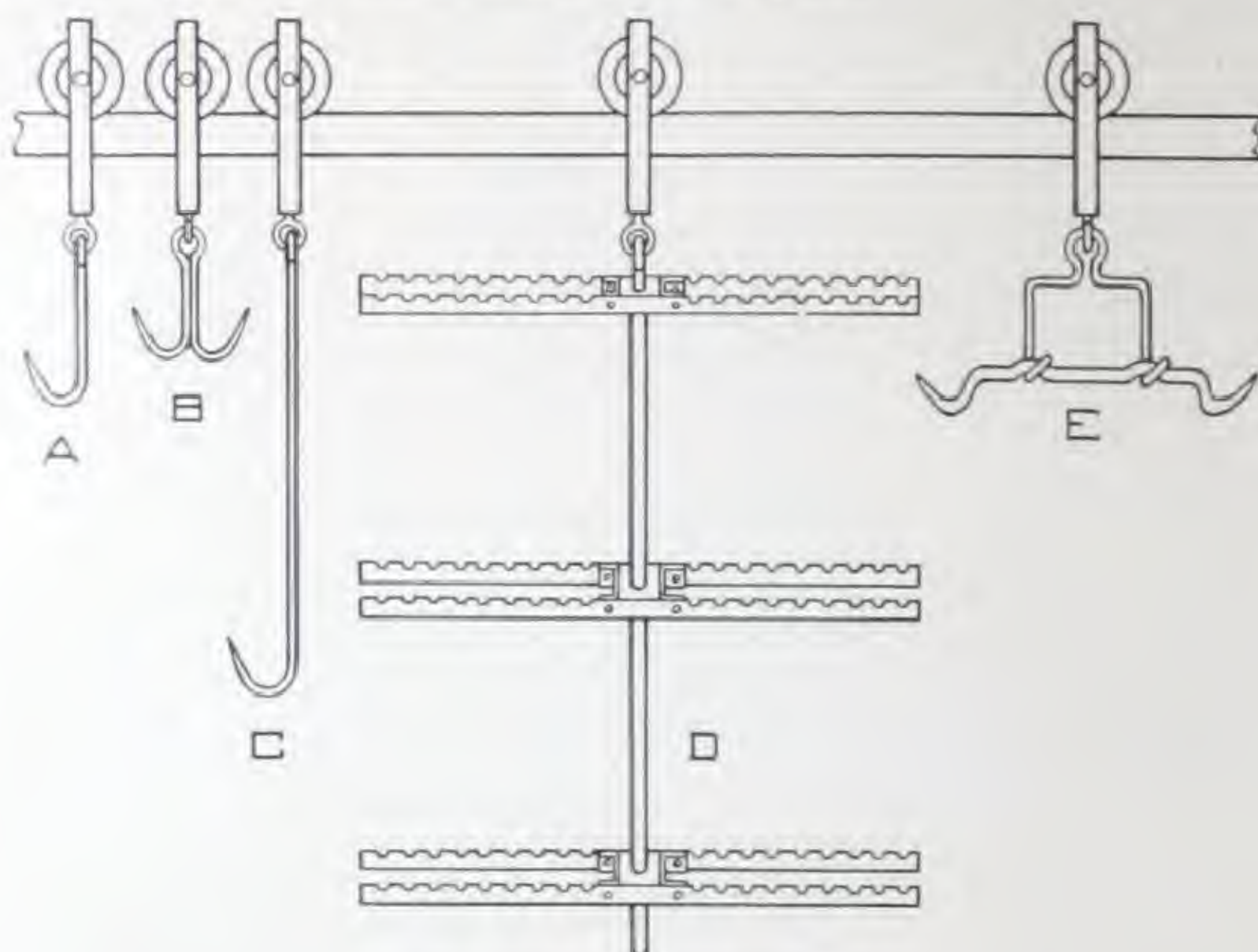
Pritch plates for the beef dressing floor of heavy cast iron with special ribbed surface as illustrated above can be furnished in various sizes to suit conditions.

Made in different designs, varying in weight from 13 to 27 lbs. per square foot.



## MEAT TROLLEYS

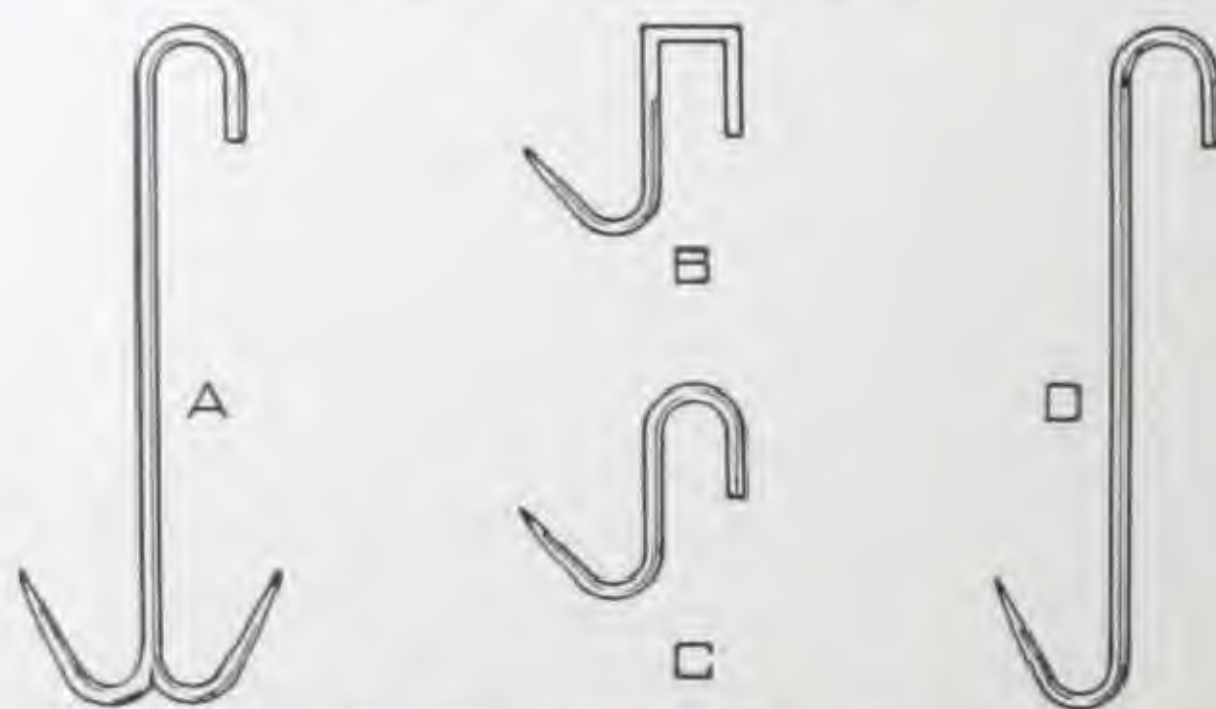
We can supply the most modern and improved designs of trolleys for packing-houses and markets. The wheels are machined in the groove and run on cold rolled steel pins, which makes them very easy to operate.



No. 119—Standard Meat Trolleys

In the illustration above, A represents a hind-quarter beef trolley; B, a double-hook sheep trolley; and C, a fore-quarter beef trolley. A three-station smokehouse trolley is shown by D, while E shows a hog trolley with steel gambrel. Other styles may be had to suit individual requirements.

## CAR AND MEAT HOOKS



No. 120—Types of Meat Hooks

Above are shown some of the types of hooks made for packing-house use. Single and double car hooks are shown by A and D; C represents a shorter car hook, while B shows a meat hook. These hooks can be furnished black or tinned.



# GYMNASIUM EXERCISES



Fig. 100. Truss member view.



Fig. 101. Truss member view.

The device is provided with a series of vertical rods, as the bottom is not a solid plate. It is not necessary to provide a solid plate, as the rods are sufficient to support the structure. The rods are spaced at intervals of 12 inches.



The device is provided with a series of vertical rods, as the bottom is not a solid plate. It is not necessary to provide a solid plate, as the rods are sufficient to support the structure. The rods are spaced at intervals of 12 inches.



## PACKING-HOUSE TRUCKS

We can supply a variety of styles of meat trucks for packing-house use, which will prove well adapted to the style of work done by packers.



No. 123—Sanitary Meat Truck

A popular model is shown by No. 123 above. The body is made of No. 14 steel with all seams welded, which makes it easy to clean. It is made up complete and then galvanized so that all crevices are filled and the body is protected by the heaviest possible coat. Well-rounded corners insure the greatest possible sanitation. The reinforced edge is constructed by bending the sheet over and under, forming a beading which is perfectly smooth and free from crevices. All wheels are accurately fitted to the proper size and with a smooth-running fit on the axle, thereby reducing friction to the minimum.



No. 124—Tank-Charging Truck

The galvanized steel truck shown by No. 124 is well adapted for all work requiring the use of a round-nose truck. The body is made of No. 12 steel with welded seams, rounded corners and galvanizing features as in the model shown by No. 123.

Trucks can be constructed in sizes and styles to meet the ideas of the customer. Please furnish us with particulars and your requests will be accorded the closest attention.

The ty  
standard

Fitting  
valve, d  
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Cap. Gal.	Di I
25	2
50	2
75	2
100	3
150	3
300	4



## RENDERING TANKS

Rendering tanks for any purpose, and in any size to suit the customer's demands, can readily be supplied by us.



The illustration at the left shows a vertical fixed rendering tank for separating grease from lardstock and other matters to yield a fine rendered piece of material.

It is constructed of heavy boiler steel, with large tank and discharge openings, and is equipped with draw-off valves to remove the grease. It can be supplied in any size and for any purpose. Additional details furnished.

No. 128 Vertical Rendering Tank

## LARD KETTLES

The type of fixed and portable lard kettle shown herewith is made in all standard sizes, varying from 15 to 300 gallons in capacity.

Through numerous air valves, stop valves, water pump and draw work for taping the lard.

The table herewith gives the dimensions of the standard sizes of lard kettles.

Capacity Gals.	Height In.	Depth In.	Height In.
25	30	18	42
50	36	24	51
75	42	30	60
100	48	36	69
150	54	42	78
200	60	48	87



No. 129 Portable Lard Kettle



## POLE LINE HARDWARE

We carry a full line of pole line hardware, available in stock sizes, as noted in the following paragraphs, or in additional sizes on special order; the material can be supplied either plain or galvanized by the "hot-dip" process.

**Eye Bolts**—These bolts can be made in any size desired and with eye welded



No. 127—Eye Bolt

or not welded and with square nut. Stocked in the following sizes and weights:

Size, In.	Weight per 100 Lbs.
$\frac{5}{8}$ x 20.....	227
$\frac{5}{8}$ x 22.....	240
$\frac{5}{8}$ x 24.....	260

**Machine or Pole Bolts**—This style of bolt has a square head and nut; sizes



No. 128—Machine Bolt

13 inches long and shorter have four inches of thread, while sizes longer than 13 inches have six inches of thread. The following sizes are stocked:

Size, In.	Weight per 100, Lbs.	Size, In.	Weight per 100, Lbs.
$\frac{5}{8}$ x 10.....	101	$\frac{5}{8}$ x 16.....	150
$\frac{5}{8}$ x 12.....	117	$\frac{5}{8}$ x 18.....	171
$\frac{5}{8}$ x 14.....	133	$\frac{5}{8}$ x 20.....	192
$\frac{5}{8}$ x 15.....	140		

**Double Arming Bolts**—Made with two square nuts and four inches of thread



No. 129—Double Arming Bolt

on each end. Can be supplied to suit any specifications. Stock sizes are:

Size, In.	Weight per 100, Lbs.	Size, In.	Weight per 100, Lb.
$\frac{5}{8}$ x 12.....	131	$\frac{5}{8}$ x 18.....	190
$\frac{5}{8}$ x 14.....	150	$\frac{5}{8}$ x 20.....	212
$\frac{5}{8}$ x 16.....	170		

**Cross-Arm Braces**—Standard cross-arm braces are one inch or  $1\frac{1}{4}$ -inch wide,



No. 130—Cross-Arm Brace

with  $\frac{3}{16}$ -inch holes at ends, center of hole one inch from end of brace. Lengths are as specified. Stock sizes are:

Size, In.	Weight per 100, Lbs.	Size, In.	Weight per 100, Lbs.
$\frac{1}{4}$ x 1 x 24.....	167	$\frac{1}{4}$ x $1\frac{1}{4}$ x 24.....	212
$\frac{1}{4}$ x 1 x 26.....	181	$\frac{1}{4}$ x $1\frac{1}{4}$ x 26.....	230
$\frac{1}{4}$ x 1 x 28.....	195	$\frac{1}{4}$ x $1\frac{1}{4}$ x 28.....	247
$\frac{1}{4}$ x 1 x 30.....	215	$\frac{1}{4}$ x $1\frac{1}{4}$ x 30.....	265



**Transposition Brackets**—These brackets are for use with glass or porcelain



No. 125—Transposition Bracket

insulators. Provided with square end and round glass rubber. Made to suit specifications standard size is:

Size, In.		Weight per 100, Lbs.	
4 1/4 x 1 1/2		30	

**Guy Clamps**—Made of rolled steel with longitudinal grooves to grip wire



No. 126—Guy Clamp (Type A)



No. 126—Guy Clamp (Type B)

One groove type for round wire and one raised grip. Provided for small sizes where dimensions. The following give the standard sizes:

Size, In.		Weight per 100, Lbs.	
4 inch x 4		40	
4 inch x 5		110	
4 inch x 6		130	

**Anchor Rods**—Made with square tapered or long tapered end as per specification



No. 127—Anchor Rod

with flanged end square end or other end. The following sizes are standard in stock:

Size, In.		Weight per 100, Lbs.		Size, In.		Weight per 100, Lbs.	
1/2 x 8		300		1/2 x 10		400	
1/2 x 9		340		1/2 x 11		450	
1/2 x 10		380		1/2 x 12		500	
1/2 x 11		420		1/2 x 14		600	
1/2 x 12		460		1/2 x 16		800	
1/2 x 13		500		1/2 x 18		1000	
1/2 x 14		540		1/2 x 20		1200	
1/2 x 15		580		1/2 x 22		1400	

**Ground Rods**—These rods are made of rolled steel and are to be galvanized and painted or drilled, galvanized and painted. The following sizes are standard in stock:

Standard size Rods		Standard size Rods	
Size, In.		Size, In.	
1/2 x 10	300	1/2 x 10	300
1/2 x 12	400	1/2 x 12	400
1/2 x 14	500	1/2 x 14	500



**Lag Screws**—These screws are made with square head, cone-point drive and cut thread. We carry them in the following stock sizes:

Size, In.	Weight per 100, Lbs.	Size, In.	Weight per 100, Lbs.
$\frac{3}{4} \times 2$	7	$\frac{3}{4} \times 2\frac{1}{2}$	11
$\frac{3}{4} \times 2\frac{1}{2}$	8 $\frac{1}{2}$	$\frac{3}{4} \times 4$	41
$\frac{3}{4} \times 3$	10		

**Pole Shims**—The standard sizes of pole shims are as follows:

Size, In.	Weight per 100, Lbs.	Size, In.	Weight per 100, Lbs.
$\frac{3}{4} \times 1 \times 6$	22	$\frac{3}{4} \times 1 \times 8$	43

**Wire Rope Thimbles**—Made of iron or mild steel and stocked in the following sizes:

Size, In.	Weight per 100, Lbs.
$\frac{7}{8}$	7
1 $\frac{1}{2}$	12

**Square Washers**—Made of pressed steel plate with punched hole. Follows tag list stock sizes:

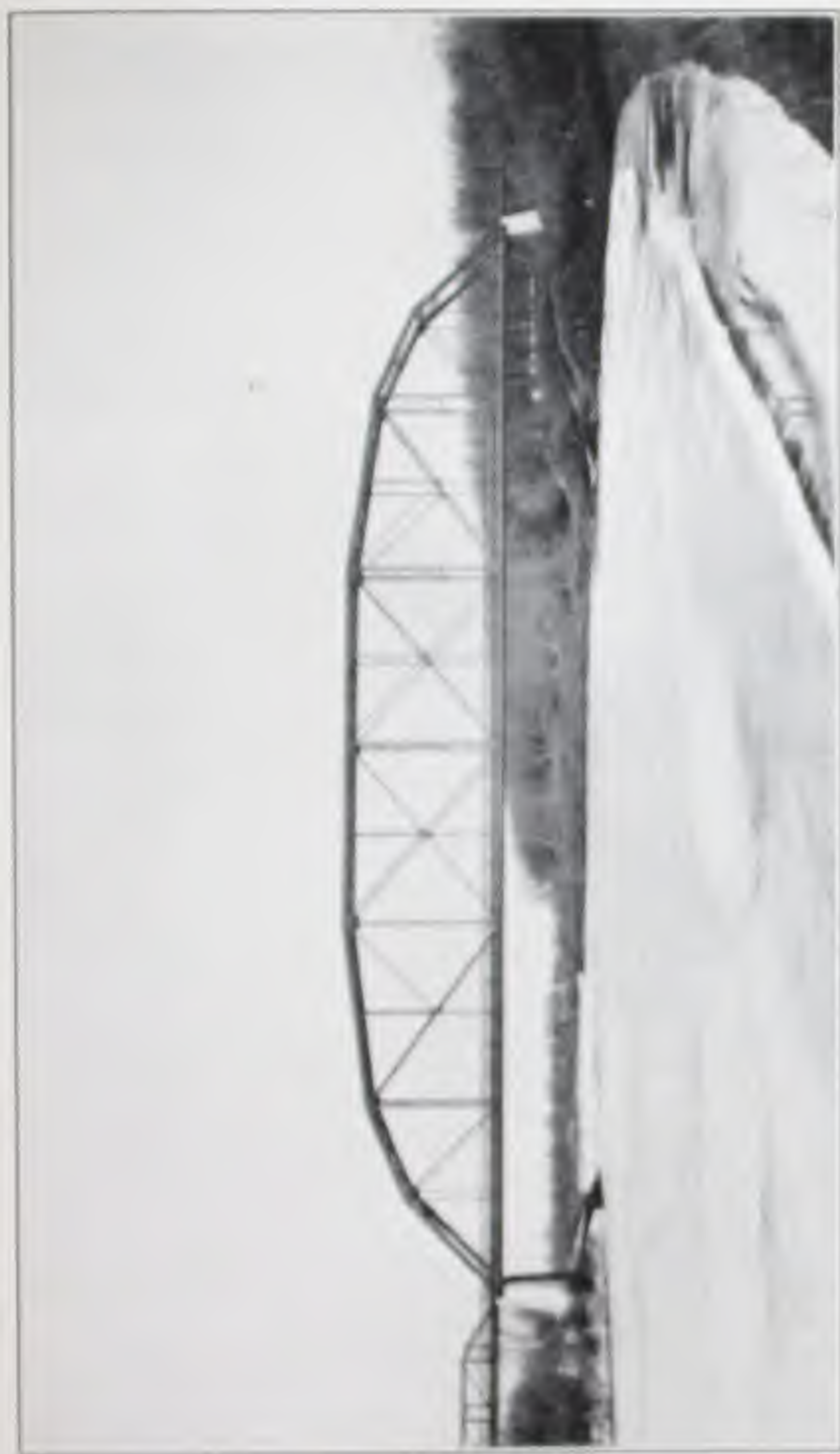
Size, In.	Weight per 100, Lbs.	Size, In.	Weight per 100, Lbs.
$2\frac{1}{4} \times 2\frac{1}{4} \times \frac{1}{8}$	25	$4 \times 4 \times \frac{1}{4}$	115
$2\frac{1}{4} \times 2\frac{1}{4} \times \frac{3}{16}$	32	$4 \times 4 \times \frac{1}{2}$	140
$2\frac{1}{4} \times 2\frac{1}{4} \times \frac{1}{2}$	41	$4 \times 4 \times \frac{3}{4}$	170
$4 \times 4 \times \frac{1}{2}$	85	$4 \times 4 \times \frac{3}{4}$	227

All the previously mentioned lines of pole line hardware can be supplied either plain or "hot-dip" galvanized, and to any specifications, whether provincial government telephones or railway telegraphs.

### COMMERCIAL GALVANIZING

We are fully equipped to handle orders of galvanizing for special commercial purposes, such as tanks, boilers, angles, pump rods, castings, etc. This galvanizing can be done either by the "hot-dip" or by the cold electrolytic process.



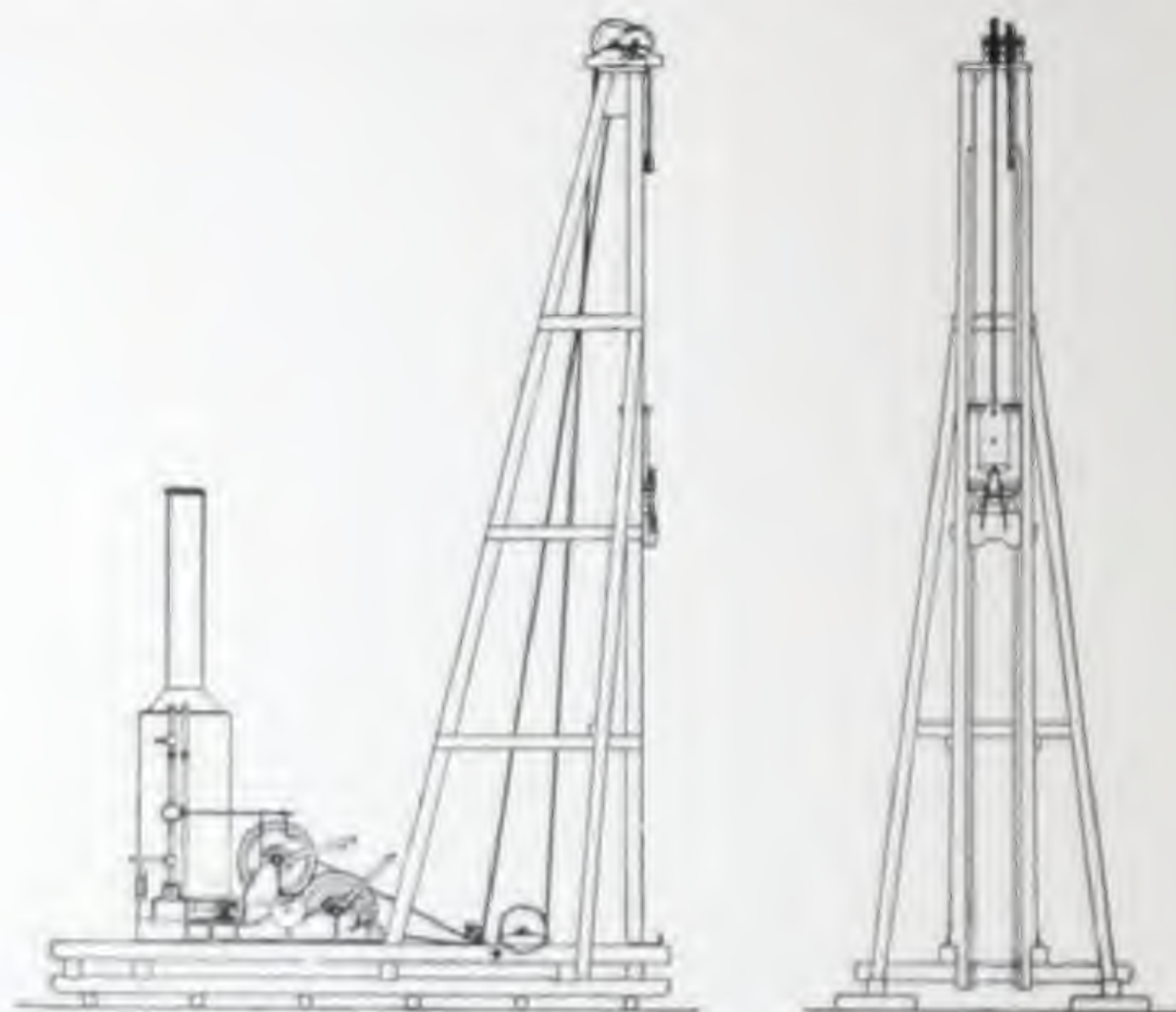


No. 100—100-foot Hollows Bridge over Red River at Minn. Fabricated and erected by The Manitoba Bridge and Iron Works, Limited.



## PILE-DRIVERS

We furnish all iron-work required for any style of pile-driver, but we do not handle the wooden portion of the frame-work. A full set of iron-work usually



No. 136—Contractor's Standard Pile-Driver with Extension Sills

consists of the following: Hammer, with steel pin fitted in; top sheaves; shafts; boxes and belts; toggles with bolts; and channel iron liners with bolts and washers. When a pile cap is used, toggles are not required.

The illustration No. 136 shows a contractor's standard driver with extension sills, adapted to carry the engine. They are also constructed with shorter sills for use when the engine is located elsewhere or when it is necessary to move the leaders in a circle for the purpose of driving a number of piles in a limited area.

A special form of this driver can be arranged by leaving out the rollers under the sills and substituting rigid roller bearings. Four of these would be used, bolted directly to the lower sill, using either the 10-inch iron pipe or 10-inch oak rollers, the roller lying across the driver instead of lengthwise.

Other types of pile-drivers may be constructed to suit customers' specifications; our engineering department will make up designs of any kind of pile-driver for our customers without charge.

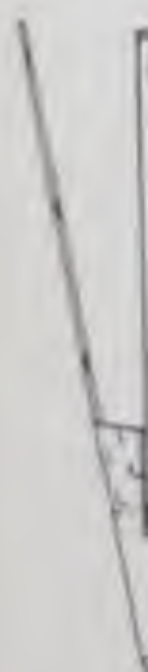
Prices on all iron-work will be supplied on request. When ordering or asking for prices, state fully dimensions of driver and give list of iron-work required.



No. 137—

remaining  
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trimmed  
We supply  
up to 12-  
the casting  
up to 16 in  
diameter  
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driving wh

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time to se  
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No. 140



## PILE HAMMERS



No. 137. Pile Hammer

We have extensive patterns in stock from which we can supply pile-hammers of all sizes and weights, and are able to make pile-hammers to any specifications. Illustration No. 137 shows a differential pile-hammer with differential and constant air-cushion of the variety now in common use very perfectly. In designing we aim to supply the best kind of hammer suitable for the purpose, and we give careful attention to three points:—

1. To get as much of the weight as possible in the hammer.
2. To have the hammer as long as the size of bucket will permit, this gives longer hammer in the water.
3. To have as little size as possible between the hammer and the bucket, this is intended to reduce as much as possible the gap in the water at the moment of impact.

## PILE-CAPS AND COVERS

In foundation work, when not required to be driven, before the piling commences driving, when driven to the end of the bucket, a follower has to be used for the remaining distance. The follower cap shown in No. 138 is mounted on the hammer, the same as the pile cap, in the case of the pile. It is an upper and the remaining upper and holds a pile of the remaining length, with an upper and removed to fit into the pile cap or down hammer. We supply these caps in two sizes. "A" also is for pile up to 17 inches diameter follower, with a 12 inches long the mating is 12 inches long, central. "B" also is for pile up to 14 inches diameter, the upper same as for a 12 inch diameter follower and is 8 inches long, the mating is 12 inches long, central. Both are included. Water-tight joints making what use is required.

To protect pile heads from the weather, and at the same time to serve as an efficient protecting machinery, cylindrical covers are shown in No. 139, and used. The radius of the bucket or cover, the radius of the bucket will be used, no flats are desired in order of cylindrical cover, and water-tight. The regular sizes for this work are 12 in. and 14 in. radius diameter. We have a variety of patterns in stock. Write for prices and details.



No. 138. Follower Cap



No. 139. Cylindrical Cover



No. 140. Pile Shoe

## PILE POINTS OR "SHOES"

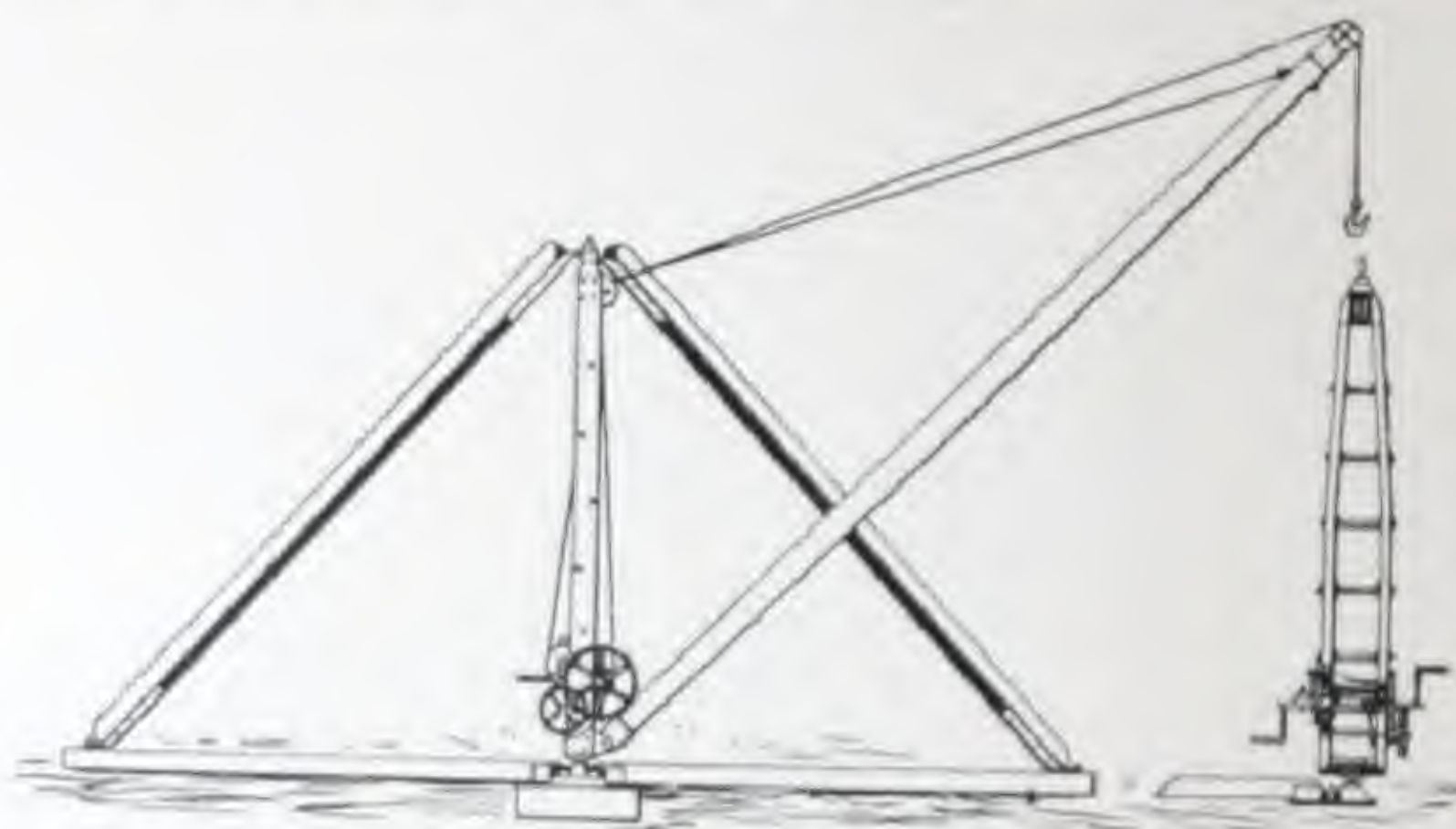
The purpose of a pile shoe is to drive into the sand and sand then connect the pile from the bucket, connecting as a part of the pile hammer. The shoe shown in No. 140 is made of steel, 1/2 in. or 3/4 in. in diameter, with tapering angles of 45° to 60° each side the vertical, and may be mounted on a pile. All shoes are mounted on the top of bucket and 12 inches from water will do, but if a shoe larger size is the pile should be mounted in the water.

Extensive list and work of patterns will gladly be submitted on request.



## DERRICKS

We can supply iron-work for any type of contractors' or builders' derricks, especially of the Scotch and Stiff-Leg design. We make up special steel-angle derricks for use in steel erection and other heavy work.



No. 141—Scotch Derrick—(Hand Power).

## SPECIFICATIONS FOR SCOTCH DERRICK

Capacity, Tons	Length Boom, Ft.	Weight, Lbs.	Rope Equipment			
			Diam. In.	Hoist, Ft.	Boom, Ft.	Total Feet
$\frac{3}{4}$	25	2300	$\frac{1}{2}$	80	45	125
1	25	2400	$\frac{1}{2}$	130	55	185
$1\frac{1}{2}$	30-35	2700	$\frac{3}{8}$	140	65	205
2	35-40	3000	$\frac{3}{8}$	150	75	225
3	40-45	4200	$\frac{3}{8}$	150	75	225
4	40-45	4800	$\frac{3}{8}$	150	75	225
5	45-50	5700	$\frac{3}{8}$	150	110	260

## HORSE POWER OF AN ENGINE

$a$  = area of piston in square inches.

$p$  = mean pressure of the steam on the piston per square inch.

$v$  = velocity of piston per minute in feet.

$$\text{Then H. P.} = \frac{a \times p \times v}{33000}$$



### DERRICK BULL-WHEELS

The bull-wheel, for swinging booms on power derricks is a most valuable feature in any derrick, and will save enough time and labor to pay for itself several times in a season. It may be attached, without changes, to any power derrick mast bottom.



No. 142—Derrick Bull-Wheel

It takes time and money to swing a derrick by hand with men pulling on the tag line when teams, cars or men are waiting for the derrick.

With a bull-wheel and derrick swinging engine, the engineer can lift the load and swing it into place in the time it takes to do the lifting only.

The accompanying illustration shows a 12-foot bull-wheel and gives a good view of the bracing to mast and boom.

### STONE GRABS AND TONGS

We can supply promptly stone-setters' grabs or stone tongs of any capacity merely upon your specification of opening and maximum capacity. No. 143



No. 143—Stone-Setters' Grab



No. 144—Stone Tongs

shows a stone-setters' grab, which can be furnished suitable for any kind of stone. A common style of stone tong is shown by No. 144. Prices quoted upon request.



## ORE BUCKETS

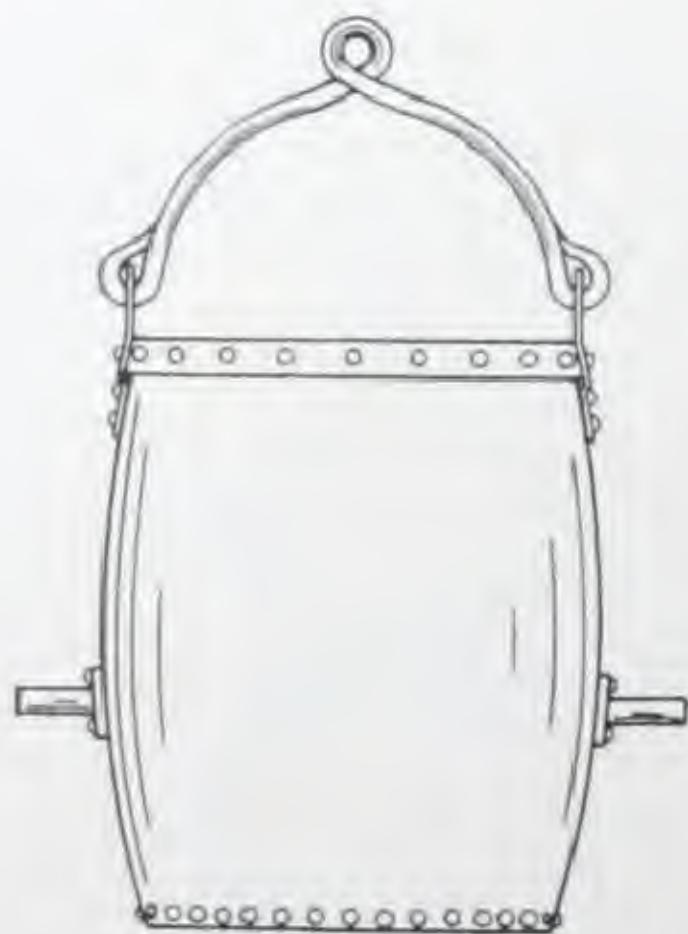
Ore buckets can be supplied in either the self-dumping style or in the regular side-lug type; in the former the bale is attached below the center of gravity and in the latter it is fixed to the bucket above the center of gravity.

**Self-Dumping Type**—The center-swing type of bucket for easy dumping is shown by No. 145. It is constructed throughout of  $\frac{3}{16}$ -inch steel, except in the  $1\frac{1}{2}$ -cubic-yard size, in which the bottom is  $\frac{1}{4}$ -inch steel. The bail and trunnions are heavy, while the catch is strong, reliable and simple in operation. Specifications for this type of bucket follow:

No. 145 (At Right)—Self-Dumping Ore Bucket



Capacity	Diam. Top, In.	Diam. Bottom, In.	Depth, In.	Weight, Lbs.
8 Cubic Feet	26	23	27	240
10 Cubic Feet	29	25	30	300
$\frac{1}{2}$ Cubic Yard	32	27	35	360
$\frac{3}{4}$ Cubic Yard	36	31	40	430
1 Cubic Yard	39	34	45	500
$1\frac{1}{2}$ Cubic Yards	45	40	50	650



**Regular Type**—The sides and bottom of this style of bucket, illustrated by No. 146, are made of  $\frac{3}{16}$ -inch steel, pressed into shape by hydraulic pressure. The sides have welded or countersunk-riveted seams to prevent catching upon sides of shaft. Banded around top. This bucket can be constructed in any size to suit any specification. Estimates furnished on request.

No. 146 (At Left)—Regular Style Ore Bucket



## CONTRACTORS' BUCKETS

We can construct self-dumping and self-righting contractors' buckets to suit individual requirements. Steel plate,  $\frac{3}{8}$ -inch, is used, securely rivetted. The



No. 147—Self Dumping Bucket



No. 148—Self-Righting Bucket

illustrations show both types of contractors' buckets, self-dumping and self-righting, in typical patterns. Write for prices giving full particulars as to height, diameter, capacity, etc.

## DERRICK SKIPS

Derrick skips for handling stone, clay, earth, etc., can be supplied in either steel or wood construction and in any design required. The skip shown in No. 149 is constructed of well-ironed two-inch oak in any capacity specified, usually one



No. 149—Wooden Derrick Skip



No. 150—Steel Derrick Skip

or two cubic yards. No. 150 illustrates the steel derrick skip of which the standard capacity is 35 cubic feet. The box is constructed of No. 8 steel, well rivetted and braced, with angle corners and flat top band, and supported by three  $\frac{1}{2}$ -inch diameter chains. Heavier skips of any size can be supplied on order.

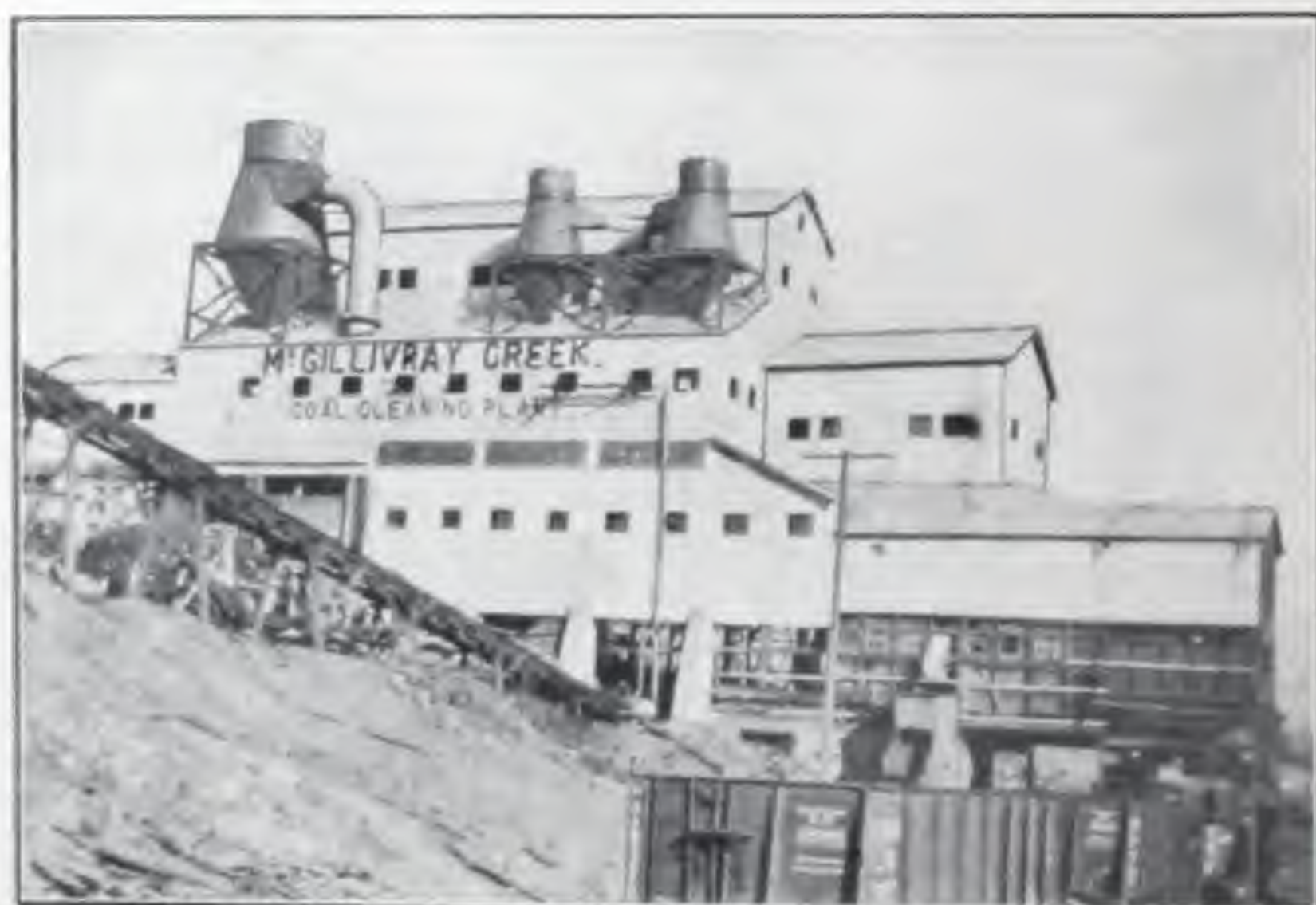
When ordering or asking for prices specify full dimensions, thickness of plate or wood desired, where chains are to be attached, etc.



# COAL-MINING EQUIPMENT



No. 151—Steel Tipple and Pneumatic Cleaning Plant of the International Coal and Coke Company, Coleman, Alta.



No. 152—McGillivray Creek Coal and Coke Co.'s Steel Tipple and Pneumatic Cleaning Plant at Coleman, Alta.

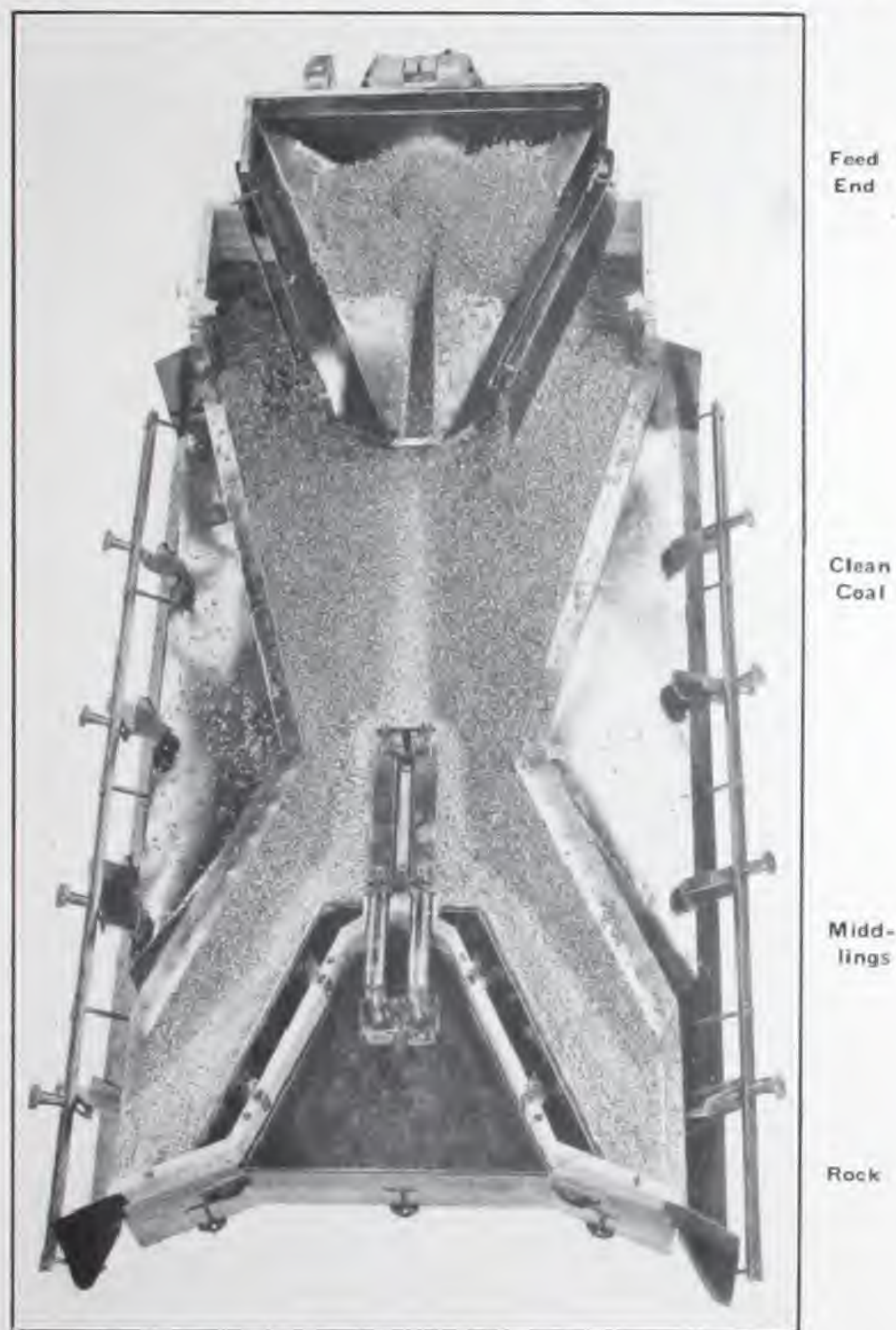
We design, fabricate and erect coal-mining buildings and equipment of all kinds, including pneumatic tables for coal-cleaning, Marcus screens, rotary dumps,

shaking,  
conveyors,  
separator  
work for  
Merco

The  
rock and  
Winnipeg  
W.Va.  
five Y-  
Canada



shaking, rotary and bar screens, weigh pans, pan, belt, scraper and Eickhoff conveyors, elevators, belt and chain car irons, steel car ends, steel rock cars, spiral separators, etc. We specialize particularly in all-steel coal tipples and have done work for many of the prominent Western Canadian mines including Regal, Luscar, Mercoal, Cadomin, International, McGillivray and West Canadian Collieries.



No. 153—Air-Cleaning Y-Table.

The illustration above conveys a good idea of the definite stream-line between rock and coal on the pneumatic table. These tables are manufactured by us at Winnipeg under license from the American Coal Cleaning Corporation, Welch, W.Va. Three Y- and three SJ-tables are installed in the International plant, five Y- and one SJ-table at the McGillivray plant, and two SJ-tables at the West Canadian Collieries' Bellevue plant.



## MINE CARS

All-steel dump cars for carrying stone, clay, earth, cinders, ashes, coal, concrete, etc., can be supplied according to specifications. These cars may have hook or rotary dump arrangement.



No. 154—Hook Dump Car



No. 155—Rotary Dump Car

The hook type of sub-dump car is seen in No. 154 above, in dumping position. The dumping arrangement is positive and easily worked, none of the contents falling between the rails. Box can be held in a slanting position for convenience in loading.

A scoop-bed dump car of rotary type is illustrated in dumping position by No. 155. The body is supported on a wrought steel turn-table and is securely locked to the track by a treadle catch; when unlocked, body is swung on its turn-table, permitting the load to be dumped at the end or either side.

All cars are made of  $\frac{1}{2}$ -inch steel plate riveted. We are prepared to design and manufacture all steel cars for any purpose whatever. Wheels, axles, trucks, etc., will also be furnished without the cars if wanted. We have a number of patterns of car wheels in stock and can promise quick delivery of material.

For coal mines we can supply complete sets of trams for use with wooden cars; we also manufacture steel plate cars for wooden cars.



## FIELD STOVES

Field stoves or salamanders are used by contractors, water supply companies, and others, for heating food on construction work, for heating buildings under construction, and for similar purposes.

The sides of the stoves are of No. 14-gauge plate, riveted; the grate is of  $\frac{1}{2}$ -inch cast iron plate, perforated.

Field stoves may be supplied with or without handles, as desired.

All sizes of field stoves can be made to order, unless patterns are available if desired.

In writing for prices, state sizes required and specify preference as to patterns.



No. 156 (21 Left)—Field Stove or Salamander



# COAL AND ASH HANDLING EQUIPMENT

The design, manufacture and erection of all handling equipment for power houses, in the Dominion and abroad, is a specialty of this firm. We have installed many large systems for the Dominion and abroad.



No. 100. Heavy hoist, installed at the Maryton Bridge and Iron Works, Ltd., Maryton, Alberta.

We also supply machinery for the handling of coal and ash from the Maryton Bridge and Iron Works, Ltd., Maryton, Alberta, and from other sources.



# SEAMLESS BOILER TUBES

## WEIGHTS AND DIMENSIONS

Ex- ternal Diam.	MINIMUM STANDARD THICKNESS		Nominal Weight per Foot in Pounds					
	Birming- ham Wire Gauge	Inches	STANDARD THICKNESS		ONE EXTRA WIRE GAUGE		TWO EXTRA WIRE GAUGES	
			Exact Theoret- ical Weight	Approx. Manu- fact'g Weight	Exact Theoret- ical Weight	Approx. Manu- fact'g Weight	Exact Theoret- ical Weight	Approx. Manu- fact'g Weight
1	13	.095	.92	1.06	1.04	1.20	1.13	1.30
1 1/4	13	.095	1.17	1.34	1.33	1.53	1.45	1.67
1 1/2	13	.095	1.42	1.63	1.62	1.86	1.77	2.03
1 3/4	13	.095	1.68	1.93	1.91	2.20	2.09	2.40
2	13	.095	1.93	2.22	2.20	2.53	2.41	2.77
2 1/4	13	.095	2.19	2.52	2.49	2.86	2.73	3.14
2 1/2	12	.109	2.78	3.20	3.05	3.51	3.39	3.90
2 3/4	12	.109	3.07	3.53	3.37	3.87	3.74	4.30
3	12	.109	3.37	3.87	3.69	4.24	4.10	4.71
3 1/4	11	.120	4.01	4.61	4.46	5.00	4.90	5.63
3 1/2	11	.120	4.33	4.98	4.82	5.54	5.30	6.09
4	10	.134	5.53	6.36	6.09	7.00	6.76	7.77
4 1/2	10	.134	6.25	7.18	6.88	7.91	7.64	8.78
5	9	.148	7.67	8.82	8.52	9.79	9.27	10.66
6	8	.165	10.28	11.82	11.19	12.86	12.57	14.45
			THREE EXTRA WIRE GAUGES		FOUR EXTRA WIRE GAUGES			
			Exact Theoretical Weight	Approx. Manuf'g Weight	Exact Theoretical Weight	Approx. Manuf'g Weight		
1	13	.095	1.24	1.43	1.35	1.55		
1 1/4	13	.095	1.60	1.84	1.74	2.00		
1 1/2	13	.095	1.95	2.24	2.14	2.46		
1 3/4	13	.095	2.31	2.66	2.53	2.91		
2	13	.095	2.67	3.07	2.93	3.37		
2 1/4	13	.095	3.02	3.47	3.32	3.82		
2 1/2	12	.109	3.72	4.28	4.12	4.74		
2 3/4	12	.109	4.11	4.72	4.56	5.24		
3	12	.109	4.51	5.18	5.00	5.75		
3 1/4	11	.120	5.44	6.25	5.90	6.78		
3 1/2	11	.120	5.88	6.76	6.38	7.33		
4	10	.134	7.34	8.44	8.23	9.46		
4 1/2	10	.134	8.30	9.54	9.32	10.71		
5	9	.148	10.40	11.95	11.23	12.91		
6	8	.165	13.58	15.61	14.65	16.84		

Boiler tubes to special specifications, if desired.



# **BOILER TUBES** **STANDARD DIMENSIONS**

Nom. diam. in.	Nom. wall thick.	Length in.	Weight lb.	Nominal diam. in.		Nominal wall thick. in.		Length in.		Weight lb.
				Inside	Outside	Inside	Outside	Inside	Outside	
1		8100	1800 12	2 1/2	2 3/4	1/16	3/16	2000	2100	210
1 1/4		1800	1800 12	2 3/4	2 7/8	1/16	3/16	2100	2200	220
1 1/2		3100	1800 12	3 1/4	3 1/2	1/16	3/16	2100	2200	220
1 3/4		3800	1800 12	3 3/4	3 7/8	1/16	3/16	2100	2200	220
2		4200	1800 12	4 1/4	4 1/2	1/16	3/16	2100	2200	220
2 1/4		2 1800	1800 12	4 3/4	4 7/8	1/16	3/16	2100	2200	220
2 1/2		2 2800	1800 12	5 1/4	5 1/2	1/16	3/16	2100	2200	220
2 3/4		2 3800	1800 12	5 3/4	5 7/8	1/16	3/16	2100	2200	220
3		2 4800	1800 12	6 1/4	6 1/2	1/16	3/16	2100	2200	220
3 1/4		2 5800	1800 12	6 3/4	6 7/8	1/16	3/16	2100	2200	220
3 1/2		2 6800	1800 12	7 1/4	7 1/2	1/16	3/16	2100	2200	220
3 3/4		2 7800	1800 12	7 3/4	7 7/8	1/16	3/16	2100	2200	220
4		2 8800	1800 12	8 1/4	8 1/2	1/16	3/16	2100	2200	220
4 1/4		2 9800	1800 12	8 3/4	8 7/8	1/16	3/16	2100	2200	220
4 1/2		3 0800	1800 12	9 1/4	9 1/2	1/16	3/16	2100	2200	220
4 3/4		3 1800	1800 12	9 3/4	9 7/8	1/16	3/16	2100	2200	220
5		3 2800	1800 12	10 1/4	10 1/2	1/16	3/16	2100	2200	220
5 1/4		3 3800	1800 12	10 3/4	10 7/8	1/16	3/16	2100	2200	220
5 1/2		3 4800	1800 12	11 1/4	11 1/2	1/16	3/16	2100	2200	220
5 3/4		3 5800	1800 12	11 3/4	11 7/8	1/16	3/16	2100	2200	220
6		3 6800	1800 12	12 1/4	12 1/2	1/16	3/16	2100	2200	220
6 1/4		3 7800	1800 12	12 3/4	12 7/8	1/16	3/16	2100	2200	220
6 1/2		3 8800	1800 12	13 1/4	13 1/2	1/16	3/16	2100	2200	220
6 3/4		3 9800	1800 12	13 3/4	13 7/8	1/16	3/16	2100	2200	220
7		4 0800	1800 12	14 1/4	14 1/2	1/16	3/16	2100	2200	220
7 1/4		4 1800	1800 12	14 3/4	14 7/8	1/16	3/16	2100	2200	220
7 1/2		4 2800	1800 12	15 1/4	15 1/2	1/16	3/16	2100	2200	220
7 3/4		4 3800	1800 12	15 3/4	15 7/8	1/16	3/16	2100	2200	220
8		4 4800	1800 12	16 1/4	16 1/2	1/16	3/16	2100	2200	220
8 1/4		4 5800	1800 12	16 3/4	16 7/8	1/16	3/16	2100	2200	220
8 1/2		4 6800	1800 12	17 1/4	17 1/2	1/16	3/16	2100	2200	220
8 3/4		4 7800	1800 12	17 3/4	17 7/8	1/16	3/16	2100	2200	220
9		4 8800	1800 12	18 1/4	18 1/2	1/16	3/16	2100	2200	220
9 1/4		4 9800	1800 12	18 3/4	18 7/8	1/16	3/16	2100	2200	220
9 1/2		5 0800	1800 12	19 1/4	19 1/2	1/16	3/16	2100	2200	220
9 3/4		5 1800	1800 12	19 3/4	19 7/8	1/16	3/16	2100	2200	220
10		5 2800	1800 12	20 1/4	20 1/2	1/16	3/16	2100	2200	220
10 1/4		5 3800	1800 12	20 3/4	20 7/8	1/16	3/16	2100	2200	220
10 1/2		5 4800	1800 12	21 1/4	21 1/2	1/16	3/16	2100	2200	220
10 3/4		5 5800	1800 12	21 3/4	21 7/8	1/16	3/16	2100	2200	220
11		5 6800	1800 12	22 1/4	22 1/2	1/16	3/16	2100	2200	220
11 1/4		5 7800	1800 12	22 3/4	22 7/8	1/16	3/16	2100	2200	220
11 1/2		5 8800	1800 12	23 1/4	23 1/2	1/16	3/16	2100	2200	220
11 3/4		5 9800	1800 12	23 3/4	23 7/8	1/16	3/16	2100	2200	220
12		6 0800	1800 12	24 1/4	24 1/2	1/16	3/16	2100	2200	220
12 1/4		6 1800	1800 12	24 3/4	24 7/8	1/16	3/16	2100	2200	220
12 1/2		6 2800	1800 12	25 1/4	25 1/2	1/16	3/16	2100	2200	220
12 3/4		6 3800	1800 12	25 3/4	25 7/8	1/16	3/16	2100	2200	220
13		6 4800	1800 12	26 1/4	26 1/2	1/16	3/16	2100	2200	220
13 1/4		6 5800	1800 12	26 3/4	26 7/8	1/16	3/16	2100	2200	220
13 1/2		6 6800	1800 12	27 1/4	27 1/2	1/16	3/16	2100	2200	220
13 3/4		6 7800	1800 12	27 3/4	27 7/8	1/16	3/16	2100	2200	220
14		6 8800	1800 12	28 1/4	28 1/2	1/16	3/16	2100	2200	220
14 1/4		6 9800	1800 12	28 3/4	28 7/8	1/16	3/16	2100	2200	220
14 1/2		7 0800	1800 12	29 1/4	29 1/2	1/16	3/16	2100	2200	220
14 3/4		7 1800	1800 12	29 3/4	29 7/8	1/16	3/16	2100	2200	220
15		7 2800	1800 12	30 1/4	30 1/2	1/16	3/16	2100	2200	220
15 1/4		7 3800	1800 12	30 3/4	30 7/8	1/16	3/16	2100	2200	220
15 1/2		7 4800	1800 12	31 1/4	31 1/2	1/16	3/16	2100	2200	220
15 3/4		7 5800	1800 12	31 3/4	31 7/8	1/16	3/16	2100	2200	220
16		7 6800	1800 12	32 1/4	32 1/2	1/16	3/16	2100	2200	220
16 1/4		7 7800	1800 12	32 3/4	32 7/8	1/16	3/16	2100	2200	220
16 1/2		7 8800	1800 12	33 1/4	33 1/2	1/16	3/16	2100	2200	220
16 3/4		7 9800	1800 12	33 3/4	33 7/8	1/16	3/16	2100	2200	220
17		8 0800	1800 12	34 1/4	34 1/2	1/16	3/16	2100	2200	220
17 1/4		8 1800	1800 12	34 3/4	34 7/8	1/16	3/16	2100	2200	220
17 1/2		8 2800	1800 12	35 1/4	35 1/2	1/16	3/16	2100	2200	220
17 3/4		8 3800	1800 12	35 3/4	35 7/8	1/16	3/16	2100	2200	220
18		8 4800	1800 12	36 1/4	36 1/2	1/16	3/16	2100	2200	220
18 1/4		8 5800	1800 12	36 3/4	36 7/8	1/16	3/16	2100	2200	220
18 1/2		8 6800	1800 12	37 1/4	37 1/2	1/16	3/16	2100	2200	220
18 3/4		8 7800	1800 12	37 3/4	37 7/8	1/16	3/16	2100	2200	220
19		8 8800	1800 12	38 1/4	38 1/2	1/16	3/16	2100	2200	220
19 1/4		8 9800	1800 12	38 3/4	38 7/8	1/16	3/16	2100	2200	220
19 1/2		9 0800	1800 12	39 1/4	39 1/2	1/16	3/16	2100	2200	220
19 3/4		9 1800	1800 12	39 3/4	39 7/8	1/16	3/16	2100	2200	220
20		9 2800	1800 12	40 1/4	40 1/2	1/16	3/16	2100	2200	220
20 1/4		9 3800	1800 12	40 3/4	40 7/8	1/16	3/16	2100	2200	220
20 1/2		9 4800	1800 12	41 1/4	41 1/2	1/16	3/16	2100	2200	220
20 3/4		9 5800	1800 12	41 3/4	41 7/8	1/16	3/16	2100	2200	220
21		9 6800	1800 12	42 1/4	42 1/2	1/16	3/16	2100	2200	220
21 1/4		9 7800	1800 12	42 3/4	42 7/8	1/16	3/16	2100	2200	220
21 1/2		9 8800	1800 12	43 1/4	43 1/2	1/16	3/16	2100	2200	220
21 3/4		9 9800	1800 12	43 3/4	43 7/8	1/16	3/16	2100	2200	220
22		10 0800	1800 12	44 1/4	44 1/2	1/16	3/16	2100	2200	220
22 1/4		10 1800	1800 12	44 3/4	44 7/8	1/16	3/16	2100	2200	220
22 1/2		10 2800	1800 12	45 1/4	45 1/2	1/16	3/16	2100	2200	220
22 3/4		10 3800	1800 12	45 3/4	45 7/8	1/16	3/16	2100	2200	220
23		10 4800	1800 12	46 1/4	46 1/2	1/16	3/16	2100	2200	220
23 1/4		10 5800	1800 12	46 3/4	46 7/8	1/16	3/16	2100	2200	220
23 1/2		10 6800	1800 12	47 1/4	47 1/2	1/16	3/16	2100	2200	220
23 3/4		10 7800	1800 12	47 3/4	47 7/8	1/16	3/16	2100	2200	220
24		10 8800	1800 12	48 1/4	48 1/2	1/16	3/16	2100	2200	220
24 1/4		10 9800	1800 12	48 3/4	48 7/8	1/16	3/16	2100	2200	220
24 1/2		11 0800	1800 12	49 1/4	49 1/2	1/16	3/16	2100	2200	220
24 3/4		11 1800	1800 12	49 3/4	49 7/8	1/16	3/16	2100	2200	220
25		11 2800	1800 12	50 1/4	50 1/2	1/16	3/16	2100	2200	220
25 1/4		11 3800	1800 12	50 3/4	50 7/8	1/16	3/16	2100	2200	220
25 1/2		11 4800	1800 12	51 1/4	51 1/2	1/16	3/16	2100	2200	220
25 3/4		11 5800	1800 12	51 3/4	51 7/8	1/16	3/16	2100	2200	220
26		11 6800	1800 12	52 1/4	52 1/2	1/16	3/16	2100	2200	220
26 1/4		11 7800	1800 12	52 3/4	52 7/8	1/16	3/16	2100	2200	220
26 1/2		11 8800	1800 12	53 1/4	53 1/2	1/16	3/16	2100	2200	220
26 3/4		11 9800	1800 12	53 3/4	53 7/8	1/16	3/16	2100	2200	220
27		12 0800	1800 12	54 1/4	54 1/2	1/16	3/16	2100	2200	220
27 1/4		12 1800	1800 12	54 3/4	54 7/8	1/16	3/16	2100	2200	220
27 1/2		12 2800	1800 12	55 1/4	55 1/2	1/16	3/16	2100	2200	220
27 3/4		12 3800	1800 12	55 3/4	55 7/8	1/16	3/16	2100	2200	220
28		12 4800	1800 12	56 1/4	56 1/2	1/16	3/16	2100	2200	220
28 1/4		12 5800	1800 12	56 3/4	56 7/8	1/16	3/16	2100	2200	220
28 1/2		12 6800	1800 12	57 1/4	57 1/2	1/16	3/16	2100	2200	220
28 3/4		12								



### STANDARD WROUGHT MERCHANT PIPE FOR STEAM, WATER, GAS AND OIL

Nominal Inside Diam., In.	Thick- ness, In.	Nominal Wt. per Ft., Lbs.	No. of Threads per In. of Screw	Nominal Inside Diam., In.	Thick- ness, In.	Nominal Wt. per Ft., Lbs.	No. of Threads per In. of Screw
$\frac{1}{8}$	.068	.24	27	$3\frac{1}{2}$	.226	9.00	8
$\frac{1}{4}$	.088	.42	18	4	.237	10.66	8
$\frac{3}{8}$	.091	.56	18	$4\frac{1}{2}$	.246	12.34	8
$\frac{1}{2}$	.109	.84	14	5	.259	14.50	8
$\frac{3}{4}$	.113	1.12	14	6	.280	18.76	8
1	.134	1.67	$11\frac{1}{2}$	7	.301	23.27	8
$1\frac{1}{4}$	.140	2.24	$11\frac{1}{2}$	8	.322	28.18	8
$1\frac{1}{2}$	.145	2.68	$11\frac{1}{2}$	9	.344	33.70	8
2	.154	3.61	$11\frac{1}{2}$	10	.366	40.06	8
$2\frac{1}{2}$	.204	5.74	8	1	.375	45.02	8
3	.217	7.54	8	2	.375	49.00	8

Stock lengths of merchant pipe are 19, 21 and 22 feet.

### "XX" STRONG PIPE

Size, In.	Actual Out- side Diam., In.	Nom- inal Inside Diam., In.	Thick- ness, In.	Nom- inal Wt. per Ft., Lbs.	Size, In.	Actual Out- side Diam., In.	Nom- inal Inside Diam., In.	Thick- ness, In.	Nom- inal Wt. per Ft., Lbs.
$\frac{1}{8}$	.84	.244	.298	1.70	$3\frac{1}{2}$	4.00	2.716	.642	22.75
$\frac{3}{4}$	1.05	.422	.314	2.44	4	4.50	3.136	.682	27.48
1	1.315	.587	.364	3.65	$4\frac{1}{2}$	5.00	3.56	.72	32.53
$1\frac{1}{4}$	1.66	.885	.388	5.20	5	5.563	4.063	.75	38.12
$1\frac{1}{2}$	1.90	1.088	.406	6.40	6	6.625	4.875	.875	53.11
2	2.375	1.491	.442	9.02	7	7.625	5.875	.875	62.38
$2\frac{1}{2}$	2.875	1.755	.560	13.68	8	8.625	6.875	.875	71.62
3	3.50	2.284	.608	18.56					

Stock lengths of "XX" Pipe are 19, 21 and 22 feet. This class of pipe is always shipped, plain ends, unless otherwise specified.

The outside diameters of "XX" pipe are the same as standard, the extra thick-ness decreasing the inside diameter.

### CAST IRON PIPE

We manufacture cast iron specials of all classes, in elbows, tees, bends, etc., and will send estimates on receipt of specifications.





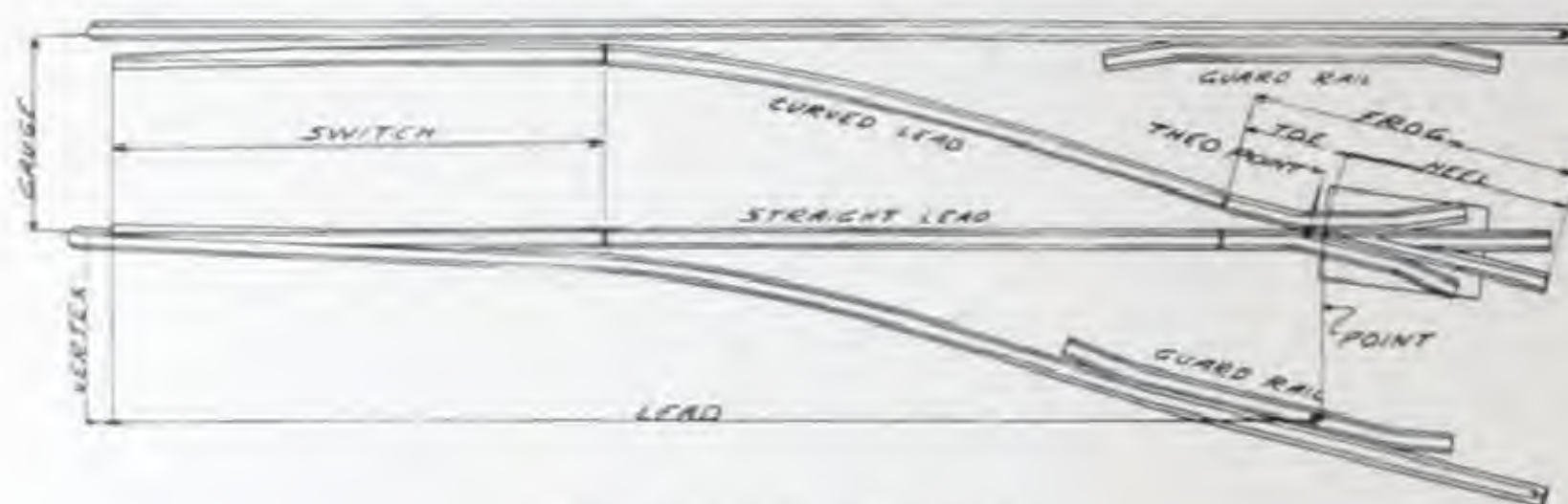
No. 158—Railway Bridge, Fabricated and in Process of Erection by the Manitoba Bridge and Iron Works, Limited



## RAILWAY TURNOUTS

We are manufacturers of complete lines of frog and switch material and diamonds for railway, industrial and mine work. The superior merit of our work is attested to by the fact that we build for both the Canadian National Railways and the Canadian Pacific Railway.

The illustration herewith shows the different parts that enter into a complete turnout. The gauge may vary from standard railway gauge down to the smallest industrial track, and the weight of the rails may range from 100 lbs. per yard, as used on the heaviest railway sections, down to 12-lb. rail used in industrial plants.



No. 159—Railway Turnout

Switches may be stub, split, spring or automatic; they may be operated by ground throws or switch stands. They can be supplied complete with riser plates, braces, bridle bars, switch rods, etc., in the most complicated types for heavy railroad traffic, or in the simplest style for periodic light traffic.

Guard rails may be plain bent for light rail, or bent and planed for heavy rail, and spiked to ties, or bent, planed and chamfered for heavy rail, and bolted to the main rail with cast iron adjustable separators.

Frogs may be bolted rigid, spring or forged for light rail, and may be made with cast manganese centers for heavy rail.

Railroad crossings or diamonds are made to any angle, of strong rigid construction. Flangeways of crossing track are planed through the heads of the rails, leaving webs and bases uncut. The filling material used for diamonds is forged wrought iron, and heavy rolled straps are used for the inside and outside corners.

Bolts are from  $\frac{7}{8}$ -inch to  $1\frac{1}{8}$ -inch diameter, depending on the size of rail, and are furnished with head and nut locks.

Crossings can be made in any number, of any rail, of any angle, with or without curves.

We make up tongue switches and mates for street railways, for use on paved streets. To ensure length of wear, these are made of special material.

We also manufacture Jackson switch stands, both low and high type, as well as ground throws, both hand and automatic.



## RAILWAY FROGS

We are capable of making any size, standard or special, single or double frog and right or left hand frog with our complete range of plant and tools.

A frog frog is a piece of metal, usually shaped by one of our machines, to form a frog. The frog is usually made of steel, and is usually made with a single or double frog.



Fig. 1. Frog frog.

The frog frog is a piece of metal, usually shaped by one of our machines, to form a frog. The frog is usually made of steel, and is usually made with a single or double frog. The frog is usually made with a single or double frog.

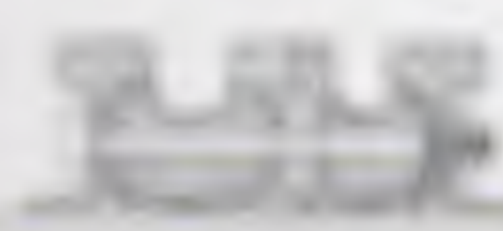


Fig. 2. Frog frog.



Fig. 3. Frog frog.

Fig. 4. Frog frog.

The frog frog is a piece of metal, usually shaped by one of our machines, to form a frog. The frog is usually made of steel, and is usually made with a single or double frog. The frog is usually made with a single or double frog.

The frog frog is a piece of metal, usually shaped by one of our machines, to form a frog. The frog is usually made of steel, and is usually made with a single or double frog. The frog is usually made with a single or double frog.



## CONCRETE REINFORCING BARS

Concrete reinforcing bars can be rolled in the shapes shown below, to any specification, structural, intermediate or hard grade, and in lengths up to eighty feet. For weights of reinforcing, see table of Rounds and Squares, pages 25 and 26.



No. 162—Plain Round



No. 163—Plain Square



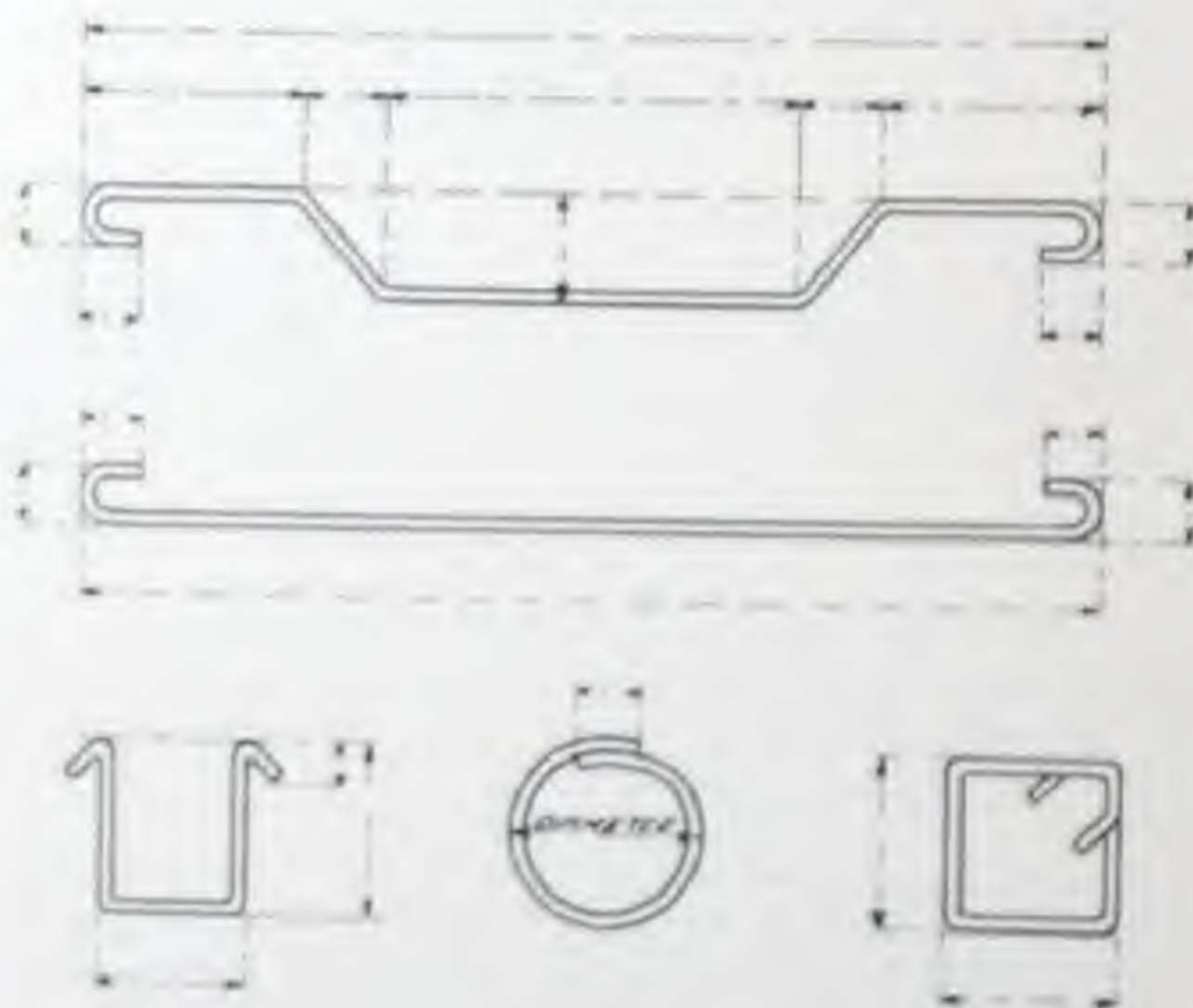
No. 164—Cold Twisted



No. 165—Deformed Round or Square

Our reinforcing bar stock of plain and deformed bars is very complete and our equipment enables us to bend reinforcing to any shape. We can make very prompt shipments from stock. Concrete specialties such as bar chairs, spacers, tees, inserts, etc., can be supplied to meet any requirements. We can also furnish wire mesh, expanded metal wire, small channels, etc.

It is to the contractor's advantage to have all reinforcing bent to shape in the shops. For the commoner different types of bars, the dimensions as shown in the diagram below, should be given. In ordering bent reinforcement, always give dimensions from outside to outside of bars.



No. 166—Dimensions Required when Ordering Reinforcing

We can also supply spirals, in ordering which, give size of wire, outside diameter of core, pitch or distance centre to centre of wire, overall length and number of spacers.



## REINFORCED CONCRETE DESIGN

The design of reinforced concrete structures assumes that the concrete and the reinforcement behave exactly as a unit and that perfect bond exists between the two materials. During such the process, the structuring of data, based upon actual test, follows the common theory of stress, moment and strain used for the concrete.

## STANDARD NOTATION

The following symbols are recommended for use in standard notation:

## a) Rectangular Beams:

- |   |  |
|---|--|
| 1. $\rightarrow$ Depth of beam in span.                         | 1. $\rightarrow$ Depth of beam.                        |
| 2. $\rightarrow$ Compressive unit stress in concrete.           | 2. $\rightarrow$ Depth of beam in span at end.         |
| 3. $\rightarrow$ Modulus of elasticity of steel.                | 3. $\rightarrow$ Depth of beam in span at end of beam. |
| 4. $\rightarrow$ Modulus of elasticity of concrete.             | 4. $\rightarrow$ Depth of beam in span at end of beam. |
| 5. $\rightarrow$ $\frac{f_c}{E_c}$ .                            | 5. $\rightarrow$ Depth of beam in span at end of beam. |
| 6. $\rightarrow$ Distance of reinforcement from bottom of beam. | 6. $\rightarrow$ Depth of beam in span at end of beam. |
| 7. $\rightarrow$ Depth of beam.                                 | 7. $\rightarrow$ Depth of beam in span at end of beam. |

## b) T-Beams:

- |                                   |                                   |
|-----------------------------------|-----------------------------------|
| 1. $\rightarrow$ Width of flange. | 1. $\rightarrow$ Width of flange. |
| 2. $\rightarrow$ Width of web.    | 2. $\rightarrow$ Width of web.    |

## c) Beams Reinforced for Compression:

- |                                       |                                       |
|---------------------------------------|---------------------------------------|
| 1. $\rightarrow$ Unit of compression. | 1. $\rightarrow$ Unit of compression. |
| 2. $\rightarrow$ Unit of compression. | 2. $\rightarrow$ Unit of compression. |
| 3. $\rightarrow$ Unit of compression. | 3. $\rightarrow$ Unit of compression. |
| 4. $\rightarrow$ Unit of compression. | 4. $\rightarrow$ Unit of compression. |

## d) Beams Reinforced with Reinforcement:

- |                                 |                                 |
|---------------------------------|---------------------------------|
| 1. $\rightarrow$ Unit of steel. | 1. $\rightarrow$ Unit of steel. |
| 2. $\rightarrow$ Unit of steel. | 2. $\rightarrow$ Unit of steel. |
| 3. $\rightarrow$ Unit of steel. | 3. $\rightarrow$ Unit of steel. |
| 4. $\rightarrow$ Unit of steel. | 4. $\rightarrow$ Unit of steel. |

## e) Columns:

- |                                 |                                 |
|---------------------------------|---------------------------------|
| 1. $\rightarrow$ Unit of steel. | 1. $\rightarrow$ Unit of steel. |
| 2. $\rightarrow$ Unit of steel. | 2. $\rightarrow$ Unit of steel. |



## FORMULAS

The formulas which follow are for working loads and assume a straight line variation of stress to deformation of concrete in compression; tension in the concrete is neglected.

## (a) Rectangular Beams—

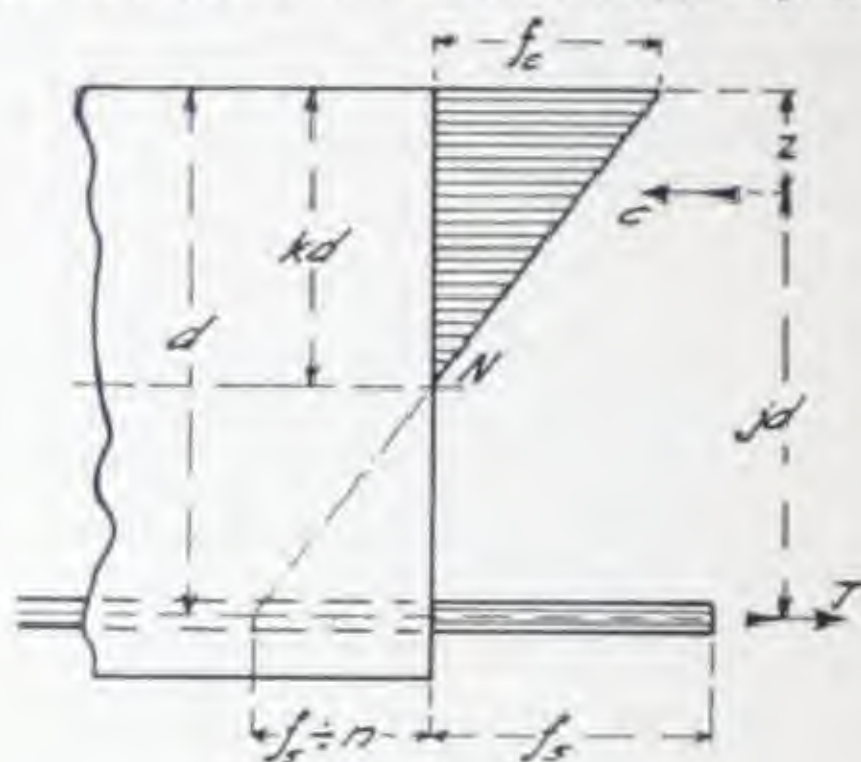
Position of neutral axis,

$$k = \sqrt{2pn + (pn)^2} - pn, \quad k = \frac{nf_c}{nf_c + f_s} \quad (1)$$

Arm of resisting couple,

$$j = 1 - \frac{1}{3}k \quad (2)$$

[For  $f_s = 15,000$  to  $16,000$  and  $f_c = 600$  to  $650$ ,  $j$  may be taken at  $\frac{7}{8}$ .]



No. 167

Fiber stresses,

$$f_s = \frac{M}{A_s j d} = \frac{M}{p j b d^2} \quad (3)$$

$$f_c = \frac{2M}{j k b d^2} \quad (4)$$

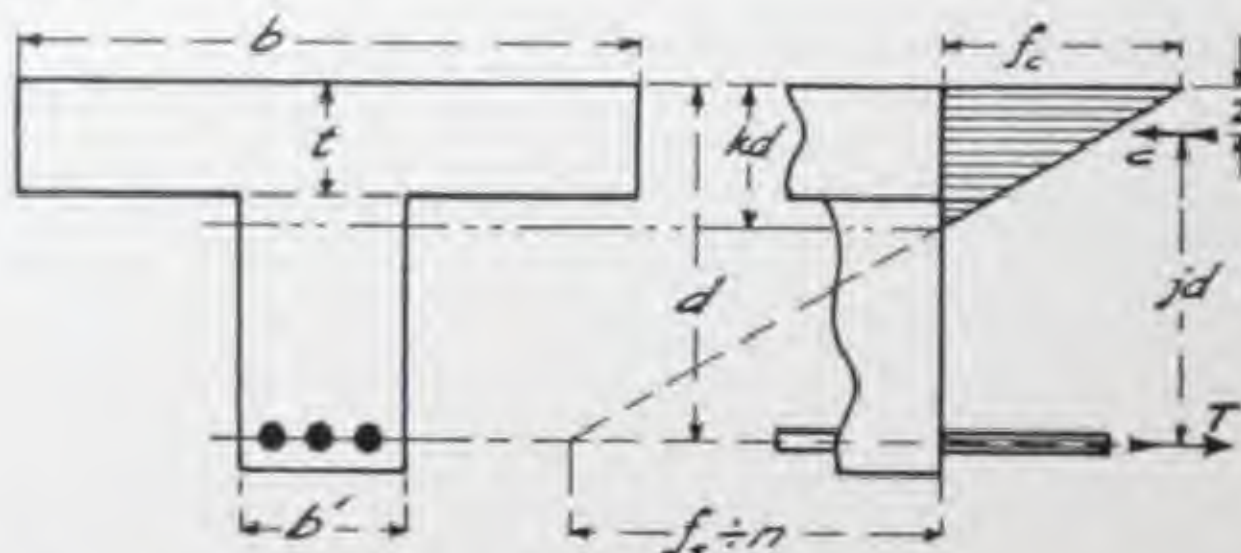
If constant  $K = \frac{1}{2} f_c k j$  or  $p f_s j$ ,

$$M = K b d^2 \quad (5)$$

Steel ratio, for balanced reinforcement,

$$p = \frac{f_s}{f_c} \left( \frac{f_s}{nf_c} + 1 \right) \quad (6)$$

## (b) T-Beams—



No. 168

CASE I. When the neutral axis lies in the flange, use the formulas for rectangular beams.



CASE II. When the neutral axis lies in the stem.

The following formulas neglect the compression in the stem.

Position of neutral axis,

$$kd = \frac{2ndA_s + bt^2}{2nA_s + 2bt} \quad (8)$$

Position of resultant compression,

$$z = \frac{3kd - 2t}{2kd - t} \cdot \frac{t}{3} \quad (9)$$

Arm of resisting couple,

$$jd = d - z. \quad (10)$$

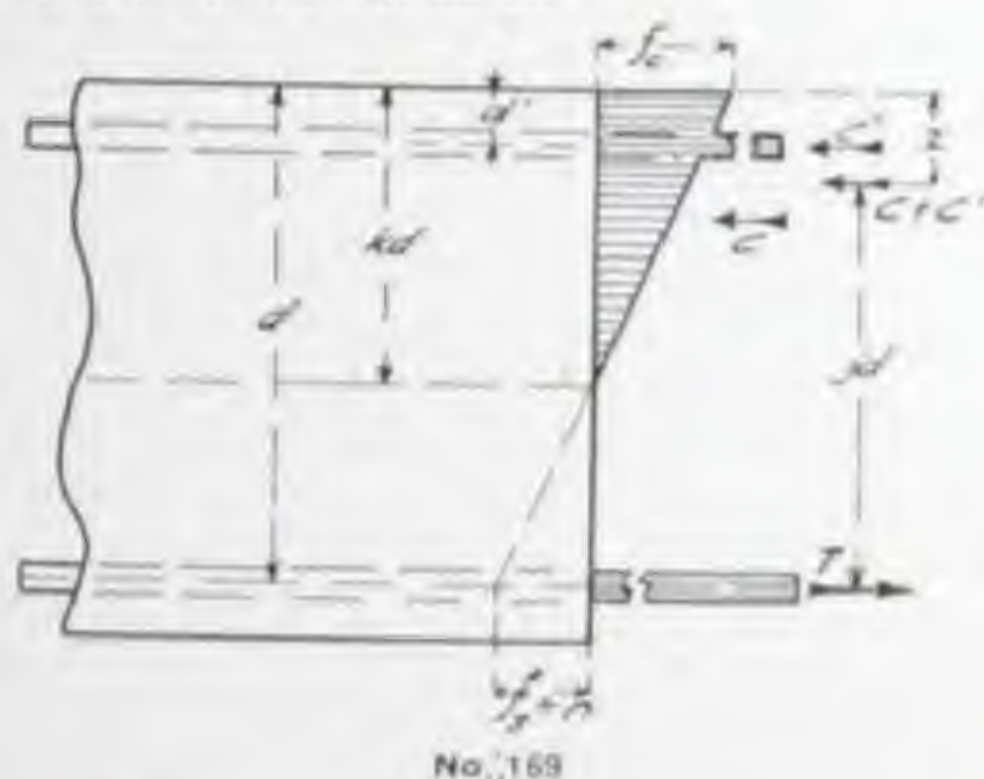
Fiber stresses,

$$f_s = \frac{M}{A_s jd} \quad (11)$$

$$f_c = \frac{Mkd}{bt(kd - \frac{1}{2}t)jd} = \frac{f_s}{n} \cdot \frac{k}{1-k} \quad (12)$$

[For approximate results, the formulas for rectangular beams may be used.]

(c) Beams Reinforced for Compression—



Position of neutral axis,

$$k = \sqrt{2n \left( p + p' \frac{d'}{d} \right) + n^2 (p + p')^2} - n(p + p') \quad (13)$$

Position of resultant compression,

$$z = \frac{\frac{1}{3}k^3d + 2p'n d' \left( k - \frac{d'}{d} \right)}{k^2 + 2p'n \left( k - \frac{d'}{d} \right)} \quad (14)$$

Arm of resisting couple,

$$jd = d - z. \quad (15)$$

Fiber stresses,

$$f_c = \frac{6M}{bd^2 \left[ 3k - k^2 + \frac{6p'n}{k} \left( k - \frac{d'}{d} \right) \left( 1 - \frac{d'}{d} \right) \right]} \quad (16)$$



$$f_s = \frac{M}{10bd^2} = n f_c \frac{1-k}{k} \quad (17)$$

$$f_s = n f_c \frac{k \frac{d^2}{k}}{k} \quad (18)$$

(d) **Shear, Bond, and Web Reinforcement**—

For rectangular beams,

$$v = \frac{V}{bd} \quad (19)$$

$$u = \frac{V}{jd \sum o} \quad (20)$$

[For approximate results,  $j$  may be taken at  $\frac{7}{8}$ .]

The stresses in web reinforcement may be estimated by means of the following formulas:

Vertical web reinforcement,

$$T_s = \frac{V_s}{j} \quad (21)$$

Bars bent up at angles between  $20^\circ$  and  $45^\circ$  with the horizontal and web members inclined at  $45^\circ$ ,

$$T_s = \frac{3}{4} \frac{V_s}{jd} \quad (22)$$

The same formulas apply to beams reinforced for compression as regards shear and bond stress for tensile steel.

For T-beams,

$$v = \frac{V}{b_d d} \quad (23)$$

$$u = \frac{V}{jd \sum o} \quad (24)$$

[For approximate results,  $j$  may be taken at  $\frac{7}{8}$ .]

(e) **Columns**—

Total side load,

$$P = f_c A_c + n A_s = f_c A [1 + (n-1)p] \quad (25)$$

Unit stress,

$$f_c = \frac{P}{A[1 + (n-1)p]} \quad (26)$$

$$f_s = n f_c \quad (27)$$

**Bending Moments.**—When the beam or slab is reinforced over its supports to take care of negative bending moments, the bending moment at the center of the span will be reduced. It is considered good practice to use the following values:

For slabs,  $M$  at center and at supports  $= \frac{1}{12} w l^2$ , where  $w$  represents the load per linear unit, and  $l$  the span length.

Beams,  $M$  at center and at supports  $= \frac{1}{12} w l^2$  for interior spans, and, for end spans,  $\frac{1}{10} w l^2$  for center and interior support for both dead and live loads.



**Working Stresses.** The following working stresses are to be used, per lb. effective area of section employed steel and cast-iron members and girth members of a 12-ft. span.

1. Steel compressive strength of members	100,000 lbs.
2. Steel tensile strength of members	100,000 lbs.
3. Steel shear strength of members	60,000 lbs.
4. Steel bearing strength of members	100,000 lbs.
5. Steel bearing strength of rivets	100,000 lbs.
6. Steel bearing strength of rivets	100,000 lbs.
7. Steel bearing strength of rivets	100,000 lbs.
8. Steel bearing strength of rivets	100,000 lbs.
9. Steel bearing strength of rivets	100,000 lbs.
10. Steel bearing strength of rivets	100,000 lbs.
11. Steel bearing strength of rivets	100,000 lbs.
12. Steel bearing strength of rivets	100,000 lbs.
13. Steel bearing strength of rivets	100,000 lbs.
14. Steel bearing strength of rivets	100,000 lbs.
15. Steel bearing strength of rivets	100,000 lbs.
16. Steel bearing strength of rivets	100,000 lbs.
17. Steel bearing strength of rivets	100,000 lbs.
18. Steel bearing strength of rivets	100,000 lbs.
19. Steel bearing strength of rivets	100,000 lbs.
20. Steel bearing strength of rivets	100,000 lbs.

Substituting in the following given the data and the stresses, the stresses in the steel will be found, and with these values the stresses in the cast-iron will be found.

$$S = \frac{P}{A} \left( 1 + \frac{e}{r^2} \right)$$

$$C = \frac{P}{A} \left( 1 - \frac{e}{r^2} \right)$$

L	Z	S				C			
		A	I	r	e	A	I	r	e
1000	100	10.0	100.0	3.16	0.0	10.0	100.0	3.16	0.0
	200	20.0	400.0	2.00	0.0	20.0	400.0	2.00	0.0
	300	30.0	900.0	1.73	0.0	30.0	900.0	1.73	0.0
	400	40.0	1600.0	1.58	0.0	40.0	1600.0	1.58	0.0
	500	50.0	2500.0	1.41	0.0	50.0	2500.0	1.41	0.0
1000	100	10.0	100.0	3.16	0.0	10.0	100.0	3.16	0.0
	200	20.0	400.0	2.00	0.0	20.0	400.0	2.00	0.0
	300	30.0	900.0	1.73	0.0	30.0	900.0	1.73	0.0
	400	40.0	1600.0	1.58	0.0	40.0	1600.0	1.58	0.0
	500	50.0	2500.0	1.41	0.0	50.0	2500.0	1.41	0.0
1000	100	10.0	100.0	3.16	0.0	10.0	100.0	3.16	0.0
	200	20.0	400.0	2.00	0.0	20.0	400.0	2.00	0.0
	300	30.0	900.0	1.73	0.0	30.0	900.0	1.73	0.0
	400	40.0	1600.0	1.58	0.0	40.0	1600.0	1.58	0.0
	500	50.0	2500.0	1.41	0.0	50.0	2500.0	1.41	0.0

**Fireproofing of Steel.** The following tables of stresses (per lb. effective area of section) are to be used.

For steel	Depth below surface of steel
1. 1/2 in. and under	100,000 lbs.
2. Between 1 1/2 in. and 2 1/2 in.	100,000 lbs.
3. 2 1/2 in. and over	100,000 lbs.
For iron	Depth below surface of steel
1. 1/2 in. and under	100,000 lbs.
2. Between 1 1/2 in. and 2 1/2 in.	100,000 lbs.
3. 2 1/2 in. and over	100,000 lbs.



The lateral spacing of parallel bars should not be less than three diameters center to center, nor should the distance from the side of the beam be less than two diameters. The clear spacing between two layers of bars should not be less than  $1\frac{1}{2}$  inches. Where more than one layer is used, at least all the bars above the lower layer should be bent up and anchored beyond the edge of the support.

**Tables of Safe Loads**—These will be found to cover fairly well the ordinary requirements. The following examples are given only to illustrate the use of the constants  $K$  and  $p$ , on page 167.

**EXAMPLE**—Given a slab of 12-ft. span, simply supported, to carry a load of 180 lbs. per sq. ft., including its own weight.

$$f_c = 700 \quad f_s = 18000 \quad n = 15$$

$$M = \frac{wl^2}{8} = \frac{(180)(12)^2(12)}{8} = 38,880 \text{ in. lb.}$$

$K$  and  $p$  may be found from the table for this combination on page 167.

$$K = \frac{M}{bd^2} = 113.1 \quad d = \sqrt{M \div bk} \quad p = 0.0072 \text{ and } A_s = pbd$$

Assuming  $b = 12$  in.,

$$d = \sqrt{38880 \div (12 \times 113.1)} = 5.34 \text{ in.}$$

$$\text{and } A_s = 0.0072 \times 12 \times 5.34 = 0.46 \text{ sq. in.}$$

Allowing for cover, the slab should be  $6\frac{1}{2}$  in. deep and the reinforcing may be  $\frac{5}{8}$ -in. round rods at  $7\frac{1}{2}$ -in. centers, which would be equivalent to 0.49 sq. in. per foot width. The weight of the slab in this case is 81 lbs., and the safe superimposed load  $= 180 - 82 = 98$  lbs. per sq. ft.

**EXAMPLE**—Design a beam of rectangular section to span 30 feet. Total uniform distributed load is 100 lbs. per lineal foot. Beam simply supported.

$$f_c = 750 \quad f_s = 18000 \quad n = 15 \quad v_c = 40$$

$$M = \frac{wl^2}{8} = \frac{(1000)(30)^2(12)}{8} = 1,350,000 \text{ in.-lb.}$$

From the table for this combination on page 167,

$$K = 125.7 \quad p = 0.008 \text{ and } A_s = pbd$$

Assuming  $b = 15$  in.,

$$d = \sqrt{1350000 \div (15 \times 125.7)} = 26.75 \text{ or, say, } 27 \text{ in.}$$

$$\text{and } A_s = 0.008 \times 15 \times 27 = 3.24 \text{ sq. in.}$$

Using three  $\frac{7}{8}$ -inch and two 1-inch round rods, the total section will be 3.38 sq. in.

$$v = \frac{15000}{(15)(\frac{7}{8})(27)} = 42 \text{ lbs.}$$

When  $v = 42$ , provision for shear is unnecessary, but for practical reasons it is advisable to use stirrups at ends.

If the two 1-inch rods are bent up at  $45^\circ$ , beginning at a point 2 ft. 6 in. from the support, a better design will result.

The three  $\frac{7}{8}$ -inch rounds remain in the bottom to develop the safe load stress.

$$\text{Bond stress } u = \frac{15000}{(8.25)(\frac{7}{8})(27)} = 77 \text{ lbs. per sq. in.}$$

This bond stress is within the safe limits and will not require special anchorage.



**Slab Design.**—Solid reinforced concrete slabs are designed by given loads by using the same formulae given for rectangular beams. A width of 12 inches is usually employed in determining the depth  $d$ , percentage  $p$ , etc. As a general rule, it is more economical to use the following values for  $f_s$  and  $f_c$ . After the point is reached beyond which the extreme fibre stress in the concrete exceeds in the design, it will be determined that the small increase in moment derived will not justify the cost of additional steel, which is added only for the purpose of lowering the neutral plane to prevent exceeding the maximum working value assigned to  $f_s$ .

For all slabs, it is advisable to use compression reinforcement  $f_{cs}$  which is bent extending perpendicular to the existing reinforcement, to prevent the slabs of cracks from shrinkage and temperature stresses, as well as to limit sag in which carrying bars can be used to preserve a given spacing.

The investigation of slabs as solid slabs is entirely necessary except in the case of heavy concentrated loads. Continuous slabs should always be provided with sufficient steel extending over the supports to take negative moments. It is customary practice to bend one-third of the bars from each opposite span, or approximately the one-length units, which gives a steel section for negative moment equal to that of the positive moment requirements at the centre of the span.

**Two-way Reinforced Slabs.**—A series of panels reinforced in two directions at right angles, and supported along four sides, should be made continuous over supports. In doing panels, the greatest length should not exceed  $l$  by more than half width. As a panel becomes oblong, the proportion of steel needed by the longer span becomes rapidly less.

Let  $x$  = proportion of total steel needed for shorter span.

$l$  = length of longer span in feet.

$b$  = breadth of panel or shorter span in feet.

$$\text{Then } x = \frac{1}{1 + \frac{l}{b}} = 0.36$$

**T-Beams.**—In calculating the strength of T-beams, advantage is taken of the floor slab, which must act as the compression flange of the member. To properly perform its function, a T-beam must be joined discontinuously with the floor slab, and the stem and flange securely tied together by means of cross ribs, stirrups and cross reinforcement from the slab. The slab should be an integral part of the beam.

The thickness of the flange is fixed by the depth of the slab, but the flange is, either side of the stem, over which compression may be assumed to act, is arbitrarily selected from the results of tests.

If T-beams are simply supported at the ends, full advantage may be taken of the flange in resisting the compressive stress, the width of flange on either side of the web being taken at not more than six times its thickness in the calculations for compressive strength. If the beam is continuous at supports, a negative moment is developed which places the flange in tension and the web in compression and the latter requires use of rectangular sections. However, as only a short section of the beam is in compression at this point, it is suggested as practicable to use a higher web concrete stress here than at the centre of the span, an increase of 15% being allowed. It is also permissible to consider the weight from the bottom of the beam as compressive reinforcement, provided they are extended sufficient distance beyond the face of the support to develop their stress in bond. It is evident that in the continuous T-beam the neutral axis should be raised on the rectangular section at the point rather than upon the T-section at the centre of the span. The web stresses and the variation in placing and curing the longitudinal reinforcement will probably be controlling factors in design.



**Web Reinforcement.**—Providing effective web reinforcement to resist diagonal tension in rectangular and T-beam sections is most essential. The intensity of the shearing stress for any point between the steel and the neutral axis is given by the formula—

$$V = \frac{V}{bjd} \text{ for rectangular beams, and } v = \frac{V}{b'jd} \text{ for T-beams.}$$

Since the value of  $j$  varies but slightly for the various percentages of steel, the ratio of  $\frac{3}{8}$  may be substituted in above, in which case—

$$v = \frac{8V}{7bd}$$

If the unit shear  $v$  exceeds 40 lbs., then stirrups must be used, even with web reinforcement;  $v$  should never exceed 120 lbs. The combination of bent rods and stirrups gives the best result. It is good design to permit the stirrups to develop the required resistance to diagonal tension and allow the bent-up rods to act only as an additional safety factor. Stirrups placed at a distance apart greater than one-half the depth of the beam are of little value.

$$v = \frac{V}{bjd} = \text{total unit shearing stress}$$

$v_1$  = unit shearing stress to be taken by concrete = 40 lbs.

$V_1$  = total shear to be taken by all stirrups in one of a beam.

$X_1$  = distance in feet from support to point beyond which stirrups are not required.

$l$  = span of beam in feet.

$A_s$  = sectional area of steel in one stirrup (2 legs for U-stirrup)

$$\text{Then } V_1 = \frac{(v-v_1)bx_1}{2} \quad (12)$$

$$X_1 = \frac{1}{2} \left( l - \frac{V_1}{v} \right)$$

$$\frac{V_1}{A_s f_s} = \text{total number of stirrups for } V_1$$

Stirrup spacing at the critical point near the bearing, assuming a given size of stirrup, will be—

$$\frac{A_s f_s}{(v-v_1)b}$$

With the distance  $x_1$ , total number of stirrups required and minimum spacing known, it will be safe to increase gradually the spacing over the distance  $x_1$  from the smallest spacing to the maximum of  $d/2$ . The number of stirrups necessary in most cases can readily be determined from the table given on page 179. For intermediate values of  $v$ , the number required can be found by interpolation. For values of  $v$  between 40 and 80, it would be well to use not less than the minimum given.

**Bond.**—Adequate bond strength should be provided. The formula given for bond stresses in beams is for straight longitudinal bars. In restrained and cantilever beams, full tensile strength exists in the reinforcing bars at the point of support and the bars should be anchored in the support sufficiently to develop this stress. Adequate bond strength throughout the length of a bar is preferable to end anchorage, but, as an additional safeguard in special cases, the ends may be hooked.



**Columns.**—It is recommended that the ratio of unsupported length to least width be limited to 15. The reinforcement consists of longitudinal bars fixed together by hoops at intervals of about 18 inches, or of longitudinal bars articulated for spiral bracing. The amount of vertical reinforcing varies from about 1% to 2% of the cross area, and of spiral bracing from 1% to 2% of the volume of the core. The point is that position of the reinforcement of the column, assumed to carry the load. The complete 1% or 2 inches of the volume of the column is not relied on for bracing and is not included in calculating for strength. If columns are eccentrically loaded, bending stresses are induced, and the reinforcement should be increased and the maximum stress close and within the working stress allowed. Formula (20) gives the total safe load for columns. Vertical loads on columns are usually applied at four points by having a sufficient distance to develop their stress in bond. Usually there are placed at the top of columns by means of details.

**Footings.**—Foundations usually require footings are of several types: (i) square or rectangular footings; (ii) circular or cylindrical footings, supporting two or more columns; (iii) spiral footings supported on piles; (iv) raft or mat footings, supporting the entire foundation area. Foundations usually require much less depth than footings of beams or plate columns, with a reinforcement varying in both quantity and arrangement. The position of a footing is to receive and distribute the load uniformly over the soil. This is accomplished in the case of the single column by placing it in the center of the footing area. Where there are two columns resting on the footing, the center of gravity of the foundation area must coincide with the center of gravity of the column loads applied to secure equilibrium of soil pressure. Having determined the position, the proportioning of the column section proceeds in accordance with the general rule though for stress and strain.



## SOLID CONCRETE SLABS

1-2-4 Mix

## SAFE LOADS IN POUNDS PER SQUARE FOOT

Including Weight of Slab

Continuous Span. Unit Stress Steel = 16,000 lbs. per sq. in., Medium Steel.

Extreme Fiber Stress Concrete = 650 lbs. per sq. in.

 $n = 15$ 

Thickness of slab, in.	Round Bars	$M (in.-lb.) = \frac{wl^2}{12} \times 12$																Weight of slab per square ft. Effective Depth, in.
		Span in Feet																
		4	5	6	7	8	9	10	11	12	13	14	15	16	17	18		
8	$3\frac{1}{4}$	323	206	143	106	80											382	
11	$5\frac{1}{4}$	504	323	224	165	126	100	80									442½	
14	$8\frac{1}{4}$	726	464	323	237	181	143	110	96	80							503	
18	$10\frac{1}{4}$	988	632	439	323	247	195	158	130	110	96						573½	
22	$12\frac{1}{4}$		826	573	421	323	255	206	170	143	122	106					634	
26	$14\frac{1}{4}$		1045	726	533	408	323	261	216	181	155	133	116	102			694½	
30	$16\frac{1}{4}$			896	658	504	397	323	266	224	191	165	143	126	111		755	
34	$18\frac{1}{4}$			1084	796	610	482	390	323	271	231	190	174	152	135	120	825½	
38	$20\frac{1}{4}$				948	726	573	464	384	323	275	237	200	181	161	143	886	
42	$22\frac{1}{4}$				1112	852	673	545	459	378	323	278	242	213	188	168	946½	
46	$24\frac{1}{4}$					988	781	632	523	439	374	323	281	247	219	195	1007	
50	$26\frac{1}{4}$					1133	896	726	600	504	429	370	323	283	251	224	1077½	
54	$28\frac{1}{4}$						1019	826	682	573	488	421	367	323	286	255	1138	
58	$30\frac{1}{4}$							1151	932	770	647	551	476	414	364	323	1198½	
62	$32\frac{1}{4}$								1045	863	726	618	533	464	408	361	1259	

Note.—This table is based on  $M = \frac{wl^2}{12}$ . Top reinforcement for negative  $M$  same area  $A_s$  as for positive  $M$  at center of span. Top steel over supports extending to  $\frac{1}{4}$  of span. For end spans, when  $M = \frac{wl^2}{10}$  use 5/6 of the values given above; for single spans, when  $M = \frac{wl^2}{8}$  use 2/3 of the above values.

To compute safe superimposed loads for spans, subtract corresponding weight of slab from the above values.



## RECTANGULAR BEAMS

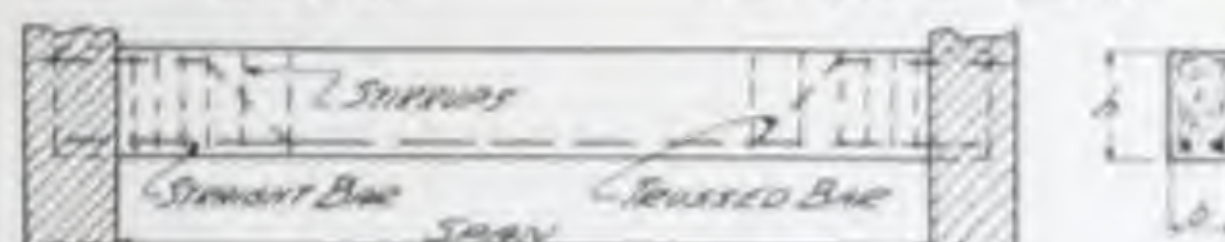
## SIMPLE SPANS

Bending Moment:

$$M = \frac{1}{8}wl^2$$

Unit Stresses:

$$f_t = 16,000 \quad f_c = 650$$



SIZE		Wt. Sectional Area, per Foot	ROUND BARS				SPAN OF BEAM IN FEET											
b,	b,		Straight		Tensioned		10	12	14	16	18	20	21	22	23	24		
In.	In.	Wt. Sectional Area, per Foot	No.	Size	No.	Size	Safe loads in Pounds per Foot Uniformly Distributed, Including Weight of Beam											
12	6	75	1	$\frac{3}{8}$	1	$\frac{1}{2}$	459	318	234	179								
	8	100	1	$\frac{3}{8}$	1	$\frac{3}{8}$	583	406	298	228								
	10	125	2	$\frac{1}{2}$	2	$\frac{1}{2}$	750	521	383	293	232							
14	8	117	1	$\frac{3}{8}$	1	$\frac{3}{8}$	849	590	433	331	262	212						
	10	146	2	$\frac{3}{8}$	1	$\frac{3}{8}$	1048	729	535	410	324	262	238					
	12	175	2	$\frac{3}{8}$	2	$\frac{3}{8}$	1315	913	671	513	406	329	298					
16	8	133	1	$\frac{3}{8}$	1	$\frac{3}{8}$	1149	799	587	450	355	288	261	238				
	10	167	1	$\frac{3}{8}$	1	$\frac{3}{8}$	1375	955	701	538	424	344	311	283				
	12	200	2	$\frac{3}{8}$	1	$\frac{3}{8}$	1724	1197	880	672	531	430	390	355				
18	8	150	1	$\frac{3}{8}$	1	$\frac{3}{8}$	1513	1050	771	591	467	378	343	312	285			
	10	188	2	$\frac{3}{8}$	2	$\frac{3}{8}$	1855	1288	946	725	573	464	421	383	350			
	12	225	2	$\frac{3}{8}$	1	$\frac{3}{8}$	2232	1550	1139	872	688	558	505	460	420	390		
	14	262	2	$\frac{3}{8}$	2	$\frac{3}{8}$	2623	1825	1341	1027	812	657	596	542	496	456		
20	8	167	1	$\frac{3}{8}$	1	$\frac{3}{8}$	1765	1225	901	690	545	442	400	364	333	306		
	10	208	2	$\frac{3}{8}$	1	$\frac{3}{8}$	2243	1560	1145	878	694	562	510	463	424	391		
	12	250	2	$\frac{3}{8}$	2	$\frac{3}{8}$	2878	1998	1468	1123	888	719	652	594	543	499		
	14	292	2	$\frac{3}{8}$	2	$\frac{3}{8}$	3364	2337	1718	1315	1040	841	763	695	635	584		
22	8	183	1	$\frac{3}{8}$	1	$\frac{3}{8}$	2252	1563	1150	880	695	563	511	465	426	391		
	10	229	1	1	1	1	2885	2003	1472	1128	890	721	655	596	545	501		
	12	275	2	$\frac{3}{8}$	2	$\frac{3}{8}$	3324	2310	1698	1300	1027	831	754	687	629	577		
	14	321	2	$\frac{3}{8}$	2	$\frac{3}{8}$	3912	2715	1995	1528	1207	977	886	808	739	679		
24	8	200	1	1	1	$\frac{3}{8}$	2800	1945	1430	1095	864	700	635	578	530	486		
	10	250	2	$\frac{3}{8}$	2	$\frac{3}{8}$	3551	2464	1812	1388	1097	887	805	734	671	616		
	12	300	2	$\frac{3}{8}$	1	1	4080	2833	2082	1595	1260	1020	925	844	772	709		
	14	350	2	$\frac{3}{8}$	2	$\frac{3}{8}$	4902	3405	2502	1915	1513	1227	1112	1013	920	851		
26	8	217	1	1	1	1	3373	2342	1720	1318	1040	843	765	697	638	585		
	10	271	2	$\frac{3}{8}$	1	1	4049	2810	2064	1580	1250	1011	918	836	765	702		
	12	325	2	$\frac{3}{8}$	2	$\frac{3}{8}$	5114	3550	2610	1996	1580	1280	1160	1057	966	888		
	14	379	2	1	2	$\frac{3}{8}$	5934	4118	3025	2317	1830	1482	1345	1225	1121	1030		
28	8	233	1	1	1	1	3807	2643	1944	1488	1176	952	864	787	720	661		
	10	292	2	$\frac{3}{8}$	1	1	4820	3350	2460	1884	1489	1205	1093	996	911	837		
	12	350	2	$\frac{3}{8}$	2	$\frac{3}{8}$	5847	4060	2980	2283	1805	1461	1325	1208	1105	1015		
	14	408	2	1	2	$\frac{3}{8}$	6722	4668	3430	2627	2077	1681	1525	1390	1271	1168		
30	10	312	2	1	1	$\frac{3}{8}$	5646	3918	2880	2261	1740	1410	1280	1167	1068	980		
	12	375	2	1	1	$\frac{3}{8}$	6705	4658	3425	2620	2070	1678	1521	1387	1268	1165		
	14	437	2	1	2	1	7976	5540	4065	3115	2460	1995	1810	1648	1508	1385		
	16	500	3	$\frac{3}{8}$	2	1	8825	6130	4500	3450	2725	2205	2000	1825	1670	1532		



## RECTANGULAR BEAMS

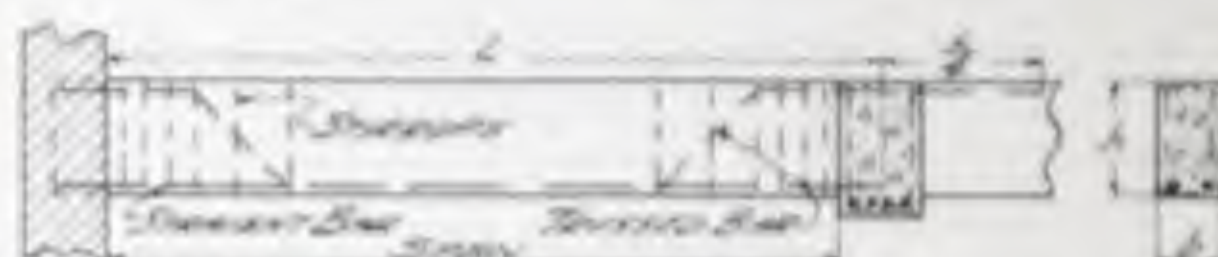
## END SPANS

Bending Moment:

Total Stresses:

$$M = \frac{1}{10}wl^2$$

$$f_c = 16,000 \quad f_t = 650$$



SIZE	d	ROUND BARS				SPAN OF BEAM IN FEET											
		Straight		Twisted		10	12	14	16	18	20	21	22	23	24		
IN.	FT.	No.	Size	No.	Size	Safe Loads in Pounds per Foot Uniformly Distributed, including Weight of Beams											
12	6	75	1	1/4	1	1/4	478	328	241	187							
	8	100	1	1/4	1	1/4	729	500	372	284	225						
	10	125	2	1/4	2	1/4	957	651	478	366	289	234	212				
14	8	117	1	1/4	1	1/4	880	611	449	344	272	220	200				
	10	140	1	1/4	1	1/4	1250	868	638	488	386	312	283	257			
	12	175	2	1/4	2	1/4	1644	1141	838	642	507	411	373	339			
16	8	133	1	1/4	1	1/4	1436	997	733	560	443	359	325	296	271		
	10	167	1	1/4	1	1/4	1836	1275	936	716	566	458	416	378	340		
	12	200	2	1/4	2	1/4	2365	1612	1139	795	628	508	461	419	384	352	
18	8	159	1	1/4	1	1/4	1671	1161	853	653	516	418	379	345	315	290	
	10	188	2	1/4	2	1/4	2319	1610	1182	905	715	580	525	478	437	401	
	12	225	2	1/4	2	1/4	2940	1925	1398	914	722	585	530	482	441	405	
	14	262	2	1/4	2	1/4	3279	2275	1672	1280	1011	820	744	677	620	569	
20	8	167	1	1/4	1	1/4	2401	1667	1225	937	741	600	544	495	454	416	
	10	208	2	1/4	2	1/4	2921	1821	1338	1024	810	655	594	541	495	454	
	12	250	2	1/4	2	1/4	3507	2500	1835	1405	1111	899	816	742	679	624	
	14	292	2	1/4	2	1/4	3752	2695	1914	1465	1158	938	850	774	708	651	
22	8	183	2	1/4	2	1/4	2888	2007	1475	1129	892	722	655	597	546	502	
	10	229	1	1	1	1	3606	2504	1841	1416	1112	901	818	745	682	626	
	12	273	2	1/4	2	1/4	4155	2887	2121	1625	1283	1040	943	859	786	722	
	14	321	2	1/4	2	1/4	5251	3630	2698	2042	1614	1308	1186	1080	993	918	
24	8	200	1	1/4	1	1/4	3169	2159	1580	1214	959	777	705	642	588	539	
	10	250	2	1/4	2	1/4	4438	3080	2263	1732	1370	1110	1006	917	839	770	
	12	300	2	1/4	2	1/4	4792	3487	2542	1990	1417	1148	1040	949	868	797	
	14	350	2	1/4	2	1/4	5327	4257	3123	2395	1891	1531	1390	1267	1159	1063	
26	8	217	1	1	1	1	4216	2925	2150	1646	1300	1052	956	871	797	732	
	10	271	2	1/4	2	1/4	4976	3455	2540	1944	1536	1244	1129	1028	940	864	
	12	325	2	1/4	2	1/4	6292	4440	3280	2465	1972	1586	1450	1323	1203	1110	
	14	379	2	1/4	2	1/4	6764	4700	3450	2642	2085	1690	1554	1408	1280	1174	
28	8	233	1	1	1	1	4759	3205	2430	1880	1470	1190	1080	984	900	829	
	10	292	2	1/4	2	1/4	5438	3767	2798	2130	1674	1357	1230	1120	1025	942	
	12	350	2	1/4	2	1/4	7308	4693	3530	2655	2157	1829	1659	1510	1382	1270	
	14	407	2	1	2	1	9518	5610	4358	3270	2540	2080	2100	1909	1800	1652	

Loads in "heavy" type should not be used unless otherwise specified.



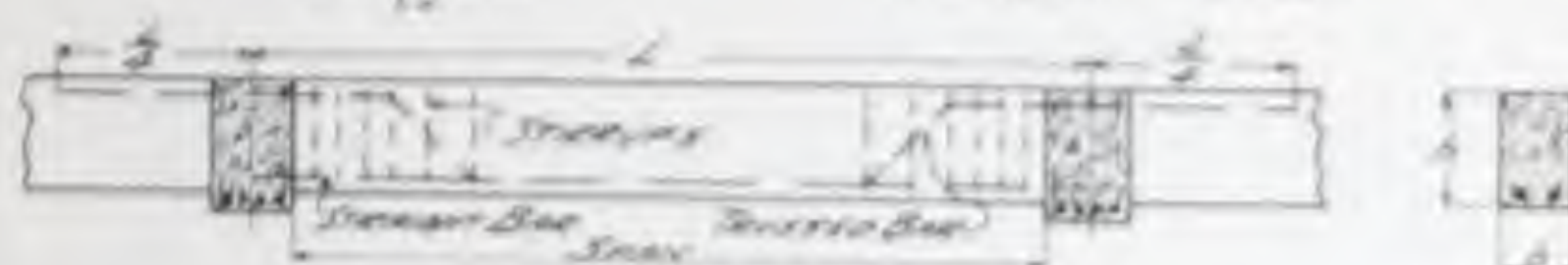
# RECTANGULAR BEAMS CONTINUOUS OVER SUPPORTS

Bending Moment:

$$M = \frac{1}{12} w l^2$$

Unit Stresses:

$$f_t = 16,000 \quad f_c = 6,500$$



SIZE		SAFE LOAD IN TONS PER FOOT	ROUND BARS		SPAN OF BEAM IN FEET									
IN.	FR.		Straight	Tressed	10	12	14	16	18	20	22	24	26	28
			No.	Size	No.	Size	Safe loads in Pounds per Foot Uniformly Distributed, Including Weight of Beam							
12	6	75	1	1/2	1	1/2	568	394	290	222				
	8	100	1	3/4	1	3/4	875	608	447	342	270	219		
	10	125	2	1	2	1	1125	781	574	440	347	281	235	
14	8	117	1	3/4	1	3/4	1056	734	539	413	326	264	240	
	10	146	1	1	1	1	1590	1040	765	585	463	375	340	309
	12	175	2	1 1/4	2	1 1/4	1973	1371	1008	771	610	493	448	407
16	8	103	1	3/4	1	3/4	1724	1195	881	674	532	431	391	356
	10	167	1	1	1	1	2203	1530	1125	861	680	551	501	455
	12	200	2	1 1/4	2	1 1/4	2442	1697	1247	955	754	610	554	504
18	8	150	1	3/4	1	3/4	2005	1391	1022	783	610	501	455	414
	10	188	2	1	2	1	2783	1932	1420	1088	859	686	631	575
	12	225	2	1 1/4	2	1 1/4	2808	1950	1433	1098	866	702	637	580
	14	262	2	1 1/2	2	1 1/2	3035	2142	1607	1215	964	792	712	652
20	8	167	1	3/4	1	3/4	2881	2003	1472	1127	890	721	654	595
	10	208	2	1	2	1	3146	2184	1605	1229	972	780	713	643
	12	250	2	1 1/4	2	1 1/4	4317	3000	2205	1689	1335	1080	982	915
	14	292	2	1 1/2	2	1 1/2	4563	3130	2300	1761	1391	1127	1022	951
22	8	183	2	1	2	1	3466	2407	1770	1355	1070	866	786	716
	10	229	1	1	1	1	4328	3005	2208	1690	1336	1082	981	904
	12	275	2	1 1/4	2	1 1/4	4695	3460	2542	1946	1538	1246	1130	1060
	14	321	2	1 1/2	2	1 1/2	6277	4357	3233	2453	1939	1570	1423	1297
24	8	200	1	3/4	1	3/4	3730	2591	1903	1457	1151	933	845	770
	10	250	2	1	2	1	5326	3704	2730	2060	1644	1331	1208	1090
	12	300	2	1 1/4	2	1 1/4	5510	3827	2812	2153	1700	1378	1250	1130
	14	350	2	1 1/2	2	1 1/2	7353	5105	3750	2873	2260	1840	1660	1520
26	8	217	1	1	1	1	5060	3517	2582	1978	1562	1265	1149	1047
	10	271	2	1 1/4	2	1 1/4	5972	4150	3047	2333	1842	1491	1355	1233
	12	325	2	1 1/2	2	1 1/2	7671	5327	3911	3000	2367	1918	1740	1586
	14	378	2	1 3/4	2	1 3/4	8114	5640	4145	3170	2505	2000	1841	1679
28	8	233	1	1	1	1	5711	3965	2915	2232	1764	1429	1296	1180
	10	292	2	1 1/4	2	1 1/4	6504	4518	3329	2540	2010	1627	1476	1344
	12	350	2	1 1/2	2	1 1/2	8770	6095	4475	3425	2710	2192	1980	1813
	14	407	2	1 3/4	2	1 3/4	11422	7940	5827	4460	3525	2858	2593	2362

Loads in "heavy" type should not be used unless otherwise specified.



## TEE BEAMS

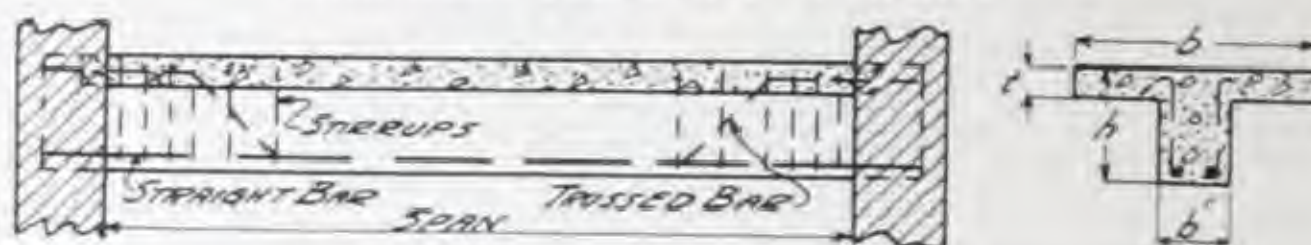
## SIMPLE SPANS

Bending Moment:

$$M = \frac{1}{8} w l^2$$

Unit Stresses:

$$f_s = 16,000 \quad f_c = 650$$

Minimum Value of  $t = 4$  Inches

SIZE			Wt., Section $\frac{1}{2}$ h, Lbs. per Foot	ROUND BARS				SPAN OF BEAM IN FEET									
h	b*	b		Straight		Trussed		10	12	14	16	18	20	22	24	25	26
				No.	Size	No.	Size										
In.	In.	In.		Safe Loads in Pounds per Foot Uniformly Distributed, Including Weight of Beam													
12	6	18	75	1	1	1	$\frac{7}{8}$	1295	900	660	506						
	8	23	100	1	$1\frac{1}{8}$	1	1	1664	1156	849	650						
	10	31	125	2	1	1	1	2195	1525	1120	856						
14	8	24	117	1	$1\frac{1}{4}$	1	$1\frac{1}{8}$	2463	1711	1257	963	761	616				
	10	28	146	2	1	1	$1\frac{1}{8}$	2875	1995	1467	1122	886	718				
	12	36	175	2	$1\frac{1}{8}$	1	$1\frac{1}{4}$	3580	2485	1828	1398	1105	895				
16	8	25	133	2	$\frac{7}{8}$	2	$\frac{7}{8}$	2954	2052	1508	1153	912	738				
	10	32	167	2	1	2	1	3794	2635	1936	1482	1171	948				
	12	36	200	3	1	2	$\frac{7}{8}$	4430	3077	2260	1731	1368	1108				
18	8	26	150	2	1	2	$\frac{7}{8}$		2717	1997	1530	1208	978	808	679		
	10	33	188	2	$1\frac{1}{8}$	2	1		3453	2538	1943	1535	1244	1028	864		
	12	40	225	3	1	2	$1\frac{1}{8}$		4219	3097	2372	1874	1519	1254	1054		
20	8	27	167	2	1	2	1		3458	2541	1945	1537	1245	1028	864	797	737
	10	34	208	3	1	2	1		4380	3220	2463	1947	1577	1302	1094	1008	932
	12	41	250	3	1	3	1		5187	3811	2918	2305	1867	1543	1297	1195	1105
SPAN OF BEAM IN FEET																	
								20	22	24	26	28	30	32	34	36	38
22	8	20	183	2	$2\frac{1}{8}$	2	1	1580	1305	1097	934	806	702				
	10	36	229	3	1	2	$1\frac{1}{8}$	1929	1594	1340	1140	984	857				
	12	44	275	3	$1\frac{1}{8}$	3	1	2367	1957	1645	1400	1208	1052				
24	10	37	250	3	1	3	1	2308	1908	1602	1367	1178	1026	901			
	12	47	300	3	$1\frac{1}{8}$	3	$1\frac{1}{4}$	2895	2391	2009	1712	1475	1286	1130			
26	10	40	271	3	$1\frac{1}{8}$	3	1	2867	2369	1991	1696	1463	1274	1119	992		
	12	47	325	3	$1\frac{1}{4}$	2	$1\frac{1}{4}$	3293	2721	2287	1948	1680	1462	1285	1140		
28	10	44	292	3	$1\frac{1}{8}$	3	$1\frac{1}{8}$				2041	1758	1532	1347	1192	1064	954
	12	49	350	3	$1\frac{1}{4}$	3	$1\frac{1}{8}$				2290	1975	1720	1512	1339	1195	1072
	14	59	408	4	$1\frac{1}{8}$	4	$1\frac{1}{8}$				2728	2352	2050	1800	1596	1424	1277
30	10	44	312	3	$1\frac{1}{4}$	2	$1\frac{1}{4}$				2287	1970	1718	1509	1338	1193	1070
	12	55	375	4	$1\frac{1}{8}$	3	$1\frac{1}{4}$				2832	2442	2127	1870	1657	1477	1326
	14	64	437	4	$1\frac{1}{4}$	4	$1\frac{1}{8}$				3290	2836	2470	2172	1923	1717	1540

Loads in "heavy" type should not be used unless stirrups are provided.



TEE BEAMS  
END SPANS

Bending Moment:

$$M = \frac{1}{10} w l^2$$

Load Intensity:

$$L = 10,000 \quad L = 600$$



H20	L	F	S	BENT END BAY		SPAN OF BEAM IN FEET							
				Neutral	Flange	10	12	14	16	18	20	22	24
H20	L	F	S	No. and Size		See Loading Table for Free End Bay							
				No. and Size		See Loading Table for Free End Bay							
12	8	75	1-1/2	1-1/2	1-1/2	700	807	822	873				
	8	100	1-1/2	1-1/2	1-1/2	1040	1067	1112	1163				
	10	125	1-1/2	1-1/2	1-1/2	1340	1367	1412	1463				
	12	150	2-1/2	2-1/2	2-1/2	1600	1712	1714	1767				
14	8	80	1-1/2	1-1/2	1-1/2	1200	1218	1212	1219	1211			
	8	117	1-1/2	1-1/2	1-1/2	1620	1625	1627	1622	1626			
	10	150	1-1/2	1-1/2	1-1/2	2000	2012	2012	2012	2012			
	12	175	2-1/2	2-1/2	2-1/2	2400	2412	2412	2412	2412			
16	8	100	1-1/2	1-1/2	1-1/2	1800	1812	1812	1812	1812			
	8	133	1-1/2	1-1/2	1-1/2	2372	2387	2387	2387	2387			
	10	167	2-1/2	2-1/2	2-1/2	2817	2827	2827	2827	2827			
	12	200	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	3200	3212	3212	3212	3212			
18	8	120	1-1/2	1-1/2	1-1/2	2000	2012	2012	2012	2012			
	8	160	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	2600	2612	2612	2612	2612			
	10	200	2-1/2	2-1/2	2-1/2	3200	3212	3212	3212	3212			
	12	240	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	3800	3812	3812	3812	3812			
20	8	140	1-1/2	1-1/2	1-1/2	2200	2212	2212	2212	2212			
	8	180	2-1/2	2-1/2	2-1/2	2800	2812	2812	2812	2812			
	10	220	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	3400	3412	3412	3412	3412			
	12	260	2-1/2	2-1/2	2-1/2	4000	4012	4012	4012	4012			
22	8	160	1-1/2	1-1/2	1-1/2	2400	2412	2412	2412	2412			
	8	200	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	3000	3012	3012	3012	3012			
	10	240	2-1/2	2-1/2	2-1/2	3600	3612	3612	3612	3612			
	12	280	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	4200	4212	4212	4212	4212			
24	8	180	1-1/2	1-1/2	1-1/2	2600	2612	2612	2612	2612			
	8	220	2-1/2	2-1/2	2-1/2	3200	3212	3212	3212	3212			
	10	260	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	3800	3812	3812	3812	3812			
	12	300	2-1/2	2-1/2	2-1/2	4400	4412	4412	4412	4412			
26	8	200	1-1/2	1-1/2	1-1/2	2800	2812	2812	2812	2812			
	8	240	2-1/2	2-1/2	2-1/2	3400	3412	3412	3412	3412			
	10	280	1-1/2 + 1-1/2	1-1/2 + 1-1/2	1-1/2 + 1-1/2	4000	4012	4012	4012	4012			
	12	320	2-1/2	2-1/2	2-1/2	4600	4612	4612	4612	4612			

Load on "Heavy" type should not be used where average only is required.



## TEE BEAMS

## CONTINUOUS OVER SUPPORTS

Bending Moment:

$$M = \frac{1}{12} w l^2$$

Unit Stresses:

$$f_s = 16,000 \quad f_c = 650$$



SIZE		ROUND BARS		SPAN OF BEAM IN FEET							
$A_s$	$W_s$			10	12	14	16	18	20	22	24
lb.	lb.	No. and Size	No. and Size	Safe loads in Pounds per Foot, Uniformly Distributed, Including Weight of Beam							
12	6 75	1- $\frac{3}{4}$	1- $\frac{3}{4}$	840	584	429	328				
	8 100	1- $\frac{3}{4}$	1- $\frac{3}{4}$	1203	830	614	470				
	10 125	1- $\frac{3}{4}$	1- $\frac{3}{4}$	1612	1120	824	630				
	12 150	2- $\frac{3}{4}$	2- $\frac{3}{4}$	1680	1167	857	656				
14	6 88	1- $\frac{3}{4}$	1- $\frac{3}{4}$	1442	1001	735	564	445			
	8 117	1- $\frac{3}{4}$	1- $\frac{3}{4}$	1944	1350	992	759	600			
	10 146	1-1	1-1	2473	1719	1262	966	764			
	12 175	2- $\frac{3}{4}$	2- $\frac{3}{4}$	2884	2004	1472	1127	890			
16	6 100	1- $\frac{3}{4}$	1- $\frac{3}{4}$	2161	1501	1102	844	667	540		
	8 133	1-1	1-1	2846	1976	1452	1111	878	712		
	10 167	2- $\frac{3}{4}$	2- $\frac{3}{4}$	3381	2348	1725	1321	1044	845		
	12 200	1- $\frac{3}{4}$ + 1- $\frac{3}{4}$	1- $\frac{3}{4}$ + 1- $\frac{3}{4}$	4027	2790	2054	1573	1243	1006		
18	8 150	1-1	1-1	2412	1772	1357	1072	868	718	603	
	10 188	1- $\frac{3}{4}$ + 1- $\frac{3}{4}$	1- $\frac{3}{4}$ + 1- $\frac{3}{4}$	3173	2331	1787	1411	1142	944	793	
	12 225	2- $\frac{3}{4}$	2- $\frac{3}{4}$	3686	2708	2074	1638	1327	1097	922	
	14 262	1-1 + 1- $\frac{3}{4}$	1-1 + 1- $\frac{3}{4}$	4285	3147	2410	1904	1542	1275	1071	
20	8 167	1-1 $\frac{1}{2}$	1-1 $\frac{1}{2}$		2460	1883	1490	1206	996	837	
	10 208	2- $\frac{3}{4}$	2- $\frac{3}{4}$		3012	2308	1822	1476	1220	1025	
	12 250	1-1 + 1- $\frac{3}{4}$	1-1 + 1- $\frac{3}{4}$		3555	2725	2152	1742	1440	1210	
	14 292	2-1	2-1		4025	3080	2435	1972	1630	1370	
				SPAN OF BEAM IN FEET							
				16	18	20	22	24	26	28	30
22	8 183	1-1 $\frac{1}{2}$	1-1 $\frac{1}{2}$	2172	1716	1300	1140	965	823	709	
	10 229	1-1 + 1- $\frac{3}{4}$	1-1 + 1- $\frac{3}{4}$	2937	2320	1879	1552	1305	1111	960	
	12 275	2-1	2-1	3450	2725	2306	1824	1533	1306	1127	
	14 321	3- $\frac{3}{4}$	3- $\frac{3}{4}$	3955	3125	2531	2092	1758	1498	1291	
24	10 250	1-1 + 1- $\frac{3}{4}$	1-1 + 1- $\frac{3}{4}$	2652	2147	1775	1492	1271	1096	955	
	12 300	3- $\frac{3}{4}$	3- $\frac{3}{4}$	3375	2733	2259	1898	1617	1395	1216	
	14 350	2-1 $\frac{1}{2}$	2-1 $\frac{1}{2}$	3800	3078	2544	2137	1821	1570	1368	
	16 400	3-1	3-1	4455	3610	2980	2505	2134	1840	1603	
26	10 271	2-1	2-1	2660	2198	1849	1574	1358	1182		
	12 325	2-1 $\frac{1}{2}$	2-1 $\frac{1}{2}$	3290	2718	2283	1945	1678	1461		
	14 375	1-1 $\frac{1}{2}$ + 1-1 $\frac{1}{2}$	1-1 $\frac{1}{2}$ + 1-1 $\frac{1}{2}$	3740	3080	2545	2211	1907	1661		
	16 433	2-1 + 2- $\frac{3}{4}$	2-1 + 2- $\frac{3}{4}$	4493	3713	3120	2658	2262	1997		

Beams in "heavy" type should not be used unless stresses are provided.



# STIRRUP REINFORCEMENT FOR UNIFORMLY LOADED BEAMS

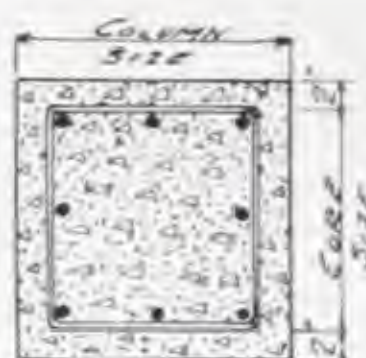
Unit Stress,  $f_c$  $f_c = 16,000$  $v = 40$ 

NOTE.—The table gives total number of stirrups per beam. Place one-half the number at each end of beam, as shown.

Clear Span of Beam, Feet	Number and Size of Round Bar U-Stirrups							
	End Shear = 80 Lbs. per Sq. In.				End Shear = 100 Lbs. per Sq. In.			
	Width of Beam, In.				Width of Beam, In.			
	8	10	12	14	8	10	12	14
10	6½	8½	10½	10½	12½	6½	8½	10½
12	8½	10½	12½	12½	6½	8½	10½	10½
14	10½	12½	14½	10½	8½	10½	10½	12½
16	10½	12½	8½	8½	8½	10½	12½	14½
18	12½	14½	8½	8½	10½	12½	14½	16½
20	12½	16½	8½	10½	10½	12½	16½	18½
22	14½	18½	10½	10½	12½	14½	16½	20½
24	16½	18½	10½	12½	12½	16½	18½	22½
26	16½	20½	12½	12½	14½	16½	20½	22½
28	18½	22½	12½	14½	14½	18½	20½	24½
30	18½	24½	12½	14½	16½	18½	22½	26½

Clear Span of Beam, Feet	Number and Size of Round Bar U-Stirrups							
	End Shear = 120 Lbs. per Sq. In.				End Shear = 140 Lbs. per Sq. In.			
	Width of Beam, In.				Width of Beam, In.			
	8	10	12	14	8	10	12	14
10	8½	10½	12½	14½	10½	12½	14½	16½
12	10½	12½	14½	16½	12½	14½	16½	18½
14	10½	14½	16½	18½	14½	16½	18½	20½
16	12½	14½	18½	12½	16½	20½	14½	16½
18	14½	16½	20½	14½	18½	22½	16½	18½
20	16½	18½	22½	16½	20½	24½	18½	20½
22	16½	20½	24½	16½	22½	26½	18½	22½
24	18½	22½	26½	18½	24½	28½	20½	24½
26	20½	24½	28½	20½	26½	30½	22½	26½
28	20½	26½	30½	20½	28½	32½	24½	28½
30	22½	28½	32½	22½	30½	34½	26½	30½





## SQUARE TIED COLUMNS

### SAFE AXIAL LOADS IN THOUSANDS OF POUNDS

Ratio of Length of Column to its Side, Limited to 15

Column Size, In.	Core Size, In.	ROUND BAR TIES		ROUND BAR VERTICALS		1: 2: 4 Concrete $f_c = 500$ lbs. per sq. in. $n = 15$	1: 1½: 3 Concrete $f_c = 600$ lbs. per sq. in. $n = 12$
		Size, In.	Spacing In.	No.	Size		
12	8	¼	7	4	½	38	44
		¼	9	4	⅝	41	46
		¼	11	4	¾	44	50
		¼	12	4	⅞	49	54
14	10	¼	9	4	⅝	59	68
		¼	11	4	¾	62	72
		¼	12	4	⅞	67	76
		¼	12	4	1	72	81
		¼	12	4	1⅛	78	86
16	12	¼	11	4	¾	84	98
		¼	12	4	⅞	89	102
		¼	12	4	1	94	107
		¼	12	4	1⅛	100	113
		¼	12	6	1⅛	114	126
18	14	¼	12	4	1	120	139
		¼	12	6	⅞	123	142
		¼	12	6	1⅛	140	158
		¼	12	8	1⅛	154	171
20	16	¼	12	6	⅞	153	177
		¼	12	8	⅞	162	185
		¼	12	8	1⅛	184	206
		¼	12	10	1⅛	197	219
22	18	¼	12	6	1	195	226
		¼	12	8	1	206	236
		¼	12	8	1¼	231	259
		¼	12	12	1⅛	245	273
24	20	¼	12	6	1⅛	242	279
		¼	12	10	1	255	292
		¼	12	12	1⅛	284	319
		¼	12	16	1⅛	311	345
26	22	¼	12	10	1	297	342
		¼	12	12	1	308	353
		¼	12	14	1⅛	340	382
		¼	12	18	1⅛	367	409
28	24	¼	12	12	1	354	408
		¼	12	14	1	365	418
		¼	12	18	1⅛	413	463
		¼	12	22	1⅛	441	490
30	26	¼	12	12	1	404	468
		¼	12	14	1⅛	435	497
		¼	12	20	1⅛	477	537
		¼	12	22	1¼	527	584





### SPIRAL COLUMNS

#### SAFE AXIAL LOADS IN THOUSANDS OF POUNDS

Ratio of Length of Column to its Side or Diameter,  
Limited to 15.

Column Diam., In.	Core Diam., In.	Round Bar Verti- cals		1: 2: 4 Concrete $f_c = 500$ lbs. per sq. in. $n = 15$		1: 1½: 3 Concrete $f_c = 600$ lbs. per sq. in. $n = 12$	
		$\frac{Z}{N}$	$\frac{Z}{N}$				
16	12	4	¾	¾" dia. - 2" pitch	¾" dia. - 1 ½" pitch	¾" dia. - 2" pitch	¾" dia. - 1 ½" pitch
		4	⅞	104	128	115	139
		4	1	109	133	119	143
		7	⅞	114	138	124	148
18	14	5	¾	¾" dia. - 1 ½" pitch	¾" dia. - 2 ¼" pitch	¾" dia. - 1 ½" pitch	¾" dia. - 2 ¼" pitch
		5	⅞	139	173	154	188
		6	1	145	179	159	193
		8	1	157	191	170	204
20	16	7	¾	¾" dia. - 2 ½" pitch	¾" dia. - 1 ½" pitch	¾" dia. - 2 ½" pitch	¾" dia. - 1 ½" pitch
		7	⅞	182	233	200	252
		8	1	189	241	208	259
		10	1	204	255	222	273
22	18	9	¾	¾" dia. - 2 ¾" pitch	¾" dia. - 2 ¾" pitch	¾" dia. - 2 ¾" pitch	¾" dia. - 2 ¾" pitch
		9	⅞	229	294	253	317
		10	1	239	304	263	327
		12	1	256	321	279	343
24	20	10	¾	¾" dia. - 2" pitch	¾" dia. - 2 ¼" pitch	¾" dia. - 2" pitch	¾" dia. - 2 ¼" pitch
		10	⅞	281	350	311	380
		12	1	292	361	321	390
		12	1 ⅛	316	385	344	413
26	22	10	¾	¾" dia. - 2 ½" pitch	¾" dia. - 2" pitch	¾" dia. - 2 ½" pitch	¾" dia. - 2" pitch
		10	⅞	332	419	368	455
		11	1	346	433	382	468
		13	1 ⅛	359	446	394	481
28	24	10	¾	¾" dia. - 2 ¾" pitch	¾" dia. - 2 ¾" pitch	¾" dia. - 2 ¾" pitch	¾" dia. - 2 ¾" pitch
		10	⅞	395	496	438	540
		12	1	419	520	461	562
		14	1 ⅛	430	531	471	572
30	26	10	¾	¾" dia. - 2 ¼" pitch	¾" dia. - 2 ¼" pitch	¾" dia. - 2 ¼" pitch	¾" dia. - 2 ¼" pitch
		10	⅞	467	581	518	632
		12	1	480	594	530	644
		14	1 ⅛	508	623	556	671
32	28	10	¾	¾" dia. - 2 ½" pitch	¾" dia. - 2 ½" pitch	¾" dia. - 2 ½" pitch	¾" dia. - 2 ½" pitch
		10	⅞	536	651	583	697
		12	1	571	685	615	730
		14	1 ⅛				

NOTE.—Size and pitch of spiral wire given at head of group of loads for each size column.



## SQUARE COLUMN FOOTINGS

Unit Stresses:

$f_s = 16,000$

$f_c = 650$



L		Soil Value, Lbs. per Sq. Ft.	Column Load in 1000 Lbs.	Minimum Column Diam., In.	h		b		Reinforcement Round Bars Each Way		Weight of Steel, Lbs.	Volume of Con- crete Cu. Ft.
Ft.	In.				Ft.	In.	Ft.	In.	No.	Size		
5	0	4000	96	13	0	7	1	10	14	$\frac{1}{2}$	88.8	23.7
5	0	6000	145	16	0	8	2	3	16	$\frac{1}{2}$	100.3	29.3
5	6	4000	116	14	0	8	2	1	14	$\frac{1}{2}$	97.0	33.3
5	6	6000	175	17	0	10	2	6	15	$\frac{1}{2}$	104.0	44.3
6	0	4000	137	15	0	9	2	3	14	$\frac{1}{2}$	106.3	44.5
6	0	6000	207	18	0	11	2	9	16	$\frac{1}{2}$	121.4	58.2
6	6	4000	161	16	0	9	2	4	17	$\frac{1}{2}$	140.3	51.6
6	6	6000	242	19	1	0	2	10	17	$\frac{1}{2}$	140.3	73.2
7	0	4000	186	17	0	10	2	6	17	$\frac{1}{2}$	151.5	66.2
7	0	6000	280	20	1	1	3	1	18	$\frac{1}{2}$	160.4	92.3
7	6	4000	212	18	0	11	2	9	18	$\frac{1}{2}$	172.3	84.3
7	6	6000	322	22	1	1	3	3	20	$\frac{1}{2}$	191.4	105.2
8	0	4000	240	19	1	0	2	10	18	$\frac{1}{2}$	184.1	103.6
8	0	6000	363	22	1	3	3	6	20	$\frac{1}{2}$	204.6	138.7
8	6	4000	272	20	1	0	2	11	21	$\frac{1}{2}$	228.7	116.0
8	6	6000	410	24	1	3	3	8	23	$\frac{1}{2}$	250.5	155.8
9	0	4000	303	21	1	1	3	2	21	$\frac{1}{2}$	242.6	141.8
9	0	6000	456	24	1	5	3	11	22	$\frac{1}{2}$	254.1	198.5
9	6	4000	333	21	1	3	3	5	16	$\frac{5}{8}$	310.8	183.4
9	6	6000	506	25	1	6	4	1	18	$\frac{5}{8}$	349.7	233.2
10	0	4000	370	22	1	3	3	6	17	$\frac{5}{8}$	384.1	201.7
10	0	6000	559	26	1	7	4	3	19	$\frac{5}{8}$	389.0	271.0
10	6	4000	405	23	1	4	3	8	18	$\frac{5}{8}$	387.5	237.0
10	6	6000	614	28	1	8	4	7	19	$\frac{5}{8}$	409.0	318.5
11	0	4000	442	24	1	5	3	11	18	$\frac{5}{8}$	406.4	277.8
11	0	6000	671	28	1	9	4	8	20	$\frac{5}{8}$	451.5	363.0
11	6	4000	484	25	1	5	4	0	20	$\frac{5}{8}$	472.5	301.8
11	6	6000	731	30	1	10	4	1	21	$\frac{5}{8}$	496.1	416.8
12	0	4000	524	26	1	6	4	2	22	$\frac{5}{8}$	542.9	347.8
12	0	6000	792	31	1	11	5	2	22	$\frac{5}{8}$	542.9	475.9
12	6	4000	566	26	1	7	4	3	23	$\frac{5}{8}$	591.7	396.0
12	6	6000	857	32	2	0	5	4	22	$\frac{5}{8}$	566.0	537.0



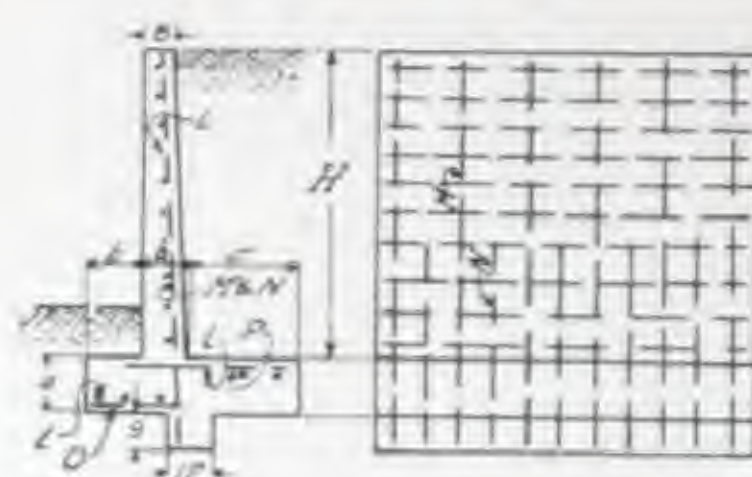
## COMBINED COLUMN FOOTINGS

 $A_s$  = Tension steel in top $A'_s$  = Transverse steel under column  $P_1$  $A''_s$  = Transverse steel under column  $P_2$  $l$  = Distance  $c_1$  to  $c_2$  of columns in feet

Unit Stresses:  
 $f_s = 16,000$   
 $f_c = 650$

$P_1 + P_2$ Lbs.	$\frac{P_1}{P_2}$	$\frac{l_c}{Ft.}$	Steel Value = 4,000 lbs. per square foot						Steel Value = 5,000 pounds per square foot					
			$\frac{B}{Ft.}$	$\frac{H}{Ft.}$	$\frac{h}{Ft.}$	$\frac{A_s}{Sq. In.}$	$\frac{A'_s}{Sq. In.}$	$\frac{A''_s}{Sq. In.}$	$\frac{B}{Ft.}$	$\frac{H}{Ft.}$	$\frac{h}{Ft.}$	$\frac{A_s}{Sq. In.}$	$\frac{A'_s}{Sq. In.}$	$\frac{A''_s}{Sq. In.}$
300,000	1.2	1.09/ + 2c	71/1	0.17/ + 0.25	1	12.9	638/2	532/2	58/1	0.19/ + 0.25	1	11.6	456/2	380/2
	1.3	1.13/ + 2c	71/1	0.17/ + 0.25	2.3-	12.4	630/2	485/2	56/1	0.19/ + 0.25	2.1-	11.1	455/2	350/2
	1.4	1.17/ + 2c	69/1	0.16/ + 0.25	6	12.4	680/2	480/2	54/1	0.18/ + 0.25	6	11.0	476/2	340/2
	1.5	1.20/ + 2c	67/1	0.16/ + 0.25		11.7	670/2	450/2	53/1	0.18/ + 0.25		10.4	482/2	322/2
	1.2	1.09/ + 2c	98/1	0.17/ + 0.25		17.4	1121/2	935/2	77/1	0.19/ + 0.25		15.6	805/2	671/2
400,000	1.3	1.13/ + 2c	96/1	0.17/ + 0.25	1	16.2	1142/2	895/2	75/1	0.19/ + 0.25	1	14.5	817/2	628/2
	1.4	1.17/ + 2c	93/1	0.16/ + 0.25	2.8-	16.2	1225/2	875/2	73/1	0.18/ + 0.25	2.6-	14.5	871/2	622/2
	1.5	1.20/ + 2c	90/1	0.16/ + 0.25	6	15.5	1200/2	810/2	71/1	0.18/ + 0.25	6	13.8	867/2	578/2
	1.2	1.09/ + 2c	122/1	0.17/ + 0.25		21.4	1734/2	1446/2	96/1	0.19/ + 0.25		19.2	1249/2	1041/2
	1.3	1.13/ + 2c	119/1	0.17/ + 0.25	1	20.0	1710/2	1420/2	94/1	0.19/ + 0.25	1	17.9	1283/2	987/2
500,000	1.4	1.17/ + 2c	115/1	0.16/ + 0.25	3.2-	20.0	1870/2	1340/2	91/1	0.18/ + 0.25	3.0-	17.9	1357/2	966/2
	1.5	1.20/ + 2c	111/1	0.16/ + 0.25	6	19.3	1840/2	1220/2	88/1	0.18/ + 0.25	6	17.2	1330/2	887/2
	1.2	1.09/ + 2c	146/1	0.17/ + 0.25		25.8	2480/2	2070/2	115/1	0.19/ + 0.25		23.1	1794/2	1494/2
	1.3	1.13/ + 2c	141/1	0.17/ + 0.25	1	24.4	2397/2	2000/2	111/1	0.19/ + 0.25	1	21.9	1788/2	1375/2
	1.4	1.17/ + 2c	136/1	0.16/ + 0.25	3.6-	24.4	2620/2	1870/2	107/1	0.18/ + 0.25	3.3-	21.9	1867/2	1333/2
600,000	1.5	1.20/ + 2c	133/1	0.16/ + 0.25	6	23.1	2630/2	1760/2	105/1	0.18/ + 0.25	6	20.6	1894/2	1263/2
	1.2	1.09/ + 2c	169/1	0.17/ + 0.25		29.9	3330/2	2770/2	133/1	0.19/ + 0.25		26.8	2390/2	1996/2
	1.3	1.13/ + 2c	164/1	0.17/ + 0.25	1	27.9	3240/2	2705/2	129/1	0.19/ + 0.25	1	25.0	2420/2	1860/2
	1.4	1.17/ + 2c	159/1	0.16/ + 0.25	3.9-	28.0	3580/2	2550/2	125/1	0.18/ + 0.25	3.6-	24.9	2555/2	1820/2
	1.5	1.20/ + 2c	155/1	0.16/ + 0.25	6	26.4	3500/2	2380/2	122/1	0.18/ + 0.25	6	23.5	2555/2	1703/2





### CANTILEVER RETAINING WALLS

Surface of Earth Horizontal

Angle of Repose,  $33^\circ$

Weight of earth, 100 lbs. per cu. ft.

$f_s = 16,000$  lbs. per sq. in.

$f_c = 650$  lbs. per sq. in.

$n = 15$

#### CONCRETE

Height of Wall H, Feet	a	b	c	Soil Pressure at Toe, Lbs. per sq. ft.	Soil Pressure at Heel, Lbs. per sq. ft.	Concrete per ft. Length of Wall, Cubic Feet
7	1' 0"	1' 0"	1' 10"	1460	90	10.41
8	1' 1"	1' 1"	2' 1"	1470	270	12.35
9	1' 1"	1' 2"	2' 9"	1770	130	14.04
10	1' 2"	1' 4"	2' 10"	2000	60	16.14
11	1' 2"	1' 6"	3' 2"	2100	90	17.65
12	1' 3"	1' 8"	3' 7"	2210	160	20.37
13	1' 4"	1' 8"	4' 0"	2480	120	23.10
14	1' 4"	2' 1"	4' 3"	2400	240	24.95
15	1' 5"	2' 1"	4' 7"	2680	200	27.79
16	1' 5"	2' 2"	4' 11"	2870	170	29.45
17	1' 6"	2' 3"	5' 3"	3060	160	32.65
18	1' 7"	2' 4"	5' 7"	3280	140	36.00
19	1' 7"	2' 6"	6' 1"	3350	230	38.25
20	1' 8"	2' 8"	6' 6"	3430	310	42.13

#### REINFORCEMENT

Bars in all Cases of Round Section.

Height of Wall H in Feet	M Bars			N Bars			O Bars			P Bars			L Bars			Wt. per Ft. Length of Wall
	Size	Spacing in In.	Length	Size	Spacing in In.	Length	Size	Spacing in In.	Length	Size	Spacing in In.	Length	No.	Size	Spacing in In.	
7	$\frac{1}{2}$	24	8' 6"	$\frac{1}{2}$	24	3' 0"	$\frac{3}{4}$	12	12' 2"	$\frac{3}{4}$	12	3' 0"	12	$\frac{1}{2}$	12	14.4
8	$\frac{1}{2}$	24	9' 0"	$\frac{1}{2}$	24	4' 3"	$\frac{3}{4}$	12	12' 2"	$\frac{3}{4}$	12	3' 3"	13	$\frac{1}{2}$	12	15.7
9	$\frac{1}{2}$	17	10' 6"	$\frac{1}{2}$	17	4' 9"	$\frac{3}{4}$	12	12' 2"	$11\frac{1}{2}$	$\frac{3}{4}$	4' 3"	15	$\frac{1}{2}$	12	21.3
10	$\frac{1}{2}$	21	11' 9"	$\frac{1}{2}$	21	5' 0"	$\frac{3}{4}$	10	12' 2"	$9\frac{1}{2}$	$\frac{3}{4}$	4' 6"	16	$\frac{1}{2}$	12	26.2
11	$\frac{3}{4}$	16	12' 0"	$\frac{3}{4}$	16	5' 3"	$\frac{3}{4}$	$7\frac{1}{2}$	12' 2"	8	$\frac{3}{4}$	4' 9"	17	$\frac{3}{4}$	12	32.3
12	$\frac{3}{4}$	20	14' 3"	$\frac{3}{4}$	20	6' 3"	$\frac{3}{4}$	11	12' 2"	10	$\frac{3}{4}$	5' 0"	20	$\frac{3}{4}$	12	41.8
13	$\frac{3}{4}$	10	15' 3"	$\frac{3}{4}$	16	6' 6"	$\frac{3}{4}$	$10\frac{1}{2}$	12' 2"	12	$\frac{3}{4}$	6' 6"	22	$\frac{3}{4}$	12	63.4
14	$\frac{3}{4}$	13	16' 3"	$\frac{3}{4}$	13	6' 9"	$\frac{3}{4}$	11	12' 2"	10	$\frac{3}{4}$	6' 9"	24	$\frac{3}{4}$	12	75.4
15	$\frac{3}{4}$	16	17' 6"	$\frac{3}{4}$	16	7' 3"	$\frac{3}{4}$	10	12' 2"	11	$\frac{3}{4}$	7' 6"	26	$\frac{3}{4}$	12	88.9
16	$\frac{3}{4}$	13	18' 0"	$\frac{3}{4}$	13	7' 3"	$\frac{3}{4}$	9	12' 2"	$9\frac{1}{2}$	$\frac{3}{4}$	7' 9"	27	$\frac{3}{4}$	12	103.2
17	1	15	19' 6"	1	15	8' 0"	$\frac{3}{4}$	$8\frac{1}{2}$	12' 2"	8	$\frac{3}{4}$	8' 0"	29	$\frac{3}{4}$	12	122.2
18	1	13	20' 6"	1	13	8' 3"	$\frac{3}{4}$	$7\frac{1}{2}$	12' 2"	$7\frac{1}{2}$	$\frac{3}{4}$	8' 6"	30	$\frac{3}{4}$	12	130.8
19	$1\frac{1}{4}$	14	21' 6"	$1\frac{1}{4}$	14	8' 9"	$\frac{3}{4}$	9	12' 2"	$7\frac{1}{2}$	$\frac{3}{4}$	9' 3"	33	$\frac{3}{4}$	12	174.7
20	$1\frac{1}{4}$	13	22' 6"	$1\frac{1}{4}$	13	9' 0"	$\frac{3}{4}$	$8\frac{1}{2}$	12' 2"	7	$\frac{3}{4}$	9' 9"	34	$\frac{3}{4}$	12	192.9

Hooks are required at lower end of M and N bars for walls over 11' 0" in height.



**BIRMINGHAM WIRE GAUGE**  
**EQUIVALENTS IN INCHES**  
**CORRESPONDING WEIGHTS OF FLAT ROLLED STEEL**

Gauge Number	Thickness, Inches	Pounds per Square Foot	Thickness, Inches		Pounds per Square Foot
			Fractional	Decimal	
0000	.454	18.5232	1/2	.5	20.4
000	.425	17.34	15/32	.46875	19.125
00	.380	15.504	7/16	.4375	17.85
0	.340	13.872	13/32	.40625	16.575
1	.300	12.24	3/8	.375	15.3
2	.284	11.5872	11/32	.34375	14.025
3	.259	10.5672	5/16	.3125	12.75
4	.238	9.7104	19/64	.296875	12.1125
5	.220	8.976	9/32	.28125	11.475
6	.203	8.2824	17/64	.265625	10.8375
7	.180	7.344	1/4	.25	10.2
8	.165	6.732	15/64	.234375	9.5625
9	.148	6.0384	7/32	.21875	8.925
10	.134	5.4672	13/64	.203125	8.2875
11	.120	4.896	3/16	.1875	7.65
12	.109	4.4472	11/64	.171875	7.0125
13	.095	3.876	5/32	.15625	6.375
14	.083	3.3864	9/64	.140625	5.7375
15	.072	2.9376	1/8	.125	5.1
16	.065	2.652	7/64	.109375	4.4625
17	.058	2.3664	3/32	.09375	3.825
18	.049	1.9992	5/64	.078125	3.1875
19	.042	1.7136	1/16	.0625	2.55
20	.035	1.428	3/64	.046875	1.9125
21	.032	1.3056			
22	.028	1.1424	1/32	.03125	1.275
23	.025	1.02			
24	.022	0.8976			
25	.020	0.816			
26	.018	0.7344			
27	.016	0.6528			
28	.014	0.5712	1/64	.015625	0.6375
29	.013	0.5304			
30	.012	0.4896			
31	.010	0.408			
32	.009	0.3672			
33	.008	0.3264	1/128	.0078125	0.31875
34	.007	0.2856			
35	.005	0.2040			
36	.004	0.1632	1/256	.00390625	0.159375



### UNITED STATES STANDARD GAUGE FOR SHEET AND PLATE IRON AND STEEL

The United States Standard Gauge is a weight gauge based upon the weights per square foot in ounces avoirdupois and approximate thickness based upon 480 pounds per cubic foot. In the practical use and application of the United States Standard Gauge, a weight variation of 2½ per cent either way may be allowed.

Gauge Number	Approximate Thickness		Weight per Square Foot, Ounces, Avoirdupois	Weight per Square Foot, Pounds, Avoirdupois
	Fractional Inches	Decimal Inches		
0000000	1/2	5	320	20 00
000000	15/32	46875	300	18 75
00000	7/16	4375	280	17 50
0000	13/32	40625	260	16 25
000	3/8	375	240	15 00
00	11/32	34375	220	13 75
0	5/16	3125	200	12 50
1	9/32	28125	180	11 25
2	17/64	265625	170	10 625
3	1/4	25	160	10 00
4	15/64	234375	150	9 375
5	7/32	21875	140	8 75
6	13/64	203125	130	8 125
7	3/16	1875	120	7 50
8	11/64	171875	110	6 875
9	5/32	15625	100	6 25
10	9/64	140625	90	5 625
11	1/8	125	80	5 00
12	7/64	109375	70	4 375
13	3/32	09375	60	3 75
14	5/64	078125	50	3 125
15	9/128	0703125	45	2 8125
16	1/16	0625	40	2 50
17	9/160	05625	36	2 25
18	1/20	05	32	2 00
19	7/160	04375	28	1 75
20	3/80	0375	24	1 50
21	11/320	034375	22	1 375
22	1/32	03125	20	1 25
23	9/320	028125	18	1 125
24	1/40	025	16	1 00
25	7/320	021875	14	875
26	3/160	01875	12	75
27	11/640	0171875	11	6875
28	1/64	015625	10	625
29	9/640	0140625	9	5625
30	1/80	0125	8	50
31	7/640	0109375	7	4375
32	13/1280	01015625	6½	40625
33	3/320	009375	6	375
34	11/1280	00859375	5½	34375
35	5/640	0078125	5	3125
36	9/1280	00703125	4½	28125
37	17/2560	006640625	4¼	265625
38	1/160	00625	4	25



## CONTENTS OF STORAGE WAREHOUSES

Material	Weights per Cubic Foot of Space, Pounds	Height of Pile, Feet	Weights per Square Foot of Floor, Pounds	Recommended Live Loads, Pounds per Square Foot
<b>Groceries</b>				
Canned Goods, in cases	58	6	348	
Coffee, Roasted, in bags	33	8	264	
Flour, in barrels	40	5	200	
Molasses, in barrels	48	5	240	
Rice, in bags	58	6	348	
Salt, in bags	70	5	350	250 to 300
Soap Powder, in cases	38	8	304	
Starch, in barrels	25	6	150	
Sugar, in barrels	43	5	215	
" in cases	51	6	306	
Tea, in chests	25	8	200	
<b>Dry Goods, Cotton, Wool, Etc.</b>				
Cotton, in bales, compressed	18	8	144	
Cotton Bleached Goods, in cases	28	8	224	
Cotton Flannel, in cases	12	8	96	
Cotton Sheetting, in cases	23	8	184	
Cotton Yarn, in cases	25	8	200	
Linen Goods, in cases	30	8	240	200 to 250
Sisal, compressed	21	8	168	
Tow, compressed	29	8	232	
Wool, in bales, compressed	48	5	240	
" " " not compressed	13	8	104	
" worsted, in cases	27	8	216	
<b>Building Materials</b>				
Cement, Natural	50	6	354	
" Portland	73	6	438	300 to 400
Lime and Plaster	53	5	265	
<b>Hardware, Etc.</b>				
Door Checks	45			
Hinges	64			
Locks, in cases, packed	31			
Nail Fasteners	48			300 to 400
Screws	101			
Sheet Tin, in boxes	278	2	556	
Wire Cables, on reels			425	
Wire, Galvanized Iron, in coils	74	4½	362	
<b>Drugs, Paints, Oil, Etc.</b>				
Bleaching Powder, in hogsheads	31	3½	102	
Linseed Oil, in barrels	36	6	216	
Rosin, in barrels	48	6	288	
Shellac, Gum	38	6	228	
Soda, Caustic, in iron drums	88	3-1/3	294	200 to 300
Sulphuric Acid	60	1-2/3	100	
White Lead Paste, in cans	174	3½	610	
White Lead, dry	86	4½	408	
Red Lead and Litharge, dry	132	3¾	495	
<b>Miscellaneous</b>				
Glass and Chinaware, in crates	40	8	320	
Hides and Leather, in bales	20	8	160	
Paper, Newspaper, and Strawboards	35	6	210	
Paper, Writing and Calendered	60	6	360	300
Rope, in coils	32	6	192	



## SPECIFIC GRAVITIES AND WEIGHTS

Substance	Specific Gravity	Weight, Pounds per Cu. Ft.	Substance	Specific Gravity	Weight, Pounds per Cu. Ft.
<b>Metals, Alloys, Ores</b>			<b>Various Liquids (Cont.)</b>		
Aluminum, cast (annealed)	2.55-2.75	165	Acids, nitric 70%	1.50	94
Aluminum, bronze	7.7	481	" sulphuric 87%	1.80	112
Brass, cast (rolled)	8.4-8.7	524	Oil, vegetable	0.91-0.94	56
Brass, 70 to 14% Zn	7.4-8.9	459	" mineral, lubricants	0.90-0.93	55
Copper, cast (rolled)	8.8-9.0	556	Water, 4°C, max. density	1.0	62.428
" ore, pyrites	4.1-4.3	254	" 100°C	0.9584	59.840
Gold, cast (annealed)	19.25-19.35	1205	" ice	0.89-0.92	55
Iron, cast (pig)	7.2	450	" snow, fresh fallen	1.05	65
" wrought	7.8-7.9	485	" sea water	1.02-1.03	64
" steel	7.8-7.9	485			
" ferro-silicon	6.5-7.3	407	<b>Ashlar Masonry</b>		
" ore, hematite	5.2	325	Granite, granite, green	2.3-2.6	145
" " magnetite	4.9-5.2	315	Limestone, marble	2.3-2.8	140
" slag	2.5-3.0	152	Sandstone, limestone	2.1-2.4	130
Lead	11.37	710			
Manganese	7.2-8.0	455	<b>Mortar Rubble Masonry</b>		
Mercury	13.6	849	Granite, granite, green	2.2-2.8	135
Nickel	8.8-9.0	556	Limestone, marble	2.2-2.8	130
" fused metal	8.8-9.0	556	Sandstone, limestone	2.0-2.3	120
Platinum, cast (annealed)	21.3-21.5	1330			
Silver, cast (annealed)	10.4-10.6	656	<b>Dry Rubble Masonry</b>		
Tin, cast (annealed)	7.2-7.5	450	Granite, granite, green	1.9-2.3	120
Zinc, cast (rolled)	6.9-7.2	435	Limestone, marble	1.9-2.1	115
			Sandstone, limestone	1.8-1.9	110
<b>Various Solids</b>			<b>Brick Masonry</b>		
Carrots, with roots		50	Pressed brick	2.0-2.4	140
" barley		35	Common brick	1.9-2.3	135
" corn, dry		45	Soft brick	1.5-1.7	100
" wheat		45			
Hay and straw, loose		20	<b>Concrete Masonry</b>		
Carbon, flux, heavy	1.82-1.90	112	Concrete, stone, sand	2.2-2.4	140
Flax	0.80-0.82	50	" slag, etc.	1.9-2.3	130
Flax, loose	0.40-0.50	25	" gravel, etc.	1.5-1.7	100
Flax, pressed	2.40-2.60	150			
Flaxseed	0.80-1.00	50	<b>Various Building Mats</b>		
Flaxseed oil	0.75-1.12	45	Asph. concrete		40-45
Flaxseed	0.80-0.90	50	Concrete, portland, loose		90
Flax, ground, oil, pressed		45	" set	2.2-2.3	140
Flaxseed	1.02	65	Flax, gypsum, loose		20-25
Flaxseed	1.02-1.05	65	Mortar, wet	1.4-1.5	85
Flaxseed	1.02	65	Flag, brick, dry		40-75
Flaxseed	1.02	65	" screenings		50-125
Flaxseed	1.02	65	" surface, dry		80
Flaxseed	1.02	65	" slag, wet		40-50
Flaxseed	1.02	65			
Flaxseed	1.02	65	<b>Earth, etc., Excavated</b>		
Flaxseed	1.02	65	Flax, dry		40
Flaxseed	1.02	65	" damp, loose		100
Flaxseed	1.02	65	Flax and gravel, dry		100
Flaxseed	1.02	65	Flax, dry, loose		70
Flaxseed	1.02	65	" packed		80
Flaxseed	1.02	65	" loose, loose		70
Flaxseed	1.02	65	" packed		80
Flaxseed	1.02	65	" rock, flowing		100
Flaxseed	1.02	65	" packed		100
Flaxseed	1.02	65	Gravel, limestone		40-45
Flaxseed	1.02	65	" sandstone		40
Flaxseed	1.02	65	" shale		100
Flaxseed	1.02	65	Sand, gravel, dry, loose		40-100
Flaxseed	1.02	65	" packed		100-120
Flaxseed	1.02	65	" wet		120-130
<b>Various Liquids</b>					
Alcohol, 100%	0.79	49			
Acetic acid, 40%	1.05	65			

The specific gravities of solids and liquids refer to water at 4°C. Those of gases to air at 0°C and 760 mm. pressure. The weights per cubic foot are derived from average specific gravities, except where stated that weights are for bulk, based on loose material, etc.



## SPECIFIC GRAVITIES AND WEIGHTS

Substance	Specific Gravity	Weight, Pounds per Cu. Ft.	Substance	Specific Gravity	Weight, Pounds per Cu. Ft.
<b>Excavations in Water</b>			<b>Stone, Quarried, Piled (Cont.)</b>		
Sand or gravel and clay		60	Shale		92
Clay		65	Gneiss, hornblende		107
River mud		80	<b>Bituminous Substances</b>		
Soil		70	Asphaltum	1.1-1.5	81
Stone flag		65	Coal, anthracite	1.4-1.7	97
<b>Minerals</b>			" bituminous	1.2-1.5	84
Asbestos	2.1-2.8	133	" lignite	1.1-1.4	78
Basalt	2.7-3.2	164	" peat, turf, dry	0.65-0.85	47
Bauxite	1.7-1.8	109	" charcoal, pine	0.28-0.34	23
Clay, hard	1.8-2.0	117	" " oak	0.47-0.57	33
Dolomite	2.8	181	" coke	1.0-1.4	75
Granite, syenite	2.5-3.1	175	Graphite	1.9-2.3	131
Gypsum, alabaster	2.3-2.4	159	Paraffine	0.87-0.91	56
Limestone, marble	2.3-2.8	165	Petroleum	0.87	54
Magnetite	3.0	187	" refined	0.79-0.82	50
Pumice, natural	0.37-0.90	40	" kerosene	0.73-0.75	46
Quartz, flint	2.3-2.8	165	" gasoline	0.66-0.69	42
Sandstone, bluestone	2.2-2.5	147	Pitch	1.07-1.15	69
Shale, slate	2.7-2.9	175	Tar, bituminous	1.20	75
Southern, talc	2.6-2.8	169	<b>Coal and Coke, Piled</b>		
<b>Stone, Quarried, Piled</b>			Coal, anthracite		47-54
Basalt, granite, gneiss		96	" bituminous, lignite		40-54
Limestone, marble, quartz		95	" peat, turf		30-39
Sandstone		82	" charcoal		10-14
			" coke		23-32

The specific gravities of solids and liquids refer to water at 4°C., those of gases to air at 0°C. and 760 mm. pressure. The weights per cubic foot are derived from average specific gravities except where stated that weights are for bulk, heaped or loose material, etc.



## STRENGTH OF MATERIALS

STRESSES IN THOUSANDS OF POUNDS PER SQUARE INCH

Metals and Alloys	Stresses					Modulus of Elasticity, Pounds	Elongation, %
	Tension, Ultimate	Elastic Limit	Compression Ultimate	Bending, Ultimate	Shearing Ultimate		
Aluminum, cast	15	6.5	12		12	11,000,000	
bars, sheets	24-28	12-14					
Aluminum Bronze,							
5% to 7½% Al	75	40	120				
10% Al	85-100	60					
Brass, cast, common	18-24	6	30	20	36	9,000,000	
wire, hard	80						
" annealed	50	16				14,000,000	
Bronze—							
Gun Metal, 9 Cu, 1 Sn	25-55	10		52		10,000,000	
Manganese, cast 10% Sn	60	30	125				
" rolled 2% Mn	100	80					
Phosphorus, cast 9% Sn	50	24					
" wire 1% P	100						
Bronze Tobin, cast—							
38% Zn	66						
(1½% Sn	80	40				4,500,000	
1/3% Pb	100						
Copper, cast	25	6	40	22	30	10,000,000	
plates, rods, bolts	32-35	10	32				
wire, annealed	36	10				15,000,000	
Delta Metal, cast—							
55-60% Cu	45						
38-40% Zn	68						
2-4% Fe	85						
1-2% Sn	100						
German Silver, 25% Zn, 20% Ni							
Iron, see next page							
Lead, cast	1.8					1,000,000	
pipe, wire	2.2-2.5					1,000,000	
rolled sheets	3.3					720,000	
Tin, cast	3.5-4.6	1.5-1.8	6	4		4,000,000	
antimony, 10 Sn, 1 Sb	11						
Zinc, cast	4-6	4	18	7		13,000,000	
rolled sheets	7-16						
<b>Steel</b>							
Shapes, Plates, Bars*							
bridges	55-65	½ tens	tensile	tensile	¾ tens	29,000,000	27.3-23.0
buildings	55-65	"	"	"	"	29,000,000	25.4-21.3
cars	50-65	"	"	"	"	29,000,000	30.0-23.0
locomotives	55-65	"	"	"	"	29,000,000	27.3-23.0
ships	58-68	"	"	"	"	29,000,000	25.9-22.1
Boiler Plates*							
fire box	55-65	½ tens	tensile	tensile	¾ tens	29,000,000	27.3-23.0
flange plates	52-62	"	"	"	"	29,000,000	28.8-24.2
Rivets*							
boilers	45-55	½ tens	tensile	tensile	¾ tens	29,000,000	33.3-27.3
bridges	46-56	"	"	"	"	29,000,000	32.6-26.8
buildings	46-56	"	"	"	"	29,000,000	30.4-25.0
cars	48-58	"	"	"	"	29,000,000	31.3-25.9
ships	55-65	"	"	"	"	29,000,000	27.3-23.0
Concrete Bars*							
plain, structural grade	55-70	33	tensile	tensile	¾ tens	29,000,000	25.4-20.0
" intermediate	70-85	40	"	"	"	29,000,000	18.6-15.3
" hard	80	50	"	"	"	29,000,000	15.0
deformed, struc'l grade	55-70	33	"	"	"	29,000,000	22.7-17.9
" intermediate	70-85	40	"	"	"	29,000,000	16.1-13.2
" hard	80	50	"	"	"	29,000,000	12.5
cold twisted		55	"	"	"	29,000,000	5.0
Castings*							
soft	60	27	tensile	tensile	¾ tens	29,000,000	22.0
medium	70	31.5	"	"	"	29,000,000	18.0
hard	80	36	"	"	"	29,000,000	15.0
Forgings*							

\*See Specifications of the Society of Testing Materials.



## STRENGTH OF MATERIALS

STRESSES IN THOUSANDS OF POUNDS PER SQUARE INCH

Metals and Alloys	Stresses					Modulus of Elasticity, Pounds	Elongation, %
	Tension, Ultimate	Elastic Limit	Compression, Ultimate	Bending, Ultimate	Shearing, Ultimate		
<b>Steel Alloys</b>							
Nickel Steel,* 3.25% Ni							
" shapes, plates, bars	85-100	50	tensile	tensile	$\frac{5}{8}$ tens	29,000,000	17.5-15.0
" rivets	70-80	45	"	"	"	29,000,000	21.4-18.8
" eye bars, unannealed	95-110	55	"	"	"	29,000,000	15.8-13.6
" " annealed	85-105	52	"	"	"	29,000,000	20.0
Copper Steel, 0.50% Cu	60-68	37-38	"	"	"	29,000,000	29.0-25.0
<b>Steel Springs and Wire</b>							
Springs, untempered	65-110	40-70					
Wire, unannealed	120	60					
" annealed	80	40					
" bridge cable	200	95					
<b>Wrought Iron</b>							
Shapes	48	26	tensile	tensile	$\frac{3}{8}$ tens	28,000,000	
Bars	50	27	"	"	"	28,000,000	
Wire, unannealed	80					15,000,000	
" annealed	60	27				25,000,000	
<b>Cast Iron</b>							
Common	15-18	8	80	30	15-20	12,000,000	
Gray	18-24			25-30			
Malleable	27-35	15-20	46	30	40		

## STRESSES IN POUNDS PER SQUARE INCH

Building Materials	Ultimate Average Stresses			Modulus of Elasticity	Safe Working Stresses		
	Compression	Tension	Bending		Compression	Bending	Shearing
<b>Stone</b>							
Blue Stone	12,000	1,200	2,500	7,000,000	1,200	1,200	300
Granite, gneiss	12,000	1,200	1,000	7,000,000	1,200	1,200	300
Limestone, marble	8,000	800	1,500	7,000,000	800	800	150
Sandstone	5,000	500	1,200	3,000,000	500	500	150
Slate	10,000	3,000	5,000	14,000,000	1,000	1,000	175
<b>Brick</b>							
Common, good	10,000	200					
" medium burned	11,000						
" hard burned	15,000						
Pressed and paving	6,000						
<b>Cement, Portland</b>							
Neat, 28 days	7,040	740					
" 90 days	7,350	740					
1:3 Sand, 28 days	1,200	320					
" 90 days	1,400	340					
<b>Masonry</b>							
Granite					135	600	
Limestone, bluestone					550	500	
Sandstone					280	400	
Rubble					140	250	
" coursed					168	240	
Concrete, P.C., 1:2:4					550	500	
" " 1:2½:5					280	300	
Brick, common					168	300	
" hard burned					210	300	
<b>Miscellaneous</b>							
Glass, common	30,000	3,000	3,000	8,000,000			
" flooring	10,000	3,000	3,000				
Plaster	700	70					
Terra-cotta	5,000						
Ropes, cast steel hoisting		80,000					
" standing, derrick		70,000					
" cables		8,000					
Bells, solid woven, cotton		7,000					
" Bar		9,000					

\*See Specifications of the Society of Testing Materials.



## EXPANSION OF BODIES BY HEAT

The linear coefficient of expansion of a body is the rate at which the unit of length changes, under constant pressure, with an increase of unit or one degree of temperature; the square surface coefficient of expansion is, approximately, two times, and the cubical or volumetric coefficient three times the linear coefficient of expansion. A bar, if not fixed, undergoes a change in length =  $ltn$ , where  $l$  is the length of the bar in inches,  $t$  the number of degrees,  $n$  the corresponding linear coefficient; if fixed at both ends, the internal stress per unit of area =  $tnE$ , pounds per square inch, where  $E$  is the modulus of elasticity, and the total temperature stress =  $AtnE$ , pounds, where  $A$  is the cross section of the bar in square inches.

To find the increase of a bar due to an increase in temperature, from the table, multiply the length of the bar by the increase in degrees and by the coefficient for 100 degrees, and divide by 100.

COEFFICIENTS OF EXPANSION FOR 100 DEGREES = 100n

Substance	Linear Expansion		Substance	Linear Expansion	
	Centigrade	Fahrenheit		Centigrade	Fahrenheit
<b>Metals and Alloys</b>			<b>Stone and Masonry</b>		
Aluminum, wrought	.00231	.00128	Ashlar masonry	.00063	.00035
Brass	.00188	.00104	Brick masonry	.00055	.00031
" wire	.00193	.00107	Cement, Portland	.00107	.00059
Bronze	.00181	.00101	Concrete	.00143	.00079
Copper	.00168	.00093	" masonry	.00120	.00067
German Silver	.00183	.00102	Granite	.00084	.00047
Gold	.00150	.00083	Limestone	.00080	.00044
Iron, cast, gray	.00106	.00059	Marble	.00100	.00056
" wrought	.00120	.00067	Plaster	.00166	.00092
" wire	.00124	.00069	Rubble masonry	.00063	.00035
Lead	.00286	.00159	Sandstone	.00110	.00061
Nickel	.00126	.00070	Slate	.00104	.00058
Platinum	.00090	.00050	<b>Timber</b>		
Platinum-Iridium, 15% Ir	.00081	.00045	Fir	.00037	.00021
Silver	.00192	.00107	Maple parallel to	.00064	.00036
Steel, cast	.00110	.00061	Oak fibre	.00049	.00027
" hard	.00132	.00073	Pine	.00054	.00030
" medium	.00120	.00067	Fir	.00058	.00032
" soft	.00110	.00061	Maple perpendicular	.00048	.00027
Tin	.00210	.00117	Oak to fiber	.00054	.00030
Zinc, rolled	.00311	.00173	Pine	.00034	.00019
<b>Miscellaneous Solids</b>			<b>Liquid Substances</b>		
Glass	.00085	.00047	Alcohol	.104	.058
Graphite	.00079	.00044	Acid, nitric	.110	.061
Gutta-percha	.05980	.03322	" sulphuric	.063	.035
Paraffin	.02785	.01547	Mercury	.018	.010
Porcelain	.00036	.00020	Oil, turpentine	.090	.050

EXPANSION OF WATER, MAXIMUM DENSITY = 1

C°	Volume	C°	Volume	C°	Volume	C°	Volume	C°	Volume	C°	Volume
0	1.000126	10	1.000257	30	1.004234	50	1.011877	70	1.022384	90	1.035829
4	1.000000	20	1.001732	40	1.007627	60	1.016954	80	1.029003	100	1.043116



## DECIMALS OF AN INCH AND OF A FOOT

Fractions of Inch or Foot		Each Equivalent Inch to Foot Fractions	Fractions of Inch or Foot		Each Equivalent Inch to Foot Fractions	Fractions of Inch or Foot		Each Equivalent Inch to Foot Fractions	Fractions of Inch or Foot		Each Equivalent Inch to Foot Fractions
64ths			64ths			64ths			64ths		
	0052	$\frac{1}{16}$		2552	$\frac{4}{16}$		5052	$\frac{8}{16}$		7552	$\frac{12}{16}$
	0104	$\frac{2}{16}$		2604	$\frac{4\frac{1}{4}}{16}$		5104	$\frac{8\frac{1}{4}}{16}$		7604	$\frac{12\frac{1}{4}}{16}$
1	015625	$\frac{1}{64}$	17	265625	$\frac{3\frac{1}{8}}{64}$	33	515625	$\frac{8\frac{1}{8}}{64}$	49	765625	$\frac{12\frac{1}{8}}{64}$
	0208	$\frac{1}{32}$		2708	$\frac{3\frac{1}{4}}{32}$		5208	$\frac{8\frac{1}{4}}{32}$		7708	$\frac{12\frac{1}{4}}{32}$
	0260	$\frac{1}{16}$		2760	$\frac{3\frac{1}{2}}{16}$		5260	$\frac{8\frac{1}{2}}{16}$			
2	03125	$\frac{1}{32}$	18	28125	$\frac{4\frac{1}{8}}{32}$	34	53125	$\frac{8\frac{1}{8}}{32}$	50	78125	$\frac{12\frac{1}{8}}{32}$
	0365	$\frac{1}{16}$		2865	$\frac{4\frac{1}{4}}{16}$		5365	$\frac{8\frac{1}{4}}{16}$		7865	$\frac{12\frac{1}{4}}{16}$
	0417	$\frac{1}{8}$		2917	$\frac{4\frac{1}{2}}{8}$		5417	$\frac{8\frac{1}{2}}{8}$		7917	$\frac{12\frac{1}{2}}{8}$
3	046875	$\frac{3}{64}$	19	296875	$\frac{3\frac{3}{8}}{64}$	35	546875	$\frac{8\frac{3}{8}}{64}$	51	796875	$\frac{12\frac{3}{8}}{64}$
	0521	$\frac{1}{32}$		3021	$\frac{3\frac{1}{4}}{32}$		5521	$\frac{8\frac{1}{4}}{32}$		8021	$\frac{12\frac{1}{4}}{32}$
	0573	$\frac{1}{16}$		3073	$\frac{3\frac{1}{2}}{16}$		5573	$\frac{8\frac{1}{2}}{16}$		8073	$\frac{12\frac{1}{2}}{16}$
4	0625	$\frac{1}{16}$	20	3125	$\frac{3}{8}$	36	5625	$\frac{9}{32}$	52	8125	$\frac{9}{16}$
	0677	$\frac{1}{8}$		3177	$\frac{3\frac{1}{4}}{8}$		5677	$\frac{9\frac{1}{4}}{8}$		8177	$\frac{9\frac{1}{4}}{8}$
	0729	$\frac{1}{4}$		3229	$\frac{3\frac{1}{2}}{4}$		5729	$\frac{9\frac{1}{2}}{4}$		8229	$\frac{9\frac{1}{2}}{4}$
5	078125	$\frac{1}{8}$	21	328125	$\frac{3\frac{3}{8}}{8}$	37	578125	$\frac{9\frac{3}{8}}{8}$	53	828125	$\frac{9\frac{3}{8}}{8}$
	0833	$\frac{1}{4}$		3333	$\frac{4}{4}$		5833	$\frac{9\frac{1}{2}}{4}$		8333	$\frac{10}{4}$
	0885	$\frac{1}{2}$		3385	$\frac{4\frac{1}{4}}{4}$		5885	$\frac{9\frac{1}{4}}{4}$		8385	$\frac{10\frac{1}{4}}{4}$
6	09375	$\frac{1}{4}$	22	34375	$\frac{4\frac{1}{8}}{8}$	38	59375	$\frac{9\frac{1}{8}}{8}$	54	84375	$\frac{10\frac{1}{8}}{8}$
	0990	$\frac{1}{2}$		3490	$\frac{4\frac{1}{4}}{2}$		5990	$\frac{9\frac{1}{4}}{2}$		8490	$\frac{10\frac{1}{4}}{2}$
	1042	$\frac{1}{2}$		3542	$\frac{4\frac{1}{2}}{2}$		6042	$\frac{9\frac{1}{2}}{2}$		8542	$\frac{10\frac{1}{2}}{2}$
7	109375	$\frac{1}{2}$	23	359375	$\frac{4\frac{3}{8}}{8}$	39	609375	$\frac{9\frac{3}{8}}{8}$	55	859375	$\frac{10\frac{3}{8}}{8}$
	1146	$\frac{1}{2}$		3646	$\frac{4\frac{1}{2}}{4}$		6146	$\frac{9\frac{1}{2}}{4}$		8646	$\frac{10\frac{1}{2}}{4}$
	1198	$\frac{1}{2}$		3698	$\frac{4\frac{1}{4}}{2}$		6198	$\frac{9\frac{1}{4}}{2}$		8698	$\frac{10\frac{1}{4}}{2}$
8	1250	$\frac{1}{2}$	24	3750	$\frac{4\frac{1}{2}}{2}$	40	6250	$\frac{9\frac{1}{2}}{2}$	56	8750	$\frac{10\frac{1}{2}}{2}$
	1302	$\frac{1}{2}$		3802	$\frac{4\frac{3}{4}}{4}$		6302	$\frac{9\frac{3}{4}}{4}$		8802	$\frac{10\frac{3}{4}}{4}$
	1354	$\frac{1}{2}$		3854	$\frac{4\frac{3}{4}}{2}$		6354	$\frac{9\frac{3}{4}}{2}$		8854	$\frac{10\frac{3}{4}}{2}$
9	140625	$\frac{1}{2}$	25	390625	$\frac{4\frac{3}{8}}{8}$	41	640625	$\frac{9\frac{3}{8}}{8}$	57	890625	$\frac{10\frac{3}{8}}{8}$
	1458	$\frac{1}{2}$		3958	$\frac{4\frac{1}{2}}{4}$		6458	$\frac{9\frac{1}{2}}{4}$		8958	$\frac{10\frac{1}{2}}{4}$
	1510	$\frac{1}{2}$		4010	$\frac{4\frac{1}{2}}{2}$		6510	$\frac{9\frac{1}{2}}{2}$		9010	$\frac{10\frac{1}{2}}{2}$
10	15625	$\frac{1}{2}$	26	40625	$\frac{4\frac{1}{4}}{4}$	42	65625	$\frac{9\frac{1}{4}}{4}$	58	90625	$\frac{10\frac{1}{4}}{4}$
	1615	$\frac{1}{2}$		4115	$\frac{4\frac{1}{4}}{2}$		6615	$\frac{9\frac{1}{4}}{2}$		9115	$\frac{10\frac{1}{4}}{2}$
	1667	$\frac{1}{2}$		4167	$\frac{4\frac{1}{2}}{2}$		6667	$\frac{9\frac{1}{2}}{2}$		9167	$\frac{11}{2}$
11	171875	$\frac{2}{16}$	27	421875	$\frac{3\frac{3}{8}}{16}$	43	671875	$\frac{8\frac{3}{8}}{16}$	59	921875	$\frac{11\frac{3}{8}}{16}$
	1771	$\frac{2\frac{1}{4}}{16}$		4271	$\frac{3\frac{1}{4}}{16}$		6771	$\frac{8\frac{1}{4}}{16}$		9271	$\frac{11\frac{1}{4}}{16}$
	1823	$\frac{2}{8}$		4323	$\frac{3\frac{1}{2}}{8}$		6823	$\frac{8\frac{1}{2}}{8}$		9323	$\frac{11\frac{1}{2}}{8}$
12	1875	$\frac{2\frac{1}{4}}{8}$	28	4375	$\frac{3\frac{1}{4}}{4}$	44	6875	$\frac{8\frac{1}{4}}{4}$	60	9375	$\frac{11\frac{1}{4}}{4}$
	1927	$\frac{2\frac{1}{2}}{8}$		4427	$\frac{3\frac{1}{2}}{4}$		6927	$\frac{8\frac{1}{2}}{4}$		9427	$\frac{11\frac{1}{2}}{4}$
	1979	$\frac{2\frac{3}{4}}{8}$		4479	$\frac{3\frac{3}{4}}{4}$		6979	$\frac{8\frac{3}{4}}{4}$		9479	$\frac{11\frac{3}{4}}{4}$
13	203125	$\frac{2\frac{1}{8}}{16}$	29	453125	$\frac{5}{16}$	45	703125	$\frac{8\frac{5}{8}}{16}$	61	953125	$\frac{11\frac{5}{8}}{16}$
	2083	$\frac{2\frac{1}{4}}{16}$		4583	$\frac{5\frac{1}{4}}{16}$		7083	$\frac{8\frac{1}{4}}{16}$		9583	$\frac{11\frac{1}{4}}{16}$
	2135	$\frac{2\frac{1}{2}}{16}$		4635	$\frac{5\frac{1}{2}}{16}$		7135	$\frac{8\frac{1}{2}}{16}$		9635	$\frac{11\frac{1}{2}}{16}$
14	21875	$\frac{2\frac{3}{8}}{16}$	30	46875	$\frac{5\frac{3}{8}}{16}$	46	71875	$\frac{8\frac{3}{8}}{16}$	62	96875	$\frac{11\frac{3}{8}}{16}$
	2240	$\frac{2\frac{1}{4}}{8}$		4740	$\frac{5\frac{1}{4}}{8}$		7240	$\frac{8\frac{1}{4}}{8}$		9740	$\frac{11\frac{1}{4}}{8}$
	2292	$\frac{2\frac{1}{2}}{8}$		4792	$\frac{5\frac{1}{2}}{8}$		7292	$\frac{8\frac{1}{2}}{8}$		9792	$\frac{11\frac{1}{2}}{8}$
15	234375	$\frac{2\frac{3}{4}}{16}$	31	484375	$\frac{5\frac{3}{4}}{16}$	47	734375	$\frac{8\frac{3}{4}}{16}$	63	984375	$\frac{11\frac{3}{4}}{16}$
	2396	$\frac{2\frac{3}{8}}{8}$		4896	$\frac{5\frac{3}{8}}{8}$		7396	$\frac{8\frac{3}{8}}{8}$		9896	$\frac{11\frac{3}{8}}{8}$
	2448	$\frac{2\frac{1}{2}}{4}$		4948	$\frac{5\frac{1}{2}}{4}$		7448	$\frac{8\frac{1}{2}}{4}$		9948	$\frac{11\frac{1}{2}}{4}$
16	2500	$\frac{3}{8}$	32	5000	$\frac{6}{8}$	48	7500	$\frac{9}{8}$	64	1 0000	$\frac{12}{8}$



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